

CITY OF FONTANA
SOUTH FONTANA MASTER DRAINAGE PLAN
MASTER PLAN DRAINAGE STUDY
FOR

EMPIRE CENTER AREA

FACILITIES:

P1, P2, P3, DZ-1, DZ-2, DZ-2A, DZ-3, DZ-4, DZ-5, DZ-6, & DZ-7

VOLUME NO. 2

PREPARED FOR: THE CITY OF FONTANA

STEVEN NAWAR, P.E. – PROJECT MANAGER

PREPARED BY: HALL & FOREMAN, INC.

43513 RIDGE PARK DRIVE
TEMECULA, CA 92590
(951) 676-6726

GERALD J. BARIL, P.E. – PROJECT MANAGER

HERMAN HOVAGIMYAN, P.E. – PROJECT ENGINEER

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JN 04339

APPROVED
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TABLE OF CONTENTS

VOLUME NO. 1

- ☐ INTRODUCTION
- ☐ OVERVIEW AND DISCUSSION
- ☐ FINDINGS
- ☐ RECOMMENDATIONS

APPENDICES

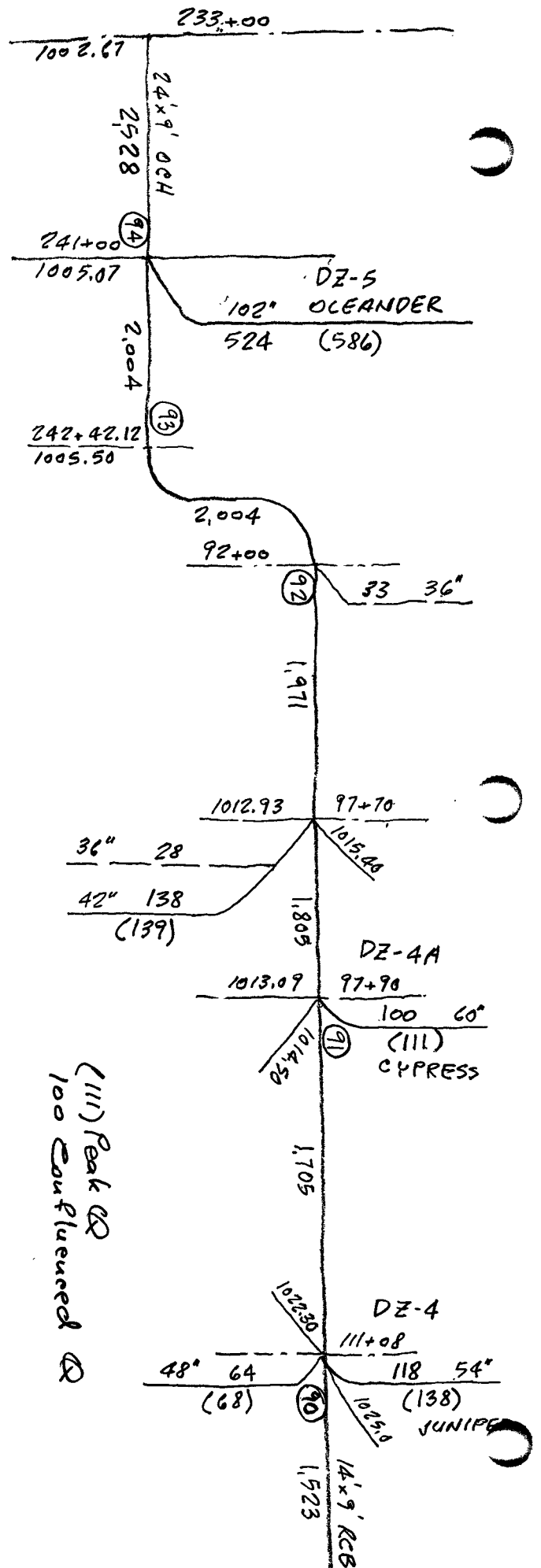
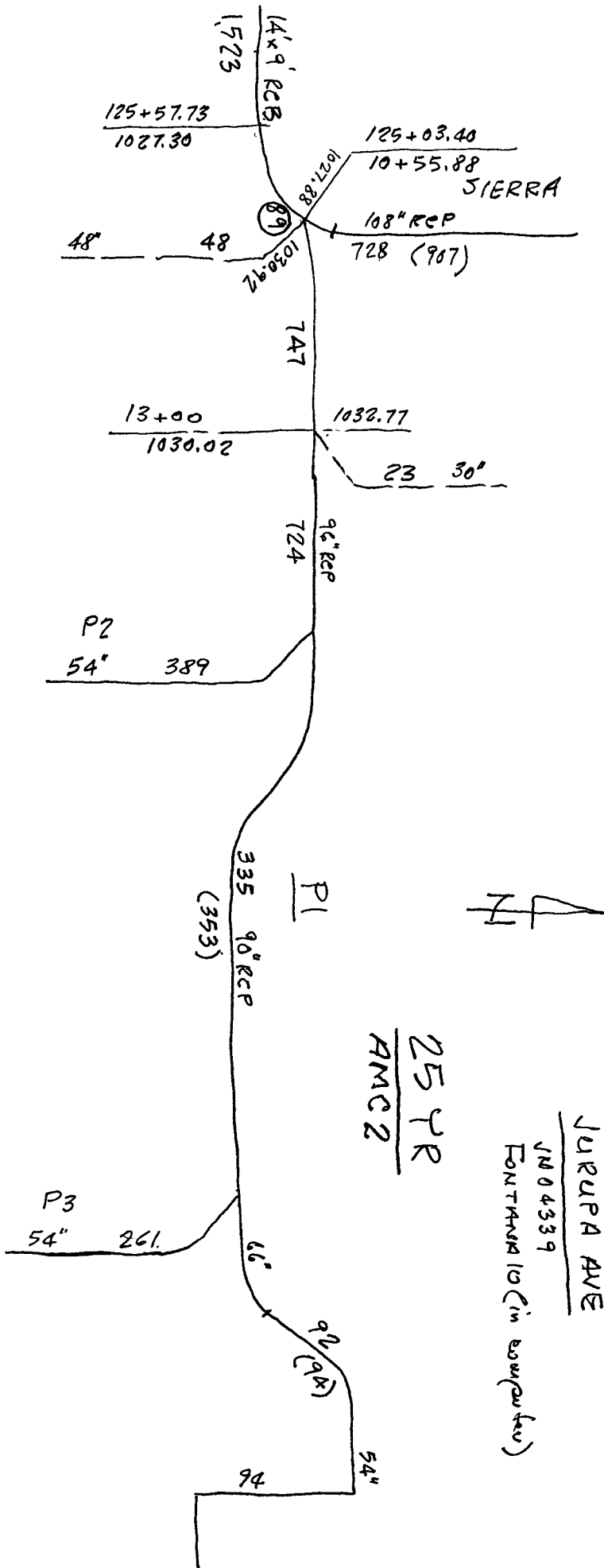
1. 100 – YEAR AMC 3 HYDROLOGY
 - ☐ HYDROLOGIC DATA
 - ☐ Q-100 SUMMARY W/O DETENTION
 - ☐ Q-100 SUMMARY W/DETENTION
 - ☐ HYDROLOGY CALCULATIONS
 - ☐ HYDRAULIC CALCULATIONS
 - DECLEZ CHANNEL W/O DETENTION
 - JURUPA RCB W/O DETENTION
 - DECLEZ CHANNEL W/DETENTION
 - JURUPA RCB W/DETENTION
2. 100-YEAR AMC 2 HYDROLOGY
 - ☐ Q-100 SUMMARY W/O DETENTION
 - ☐ HYDROLOGY CALCULATIONS
 - ☐ HYDRAULIC CALCULATIONS
 - DECLEZ CHANNEL
 - JURUPA RCB

VOLUME NO. 2

APPENDICES

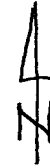
3. 25 – YEAR AMC 2 HYDROLOGY
 - ☐ Q-25 SUMMARY W/O DETENTION
 - ☐ HYDROLOGY CALCULATIONS
 - ☐ HYDRAULIC CALCULATIONS
 - DECLEZ CHANNEL
 - JURUPA RCB
 - SIERRA AVENUE LINE DZ-3 (REACHES A, B, C, & D)
 - JURUPA RCB
4. MASTER DRAINAGE PLAN UPDATES
 - ☐ SUMMARY
 - ☐ HYDRAULIC CALCULATIONS

Q₂₅ SUMMARIES

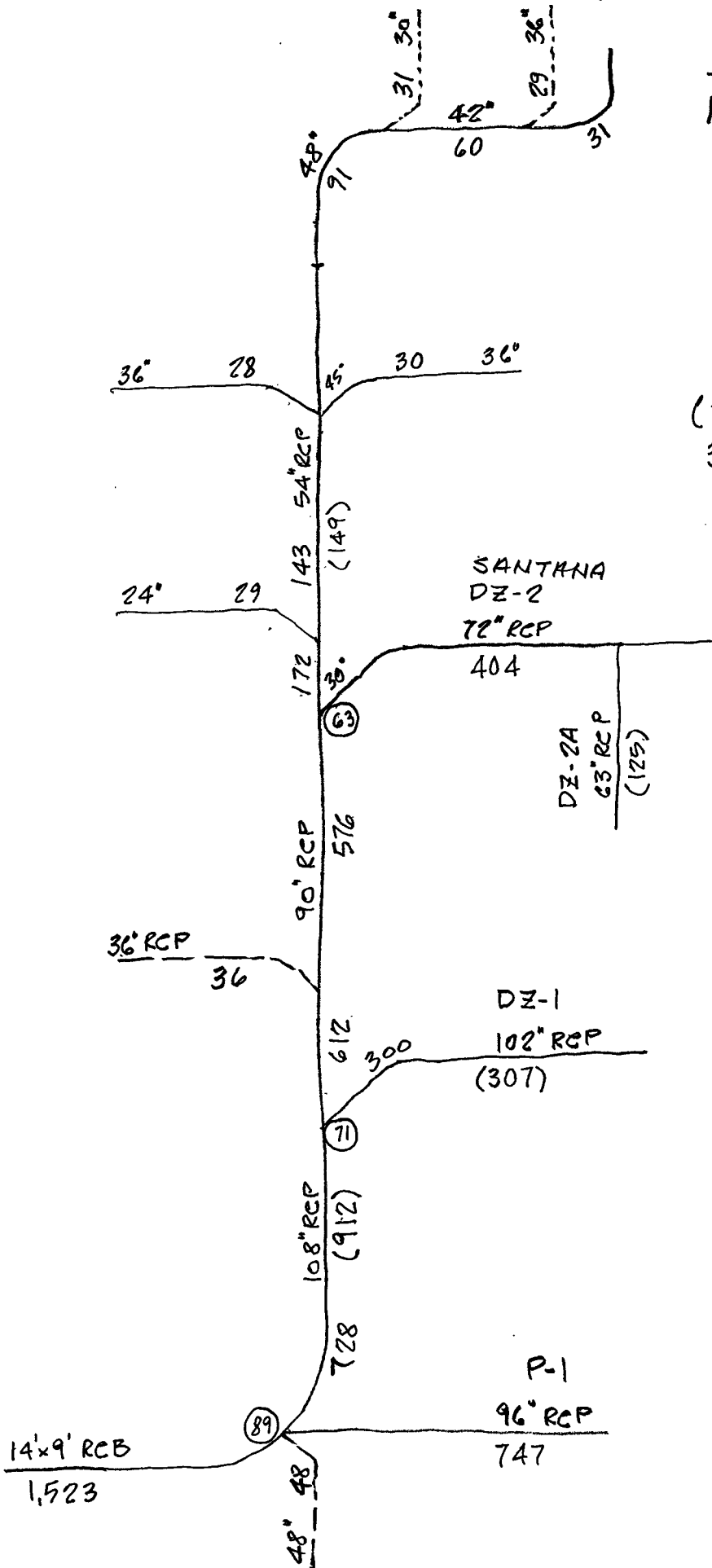


SIERRA AVE. W/O DETENTION
FONTANA 7 (in computer)

25 YR.
AMC 2



(307) Peak Q
300 Confluent Q





FONTANA

JOB No. 04339
BY HERMAN
DATE 8/2/04
SHT. 149
OF

◆ LAND PLANNING ◆ CIVIL ENGINEERING ◆ SURVEYING

25 YEAR
W/AMCZ

LINE "DZ-2A"

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
 Rational Hydrology Study Date: 01/13/05

FONTANA / LINE DZ-2A HYDROLOGY
 25 YEAR STORM
 JN 04339

Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 25.0
 10 Year storm 1 hour rainfall = 0.930(In.)
 100 Year storm 1 hour rainfall = 1.350(In.)
 Computed rainfall intensity:
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)
 Slope used for rainfall intensity curve b = 0.6000
 Soil antecedent moisture condition (AMC) = 2

 Process from Point/Station 112.000 to Point/Station 113.000
 **** INITIAL AREA EVALUATION ****

SCHOOL subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.6000 Max loss rate(Fm)= 0.440(In/Hr)
 Initial subarea data:
 Initial area flow distance = 800.000(Ft.)
 Top (of initial area) elevation = 1085.300(Ft.)
 Bottom (of initial area) elevation = 1080.300(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00625 s(%)= 0.63
 $TC = k(0.412)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 16.480 min.
 Rainfall intensity = 2.382(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.734
 Subarea runoff = 9.612(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 0.600
 Initial area Fm value = 0.440(In/Hr)

 Process from Point/Station 113.000 to Point/Station 116.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1080.300(Ft.)
 End of street segment elevation = 1076.600(Ft.)
 Length of street segment = 730.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 19.224(CFS)
 Depth of flow = 0.492(Ft.), Average velocity = 2.391(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 19.873(Ft.)
 Flow velocity = 2.39(Ft/s)
 Travel time = 5.09 min. TC = 21.57 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.027(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.813
 Subarea runoff = 17.582(CFS) for 11.000(Ac.)
 Total runoff = 27.194(CFS)
 Effective area this stream = 16.50(Ac.)
 Total Study Area (Main Stream No. 1) = 16.50(Ac.)
 Area averaged Fm value = 0.196(In/Hr)
 Street flow at end of street = 27.194(CFS)
 Half street flow at end of street = 13.597(CFS)
 Depth of flow = 0.540(Ft.), Average velocity = 2.737(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

 Process from Point/Station 116.000 to Point/Station 116.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 16.500(Ac.)
 Runoff from this stream = 27.194(CFS)
 Time of concentration = 21.57 min.
 Rainfall intensity = 2.027(In/Hr)
 Area averaged loss rate (Fm) = 0.1957(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.2667

 Process from Point/Station 114.000 to Point/Station 115.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1093.600(Ft.)
 Bottom (of initial area) elevation = 1084.400(Ft.)
 Difference in elevation = 9.200(Ft.)
 Slope = 0.00920 s(%)= 0.92
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 12.306 min.
 Rainfall intensity = 2.838(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.877
 Subarea runoff = 13.687(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

++++++
 Process from Point/Station 115.000 to Point/Station 116.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1084.400(Ft.)
 End of street segment elevation = 1076.600(Ft.)
 Length of street segment = 600.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 22.397(CFS)
 Depth of flow = 0.447(Ft.), Average velocity = 3.539(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 17.587(Ft.)
 Flow velocity = 3.54(Ft/s)
 Travel time = 2.83 min. TC = 15.13 min.

Adding area flow to street

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.507(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.874
 Subarea runoff = 13.695(CFS) for 7.000(Ac.)
 Total runoff = 27.382(CFS)
 Effective area this stream = 12.50(Ac.)

Total Study Area (Main Stream No. 1) = 29.00 (Ac.)
 Area averaged Fm value = 0.073 (In/Hr)
 Street flow at end of street = 27.382 (CFS)
 Half street flow at end of street = 13.691 (CFS)
 Depth of flow = 0.475 (Ft.), Average velocity = 3.719 (Ft/s)
 Flow width (from curb towards crown) = 19.000 (Ft.)

+++++
 Process from Point/Station 116.000 to Point/Station 116.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 12.500 (Ac.)
 Runoff from this stream = 27.382 (CFS)
 Time of concentration = 15.13 min.
 Rainfall intensity = 2.507 (In/Hr)
 Area averaged loss rate (Fm) = 0.0734 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	27.194	21.57	2.027
2	27.382	15.13	2.507
Qmax(1) =			
	1.000 *	1.000 *	27.194) +
	0.803 *	1.000 *	27.382) + = 49.172
Qmax(2) =			
	1.262 *	0.702 *	27.194) +
	1.000 *	1.000 *	27.382) + = 51.465

Total of 2 streams to confluence:
 Flow rates before confluence point:
 27.194 27.382
 Maximum flow rates at confluence using above data:
 49.172 51.465
 Area of streams before confluence:
 16.500 12.500
 Effective area values after confluence:
 29.000 24.075
 Results of confluence:
 Total flow rate = 51.465 (CFS)
 Time of concentration = 15.132 min.
 Effective stream area after confluence = 24.075 (Ac.)
 Stream Area average Pervious fraction (Ap) = 0.195
 Stream Area average soil loss rate (Fm) = 0.143 (In/Hr)
 Study area (this main stream) = 29.00 (Ac.)

+++++
 Process from Point/Station 116.000 to Point/Station 52.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1069.600 (Ft.)
 Downstream point/station elevation = 1061.900 (Ft.)
 Pipe length = 650.00 (Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 51.465 (CFS)
 Given pipe size = 39.00 (In.)

Calculated individual pipe flow = 51.465(CFS)
 Normal flow depth in pipe = 21.16(In.)
 Flow top width inside pipe = 38.86(In.)
 Critical Depth = 27.48(In.)
 Pipe flow velocity = 11.20(Ft/s)
 Travel time through pipe = 0.97 min.
 Time of concentration (TC) = 16.10 min.

+++++
 Process from Point/Station 52.000 to Point/Station 52.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 24.075(Ac.)
 Runoff from this stream = 51.465(CFS)
 Time of concentration = 16.10 min.
 Rainfall intensity = 2.416(In/Hr)
 Area averaged loss rate (Fm) = 0.1430(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1948

+++++
 Process from Point/Station 117.000 to Point/Station 118.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1076.000(Ft.)
 Bottom (of initial area) elevation = 1071.000(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.902 min.
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875
 Subarea runoff = 11.541(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

+++++
 Process from Point/Station 118.000 to Point/Station 119.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1071.000(Ft.)
 End of street segment elevation = 1068.900(Ft.)
 Length of street segment = 420.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020

Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 23.083(CFS)
 Depth of flow = 0.517(Ft.), Average velocity = 2.554(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 2.55(Ft/s)
 Travel time = 2.74 min. TC = 16.64 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073(In/Hr)
 Rainfall intensity = 2.368(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.872
 Subarea runoff = 19.438(CFS) for 10.000(Ac.)
 Total runoff = 30.980(CFS)
 Effective area this stream = 15.00(Ac.)
 Total Study Area (Main Stream No. 1) = 44.00(Ac.)
 Area averaged Fm value = 0.073(In/Hr)
 Street flow at end of street = 30.980(CFS)
 Half street flow at end of street = 15.490(CFS)
 Depth of flow = 0.561(Ft.), Average velocity = 2.871(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000(Ft.)

++++++
 Process from Point/Station 119.000 to Point/Station 119.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 15.000(Ac.)
 Runoff from this stream = 30.980(CFS)
 Time of concentration = 16.64 min.
 Rainfall intensity = 2.368(In/Hr)
 Area averaged loss rate (Fm) = 0.0734(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	51.465	16.10	2.416
2	30.980	16.64	2.368
Qmax(1) =			
	1.000 *	1.000 *	51.465) +
	1.021 *	0.967 *	30.980) + = 82.054
Qmax(2) =			

0.979 * 1.000 * 51.465) +
 1.000 * 1.000 * 30.980) + = 81.364

Total of 2 streams to confluence:

Flow rates before confluence point:

51.465 30.980

Maximum flow rates at confluence using above data:

82.054 81.364

Area of streams before confluence:

24.075 15.000

Effective area values after confluence:

38.585 39.075

Results of confluence:

Total flow rate = 82.054(CFS)

Time of concentration = 16.099 min.

Effective stream area after confluence = 38.585(Ac.)

Stream Area average Pervious fraction(Ap) = 0.158

Stream Area average soil loss rate(Fm) = 0.116(In/Hr)

Study area (this main stream) = 39.08(Ac.)

+++++
 Process from Point/Station 52.000 to Point/Station 53.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1061.900(Ft.)

Downstream point/station elevation = 1059.400(Ft.)

Pipe length = 500.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 82.054(CFS)

Given pipe size = 42.00(In.)

NOTE: Normal flow is pressure flow in user selected pipe size.

The approximate hydraulic grade line above the pipe invert is

2.519(Ft.) at the headworks or inlet of the pipe(s)

Pipe friction loss = 3.325(Ft.)

Minor friction loss = 1.694(Ft.) K-factor = 1.50

Pipe flow velocity = 8.53(Ft/s)

Travel time through pipe = 0.98 min.

Time of concentration (TC) = 17.08 min.

+++++
 Process from Point/Station 53.000 to Point/Station 53.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 38.585(Ac.)

Runoff from this stream = 82.054(CFS)

Time of concentration = 17.08 min.

Rainfall intensity = 2.332(In/Hr)

Area averaged loss rate (Fm) = 0.1163(In/Hr)

Area averaged Pervious ratio (Ap) = 0.1584

+++++
 Process from Point/Station 120.000 to Point/Station 121.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1072.000(Ft.)
 Bottom (of initial area) elevation = 1067.000(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%)= 0.50
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.902 min.
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875
 Subarea runoff = 12.696(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

++++++
 Process from Point/Station 121.000 to Point/Station 122.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1067.000(Ft.)
 End of street segment elevation = 1064.700(Ft.)
 Length of street segment = 450.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 23.083(CFS)
 Depth of flow = 0.516(Ft.), Average velocity = 2.571(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 2.57(Ft/s)
 Travel time = 2.92 min. TC = 16.82 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.353(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.872
 Subarea runoff = 17.056(CFS) for 9.000(Ac.)
 Total runoff = 29.752(CFS)
 Effective area this stream = 14.50(Ac.)
 Total Study Area (Main Stream No. 1) = 58.50(Ac.)

Area averaged Fm value = 0.073(In/Hr)
 Street flow at end of street = 29.752(CFS)
 Half street flow at end of street = 14.876(CFS)
 Depth of flow = 0.553(Ft.), Average velocity = 2.844(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++
 Process from Point/Station 122.000 to Point/Station 122.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 14.500(Ac.)
 Runoff from this stream = 29.752(CFS)
 Time of concentration = 16.82 min.
 Rainfall intensity = 2.353(In/Hr)
 Area averaged loss rate (Fm) = 0.0734(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	82.054	17.08	2.332
2	29.752	16.82	2.353
Qmax(1) =			
	1.000 *	1.000 *	82.054) +
	0.991 *	1.000 *	29.752) + = 111.529
Qmax(2) =			
	1.010 *	0.985 *	82.054) +
	1.000 *	1.000 *	29.752) + = 111.350

Total of 2 streams to confluence:
 Flow rates before confluence point:

82.054 29.752

Maximum flow rates at confluence using above data:
 111.529 111.350

Area of streams before confluence:
 38.585 14.500

Effective area values after confluence:
 53.085 52.505

Results of confluence:

Total flow rate = 111.529(CFS)
 Time of concentration = 17.076 min.
 Effective stream area after confluence = 53.085(Ac.)
 Stream Area average Pervious fraction(Ap) = 0.142
 Stream Area average soil loss rate(Fm) = 0.105(In/Hr)
 Study area (this main stream) = 53.08(Ac.)

+++++
 Process from Point/Station 53.000 to Point/Station 54.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1052.500(Ft.)
 Downstream point/station elevation = 1048.200(Ft.)
 Pipe length = 860.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 111.529(CFS)
 Given pipe size = 60.00(In.)

Calculated individual pipe flow = 111.529(CFS)
 Normal flow depth in pipe = 33.70(In.)
 Flow top width inside pipe = 59.54(In.)
 Critical Depth = 36.14(In.)
 Pipe flow velocity = 9.83(Ft/s)
 Travel time through pipe = 1.46 min.
 Time of concentration (TC) = 18.53 min.

+++++
 Process from Point/Station 54.000 to Point/Station 54.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 53.085(Ac.)
 Runoff from this stream = 111.529(CFS)
 Time of concentration = 18.53 min.
 Rainfall intensity = 2.220(In/Hr)
 Area averaged loss rate (Fm) = 0.1046(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1425

+++++
 Process from Point/Station 123.000 to Point/Station 124.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1064.700(Ft.)
 Bottom (of initial area) elevation = 1059.700(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%)= 0.50
 $TC = k(0.304) * [(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.902 min.
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875
 Subarea runoff = 16.158(CFS)
 Total initial stream area = 7.000(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

+++++
 Process from Point/Station 124.000 to Point/Station 124.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 7.000(Ac.)
 Runoff from this stream = 16.158(CFS)
 Time of concentration = 13.90 min.
 Rainfall intensity = 2.638(In/Hr)
 Area averaged loss rate (Fm) = 0.0734(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	111.529	18.53	2.220
2	16.158	13.90	2.638

Qmax(1) =

1.000 *	1.000 *	111.529) +	
0.837 *	1.000 *	16.158) + =	125.052

Qmax(2) =

1.198 *	0.750 *	111.529) +	
1.000 *	1.000 *	16.158) + =	116.346

Total of 2 streams to confluence:

Flow rates before confluence point:

111.529 16.158

Maximum flow rates at confluence using above data:

125.052 116.346

Area of streams before confluence:

53.085 7.000

Effective area values after confluence:

60.085 46.817

Results of confluence:

Total flow rate = 125.052(CFS)

Time of concentration = 18.535 min.

Effective stream area after confluence = 60.085 (Ac.)

Stream Area average Pervious fraction(Ap) = 0.138

Stream Area average soil loss rate(Fm) = 0.101(In/Hr)

Study area (this main stream) = 60.08 (Ac.)

+++++
 Process from Point/Station 54.000 to Point/Station 55.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1048.200(Ft.)

Downstream point/station elevation = 1046.500(Ft.)

Pipe length = 340.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 125.052(CFS)

Given pipe size = 63.00(In.)

Calculated individual pipe flow = 125.052(CFS)

Normal flow depth in pipe = 35.02(In.)

Flow top width inside pipe = 62.61(In.)

Critical Depth = 37.85(In.)

Pipe flow velocity = 10.11(Ft/s)

Travel time through pipe = 0.56 min.

Time of concentration (TC) = 19.10 min.

End of computations, Total Study Area = 65.50 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.142

Area averaged SCS curve number = 56.0

LINE "DZ-2"

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
 Rational Hydrology Study Date: 01/13/05

FONTANA / LINE DZ-2 HYDROLOGY
 25 YEAR STORM
 JN 04339

Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 25.0
 10 Year storm 1 hour rainfall = 0.930(In.)
 100 Year storm 1 hour rainfall = 1.350(In.)
 Computed rainfall intensity:
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)
 Slope used for rainfall intensity curve b = 0.6000
 Soil antecedent moisture condition (AMC) = 2

 Process from Point/Station 100.000 to Point/Station 101.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 960.000(Ft.)
 Top (of initial area) elevation = 1103.000(Ft.)
 Bottom (of initial area) elevation = 1098.400(Ft.)
 Difference in elevation = 4.600(Ft.)
 Slope = 0.00479 s(%)= 0.48
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.794 min.
 Rainfall intensity = 2.651(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.867
 Subarea runoff = 11.488(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.098(In/Hr)

 Process from Point/Station 101.000 to Point/Station 102.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1098.400(Ft.)
 End of street segment elevation = 1093.600(Ft.)
 Length of street segment = 590.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 17.231(CFS)
 Depth of flow = 0.443(Ft.), Average velocity = 2.781(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 17.399(Ft.)
 Flow velocity = 2.78(Ft/s)
 Travel time = 3.54 min. TC = 17.33 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.311(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.867
 Subarea runoff = 8.544(CFS) for 5.000(Ac.)
 Total runoff = 20.032(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 10.00(Ac.)
 Area averaged Fm value = 0.086(In/Hr)
 Street flow at end of street = 20.032(CFS)
 Half street flow at end of street = 10.016(CFS)
 Depth of flow = 0.464(Ft.), Average velocity = 2.886(Ft/s)
 Flow width (from curb towards crown)= 18.438(Ft.)

++++++
 Process from Point/Station 102.000 to Point/Station 50.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1085.300(Ft.)
 Downstream point/station elevation = 1079.500(Ft.)
 Pipe length = 460.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 20.032(CFS)
 Given pipe size = 24.00(In.)
 Calculated individual pipe flow = 20.032(CFS)
 Normal flow depth in pipe = 16.08(In.)
 Flow top width inside pipe = 22.57(In.)
 Critical Depth = 19.29(In.)
 Pipe flow velocity = 8.96(Ft/s)
 Travel time through pipe = 0.86 min.
 Time of concentration (TC) = 18.19 min.

++++++
 Process from Point/Station 50.000 to Point/Station 50.000

**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 10.000(Ac.)
 Runoff from this stream = 20.032(CFS)
 Time of concentration = 18.19 min.
 Rainfall intensity = 2.245(In/Hr)
 Area averaged loss rate (Fm) = 0.0856(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

+++++
 Process from Point/Station 103.000 to Point/Station 104.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type

Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1103.000(Ft.)
 Bottom (of initial area) elevation = 1098.400(Ft.)
 Difference in elevation = 4.600(Ft.)
 Slope = 0.00460 s(%) = 0.46
 $TC = k(0.304) * [(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 14.136 min.
 Rainfall intensity = 2.612(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.866
 Subarea runoff = 12.445(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.098(In/Hr)

+++++
 Process from Point/Station 104.000 to Point/Station 105.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1098.400(Ft.)
 End of street segment elevation = 1092.200(Ft.)
 Length of street segment = 700.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 23.193(CFS)
 Depth of flow = 0.479(Ft.), Average velocity = 3.090(Ft/s)
 Streetflow hydraulics at midpoint of street travel:

Halfstreet flow width = 19.189(Ft.)
 Flow velocity = 3.09(Ft/s)
 Travel time = 3.78 min. TC = 17.91 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.098(In/Hr)
 Rainfall intensity = 2.266(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.861
 Subarea runoff = 16.826(CFS) for 9.500(Ac.)
 Total runoff = 29.271(CFS)
 Effective area this stream = 15.00(Ac.)
 Total Study Area (Main Stream No. 1) = 25.00(Ac.)
 Area averaged Fm value = 0.098(In/Hr)
 Street flow at end of street = 29.271(CFS)
 Half street flow at end of street = 14.636(CFS)
 Depth of flow = 0.511(Ft.), Average velocity = 3.335(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000(Ft.)

++++++
 Process from Point/Station 105.000 to Point/Station 50.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1083.800(Ft.)
 Downstream point/station elevation = 1079.500(Ft.)
 Pipe length = 570.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 29.271(CFS)
 Given pipe size = 30.00(In.)
 Calculated individual pipe flow = 29.271(CFS)
 Normal flow depth in pipe = 20.70(In.)
 Flow top width inside pipe = 27.75(In.)
 Critical Depth = 22.15(In.)
 Pipe flow velocity = 8.10(Ft/s)
 Travel time through pipe = 1.17 min.
 Time of concentration (TC) = 19.08 min.

++++++
 Process from Point/Station 50.000 to Point/Station 50.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 15.000(Ac.)
 Runoff from this stream = 29.271(CFS)
 Time of concentration = 19.08 min.
 Rainfall intensity = 2.181(In/Hr)
 Area averaged loss rate (Fm) = 0.0978(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
---------------	--------------------	-------------	-------------------------------

1	20.032	18.19	2.245	
2	29.271	19.08	2.181	
Qmax(1) =				
	1.000 *	1.000 *	20.032) +	
	1.031 *	0.953 *	29.271) + =	48.782
Qmax(2) =				
	0.970 *	1.000 *	20.032) +	
	1.000 *	1.000 *	29.271) + =	48.709

Total of 2 streams to confluence:

Flow rates before confluence point:

20.032 29.271

Maximum flow rates at confluence using above data:

48.782 48.709

Area of streams before confluence:

10.000 15.000

Effective area values after confluence:

24.293 25.000

Results of confluence:

Total flow rate = 48.782(CFS)

Time of concentration = 18.186 min.

Effective stream area after confluence = 24.293(Ac.)

Stream Area average Pervious fraction(Ap) = 0.100

Stream Area average soil loss rate(Fm) = 0.093(In/Hr)

Study area (this main stream) = 25.00(Ac.)

 Process from Point/Station 50.000 to Point/Station 51.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1079.500(Ft.)
 Downstream point/station elevation = 1071.300(Ft.)
 Pipe length = 1320.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 48.782(CFS)
 Given pipe size = 39.00(In.)
 Calculated individual pipe flow = 48.782(CFS)
 Normal flow depth in pipe = 25.20(In.)
 Flow top width inside pipe = 37.30(In.)
 Critical Depth = 26.75(In.)
 Pipe flow velocity = 8.61(Ft/s)
 Travel time through pipe = 2.56 min.
 Time of concentration (TC) = 20.74 min.

 Process from Point/Station 51.000 to Point/Station 51.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 24.293(Ac.)
 Runoff from this stream = 48.782(CFS)
 Time of concentration = 20.74 min.
 Rainfall intensity = 2.075(In/Hr)
 Area averaged loss rate (Fm) = 0.0929(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

 Process from Point/Station 106.000 to Point/Station 107.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1093.600(Ft.)
 Bottom (of initial area) elevation = 1085.400(Ft.)
 Difference in elevation = 8.200(Ft.)
 Slope = 0.00820 s(%)= 0.82
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 12.592 min.
 Rainfall intensity = 2.800(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.876
 Subarea runoff = 13.494(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

++++++
 Process from Point/Station 107.000 to Point/Station 108.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1085.400(Ft.)
 End of street segment elevation = 1078.300(Ft.)
 Length of street segment = 700.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 20.855(CFS)
 Depth of flow = 0.454(Ft.), Average velocity = 3.167(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 17.948(Ft.)
 Flow velocity = 3.17(Ft/s)
 Travel time = 3.68 min. TC = 16.28 min.
 Adding area flow to street

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.400(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.872

Subarea runoff = 10.586(CFS) for 6.000(Ac.)
 Total runoff = 24.081(CFS)
 Effective area this stream = 11.50(Ac.)
 Total Study Area (Main Stream No. 1) = 36.50(Ac.)
 Area averaged Fm value = 0.073(In/Hr)
 Street flow at end of street = 24.081(CFS)
 Half street flow at end of street = 12.040(CFS)
 Depth of flow = 0.474(Ft.), Average velocity = 3.282(Ft/s)
 Flow width (from curb towards crown) = 18.968(Ft.)

++++++
 Process from Point/Station 108.000 to Point/Station 108.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 11.500(Ac.)
 Runoff from this stream = 24.081(CFS)
 Time of concentration = 16.28 min.
 Rainfall intensity = 2.400(In/Hr)
 Area averaged loss rate (Fm) = 0.0734(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	48.782	20.74	2.075
2	24.081	16.28	2.400
Qmax(1) =			
	1.000 *	1.000 *	48.782) +
	0.860 *	1.000 *	24.081) + = 69.500
Qmax(2) =			
	1.164 *	0.785 *	48.782) +
	1.000 *	1.000 *	24.081) + = 68.635

Total of 2 streams to confluence:

Flow rates before confluence point:

48.782 24.081

Maximum flow rates at confluence using above data:

69.500 68.635

Area of streams before confluence:

24.293 11.500

Effective area values after confluence:

35.793 30.564

Results of confluence:

Total flow rate = 69.500(CFS)

Time of concentration = 20.741 min.

Effective stream area after confluence = 35.793(Ac.)

Stream Area average Pervious fraction(Ap) = 0.100

Stream Area average soil loss rate(Fm) = 0.087(In/Hr)

Study area (this main stream) = 35.79(Ac.)

++++++
 Process from Point/Station 51.000 to Point/Station 55.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1071.300(Ft.)

Downstream point/station elevation = 1062.400(Ft.)

Pipe length = 900.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 69.500(CFS)
 Given pipe size = 42.00(In.)
 Calculated individual pipe flow = 69.500(CFS)
 Normal flow depth in pipe = 25.76(In.)
 Flow top width inside pipe = 40.91(In.)
 Critical Depth = 31.34(In.)
 Pipe flow velocity = 11.23(Ft/s)
 Travel time through pipe = 1.34 min.
 Time of concentration (TC) = 22.08 min.

++++++
 Process from Point/Station 55.000 to Point/Station 55.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 35.793(Ac.)
 Runoff from this stream = 69.500(CFS)
 Time of concentration = 22.08 min.
 Rainfall intensity = 1.999(In/Hr)
 Area averaged loss rate (Fm) = 0.0866(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

++++++
 Process from Point/Station 109.000 to Point/Station 110.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1080.000(Ft.)
 Bottom (of initial area) elevation = 1073.700(Ft.)
 Difference in elevation = 6.300(Ft.)
 Slope = 0.00630 s(%) = 0.63
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.274 min.
 Rainfall intensity = 2.712(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.876
 Subarea runoff = 10.688(CFS)
 Total initial stream area = 4.500(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

++++++
 Process from Point/Station 110.000 to Point/Station 111.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1073.700(Ft.)
 End of street segment elevation = 1069.400(Ft.)
 Length of street segment = 350.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)

Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 15.438(CFS)
 Depth of flow = 0.403(Ft.), Average velocity = 3.161(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 15.396(Ft.)
 Flow velocity = 3.16(Ft/s)
 Travel time = 1.85 min. TC = 15.12 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.509(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.874
 Subarea runoff = 7.941(CFS) for 4.000(Ac.)
 Total runoff = 18.629(CFS)
 Effective area this stream = 8.50(Ac.)
 Total Study Area (Main Stream No. 1) = 45.00(Ac.)
 Area averaged Fm value = 0.073(In/Hr)
 Street flow at end of street = 18.629(CFS)
 Half street flow at end of street = 9.315(CFS)
 Depth of flow = 0.426(Ft.), Average velocity = 3.311(Ft/s)
 Flow width (from curb towards crown)= 16.560(Ft.)

++++++
 Process from Point/Station 111.000 to Point/Station 111.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 8.500(Ac.)
 Runoff from this stream = 18.629(CFS)
 Time of concentration = 15.12 min.
 Rainfall intensity = 2.509(In/Hr)
 Area averaged loss rate (Fm) = 0.0734(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

++++++
 Process from Point/Station 125.000 to Point/Station 126.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1093.200(Ft.)
 Bottom (of initial area) elevation = 1085.300(Ft.)
 Difference in elevation = 7.900(Ft.)
 Slope = 0.00790 s(%)= 0.79
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 12.687 min.
 Rainfall intensity = 2.787(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.876
 Subarea runoff = 13.433(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

 Process from Point/Station 126.000 to Point/Station 127.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1085.300(Ft.)
 End of street segment elevation = 1076.300(Ft.)
 Length of street segment = 900.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 28.086(CFS)
 Depth of flow = 0.498(Ft.), Average velocity = 3.402(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 3.40(Ft/s)
 Travel time = 4.41 min. TC = 17.10 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.330(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.872
 Subarea runoff = 22.115(CFS) for 12.000(Ac.)
 Total runoff = 35.547(CFS)
 Effective area this stream = 17.50(Ac.)
 Total Study Area (Main Stream No. 1) = 62.50(Ac.)
 Area averaged Fm value = 0.073(In/Hr)

Street flow at end of street = 35.547(CFS)
 Half street flow at end of street = 17.774(CFS)
 Depth of flow = 0.529(Ft.), Average velocity = 3.736(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000(Ft.)

+++++
 Process from Point/Station 127.000 to Point/Station 55.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1069.300(Ft.)
 Downstream point/station elevation = 1046.500(Ft.)
 Pipe length = 1000.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 35.547(CFS)
 Given pipe size = 30.00(In.)
 Calculated individual pipe flow = 35.547(CFS)
 Normal flow depth in pipe = 16.29(In.)
 Flow top width inside pipe = 29.89(In.)
 Critical Depth = 24.28(In.)
 Pipe flow velocity = 13.05(Ft/s)
 Travel time through pipe = 1.28 min.
 Time of concentration (TC) = 18.37 min.

+++++
 Process from Point/Station 55.000 to Point/Station 55.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 17.500(Ac.)
 Runoff from this stream = 35.547(CFS)
 Time of concentration = 18.37 min.
 Rainfall intensity = 2.232(In/Hr)
 Area averaged loss rate (Fm) = 0.0734(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

+++++
 Process from Point/Station 128.000 to Point/Station 129.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1078.300(Ft.)
 Bottom (of initial area) elevation = 1069.400(Ft.)
 Difference in elevation = 8.900(Ft.)
 Slope = 0.00890 s(%)= 0.89
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 12.388 min.
 Rainfall intensity = 2.827(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.877
 Subarea runoff = 22.306(CFS)
 Total initial stream area = 9.000(Ac.)

Pervious area fraction = 0.100
Initial area Fm value = 0.073(In/Hr)

+++++
Process from Point/Station 129.000 to Point/Station 129.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 4
Stream flow area = 9.000(Ac.)
Runoff from this stream = 22.306(CFS)
Time of concentration = 12.39 min.
Rainfall intensity = 2.827(In/Hr)
Area averaged loss rate (Fm) = 0.0734(In/Hr)
Area averaged Pervious ratio (Ap) = 0.1000

+++++
Process from Point/Station 55.000 to Point/Station 55.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Soil classification AP and SCS values input by user
USER INPUT of soil data for subarea
SCS curve number for soil(AMC 2) = 56.16
Pervious ratio(Ap) = 0.1380 Max loss rate(Fm)= 0.101(In/Hr)
Rainfall intensity = 2.220(In/Hr) for a 25.0 year storm
User specified values are as follows:
TC = 18.54 min. Rain intensity = 2.22(In/Hr)
Total area this stream = 60.09(Ac.)
Total Study Area (Main Stream No. 1) = 131.59(Ac.)
Total runoff = 125.05(CFS)

+++++
Process from Point/Station 55.000 to Point/Station 55.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 5
Stream flow area = 60.090(Ac.)
Runoff from this stream = 125.050(CFS)
Time of concentration = 18.54 min.
Rainfall intensity = 2.220(In/Hr)
Area averaged loss rate (Fm) = 0.1010(In/Hr)
Area averaged Pervious ratio (Ap) = 0.1380
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	69.500	22.08	1.999
2	18.629	15.12	2.509
3	35.547	18.37	2.232
4	22.306	12.39	2.827
5	125.050	18.54	2.220

Qmax(1) =

1.000 *	1.000 *	69.500) +	
0.791 *	1.000 *	18.629) +	
0.892 *	1.000 *	35.547) +	
0.699 *	1.000 *	22.306) +	
0.896 *	1.000 *	125.050) + =	243.559

Qmax(2) =
 1.267 * 0.685 * 69.500) +
 1.000 * 1.000 * 18.629) +
 1.128 * 0.823 * 35.547) +
 0.884 * 1.000 * 22.306) +
 1.136 * 0.816 * 125.050) + = 247.530

Qmax(3) =
 1.122 * 0.832 * 69.500) +
 0.886 * 1.000 * 18.629) +
 1.000 * 1.000 * 35.547) +
 0.784 * 1.000 * 22.306) +
 1.006 * 0.991 * 125.050) + = 259.054

Qmax(4) =
 1.433 * 0.561 * 69.500) +
 1.131 * 0.819 * 18.629) +
 1.276 * 0.674 * 35.547) +
 1.000 * 1.000 * 22.306) +
 1.287 * 0.668 * 125.050) + = 233.550

Qmax(5) =
 1.115 * 0.840 * 69.500) +
 0.881 * 1.000 * 18.629) +
 0.994 * 1.000 * 35.547) +
 0.779 * 1.000 * 22.306) +
 1.000 * 1.000 * 125.050) + = 259.305

Total of 5 streams to confluence:

Flow rates before confluence point:

69.500 18.629 35.547 22.306 125.050

Maximum flow rates at confluence using above data:

243.559 247.530 259.054 233.550 259.305

Area of streams before confluence:

35.793 8.500 17.500 9.000 60.090

Effective area values after confluence:

130.883 105.418 124.336 87.999 125.149

Results of confluence:

Total flow rate = 259.305(CFS)

Time of concentration = 18.540 min.

Effective stream area after confluence = 125.149(Ac.)

Stream Area average Pervious fraction(Ap) = 0.117

Stream Area average soil loss rate(Fm) = 0.090(In/Hr)

Study area (this main stream) = 130.88(Ac.)

+++++

Process from Point/Station 55.000 to Point/Station 56.000

**** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1046.500(Ft.)

Downstream point/station elevation = 1043.300(Ft.)

Pipe length = 1000.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 259.305(CFS)

Given pipe size = 81.00(In.)

Calculated individual pipe flow = 259.305(CFS)

Normal flow depth in pipe = 54.33(In.)

Flow top width inside pipe = 76.13(In.)

Critical Depth = 51.19(In.)

Pipe flow velocity = 10.16(Ft/s)

Travel time through pipe = 1.64 min.

Time of concentration (TC) = 20.18 min.

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+++++
Process from Point/Station      56.000 to Point/Station      56.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 125.149(Ac.)
 Runoff from this stream = 259.305(CFS)
 Time of concentration = 20.18 min.
 Rainfall intensity = 2.110(In/Hr)
 Area averaged loss rate (Fm) = 0.0897(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1174

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+++++
Process from Point/Station      130.000 to Point/Station      131.000
**** INITIAL AREA EVALUATION ****

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COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1092.200(Ft.)
 Bottom (of initial area) elevation = 1084.100(Ft.)
 Difference in elevation = 8.100(Ft.)
 Slope = 0.00810 s(%)= 0.81
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 12.623 min.
 Rainfall intensity = 2.795(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.876
 Subarea runoff = 13.474(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

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+++++
Process from Point/Station      131.000 to Point/Station      132.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

```

Top of street segment elevation = 1084.100(Ft.)
 End of street segment elevation = 1075.000(Ft.)
 Length of street segment = 900.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 28.173(CFS)

Depth of flow = 0.498(Ft.), Average velocity = 3.418(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 3.42(Ft/s)
 Travel time = 4.39 min. TC = 17.01 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.337(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.872
 Subarea runoff = 22.181(CFS) for 12.000(Ac.)
 Total runoff = 35.655(CFS)
 Effective area this stream = 17.50(Ac.)
 Total Study Area (Main Stream No. 1) = 149.09(Ac.)
 Area averaged Fm value = 0.073(In/Hr)
 Street flow at end of street = 35.655(CFS)
 Half street flow at end of street = 17.827(CFS)
 Depth of flow = 0.529(Ft.), Average velocity = 3.753(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++
 Process from Point/Station 132.000 to Point/Station 56.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1068.000(Ft.)
 Downstream point/station elevation = 1043.300(Ft.)
 Pipe length = 1100.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 35.655(CFS)
 Given pipe size = 30.00(In.)
 Calculated individual pipe flow = 35.655(CFS)
 Normal flow depth in pipe = 16.41(In.)
 Flow top width inside pipe = 29.87(In.)
 Critical Depth = 24.30(In.)
 Pipe flow velocity = 12.99(Ft/s)
 Travel time through pipe = 1.41 min.
 Time of concentration (TC) = 18.42 min.

++++++
 Process from Point/Station 56.000 to Point/Station 56.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 17.500(Ac.)
 Runoff from this stream = 35.655(CFS)
 Time of concentration = 18.42 min.
 Rainfall intensity = 2.228(In/Hr)
 Area averaged loss rate (Fm) = 0.0734(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

+++++

Process from Point/Station 133.000 to Point/Station 134.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1076.300(Ft.)
 Bottom (of initial area) elevation = 1070.900(Ft.)
 Difference in elevation = 5.400(Ft.)
 Slope = 0.00540 s(%) = 0.54
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.690 min.
 Rainfall intensity = 2.663(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875
 Subarea runoff = 12.817(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

+++++
 Process from Point/Station 134.000 to Point/Station 135.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1070.900(Ft.)
 End of street segment elevation = 1064.100(Ft.)
 Length of street segment = 800.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 38.450(CFS)
 Depth of flow = 0.553(Ft.), Average velocity = 3.670(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 3.67(Ft/s)
 Travel time = 3.63 min. TC = 17.32 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)

Rainfall intensity = 2.312(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) ($Q=KCIA$) is $C = 0.871$
 Subarea runoff = 42.588(CFS) for 22.000(Ac.)
 Total runoff = 55.405(CFS)
 Effective area this stream = 27.50(Ac.)
 Total Study Area (Main Stream No. 1) = 176.59(Ac.)
 Area averaged F_m value = 0.073(In/Hr)
 Street flow at end of street = 55.405(CFS)
 Half street flow at end of street = 27.703(CFS)
 Depth of flow = 0.618(Ft.), Average velocity = 4.242(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000(Ft.)

++++++
 Process from Point/Station 135.000 to Point/Station 135.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3

Stream flow area = 27.500(Ac.)
 Runoff from this stream = 55.405(CFS)
 Time of concentration = 17.32 min.
 Rainfall intensity = 2.312(In/Hr)
 Area averaged loss rate (F_m) = 0.0734(In/Hr)
 Area averaged Pervious ratio (A_p) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	259.305	20.18	2.110
2	35.655	18.42	2.228
3	55.405	17.32	2.312
$Q_{max}(1) =$ $1.000 * 1.000 * 259.305) +$ $0.945 * 1.000 * 35.655) +$ $0.910 * 1.000 * 55.405) + = 343.395$			
$Q_{max}(2) =$ $1.059 * 0.913 * 259.305) +$ $1.000 * 1.000 * 35.655) +$ $0.962 * 1.000 * 55.405) + = 339.603$			
$Q_{max}(3) =$ $1.100 * 0.858 * 259.305) +$ $1.039 * 0.940 * 35.655) +$ $1.000 * 1.000 * 55.405) + = 335.124$			

Total of 3 streams to confluence:

Flow rates before confluence point:

259.305 35.655 55.405

Maximum flow rates at confluence using above data:

343.395 339.603 335.124

Area of streams before confluence:

125.149 17.500 27.500

Effective area values after confluence:

170.149 159.257 151.380

Results of confluence:

Total flow rate = 343.395(CFS)

Time of concentration = 20.180 min.

Effective stream area after confluence = 170.149(Ac.)

Stream Area average Pervious fraction(Ap) = 0.113
 Stream Area average soil loss rate(Fm) = 0.085(In/Hr)
 Study area (this main stream) = 170.15(Ac.)

+++++
 Process from Point/Station 56.000 to Point/Station 57.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1043.300(Ft.)
 Downstream point/station elevation = 1041.300(Ft.)
 Pipe length = 640.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 343.395(CFS)
 Given pipe size = 84.00(In.)
 Calculated individual pipe flow = 343.395(CFS)
 Normal flow depth in pipe = 66.09(In.)
 Flow top width inside pipe = 68.80(In.)
 Critical Depth = 58.60(In.)
 Pipe flow velocity = 10.57(Ft/s)
 Travel time through pipe = 1.01 min.
 Time of concentration (TC) = 21.19 min.

+++++
 Process from Point/Station 57.000 to Point/Station 57.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 170.149(Ac.)
 Runoff from this stream = 343.395(CFS)
 Time of concentration = 21.19 min.
 Rainfall intensity = 2.049(In/Hr)
 Area averaged loss rate (Fm) = 0.0854(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1128

+++++
 Process from Point/Station 136.000 to Point/Station 137.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1091.600(Ft.)
 Bottom (of initial area) elevation = 1086.600(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%)= 0.50
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.902 min.
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875
 Subarea runoff = 12.696(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

+++++
 Process from Point/Station 137.000 to Point/Station 138.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1086.600(Ft.)
 End of street segment elevation = 1074.600(Ft.)
 Length of street segment = 875.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 25.391(CFS)
 Depth of flow = 0.460(Ft.), Average velocity = 3.725(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 18.268(Ft.)
 Flow velocity = 3.72(Ft/s)
 Travel time = 3.92 min. TC = 17.82 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.273(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.871
 Subarea runoff = 19.972(CFS) for 11.000(Ac.)
 Total runoff = 32.668(CFS)
 Effective area this stream = 16.50(Ac.)
 Total Study Area (Main Stream No. 1) = 193.09(Ac.)
 Area averaged Fm value = 0.073(In/Hr)
 Street flow at end of street = 32.668(CFS)
 Half street flow at end of street = 16.334(CFS)
 Depth of flow = 0.497(Ft.), Average velocity = 3.974(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++
 Process from Point/Station 138.000 to Point/Station 57.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1067.600(Ft.)
 Downstream point/station elevation = 1041.300(Ft.)
 Pipe length = 1320.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 32.668(CFS)
 Given pipe size = 30.00(In.)
 Calculated individual pipe flow = 32.668(CFS)

Normal flow depth in pipe = 16.13(In.)
 Flow top width inside pipe = 29.92(In.)
 Critical Depth = 23.34(In.)
 Pipe flow velocity = 12.15(Ft/s)
 Travel time through pipe = 1.81 min.
 Time of concentration (TC) = 19.63 min.

++++++
 Process from Point/Station 57.000 to Point/Station 57.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 16.500(Ac.)
 Runoff from this stream = 32.668(CFS)
 Time of concentration = 19.63 min.
 Rainfall intensity = 2.145(In/Hr)
 Area averaged loss rate (Fm) = 0.0734(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

++++++
 Process from Point/Station 139.000 to Point/Station 140.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1074.700(Ft.)
 Bottom (of initial area) elevation = 1069.700(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.304) * [(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.902 min.
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875
 Subarea runoff = 12.696(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

++++++
 Process from Point/Station 140.000 to Point/Station 141.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1069.700(Ft.)
 End of street segment elevation = 1065.300(Ft.)
 Length of street segment = 875.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street

Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 25.391(CFS)
 Depth of flow = 0.530(Ft.), Average velocity = 2.657(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 2.66(Ft/s)
 Travel time = 5.49 min. TC = 19.39 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.161(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.869
 Subarea runoff = 18.301(CFS) for 11.000(Ac.)
 Total runoff = 30.997(CFS)
 Effective area this stream = 16.50(Ac.)
 Total Study Area (Main Stream No. 1) = 209.59(Ac.)
 Area averaged Fm value = 0.073(In/Hr)
 Street flow at end of street = 30.997(CFS)
 Half street flow at end of street = 15.498(CFS)
 Depth of flow = 0.561(Ft.), Average velocity = 2.876(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++
 Process from Point/Station 141.000 to Point/Station 141.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3

Stream flow area = 16.500(Ac.)
 Runoff from this stream = 30.997(CFS)
 Time of concentration = 19.39 min.
 Rainfall intensity = 2.161(In/Hr)
 Area averaged loss rate (Fm) = 0.0734(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	343.395	21.19	2.049
2	32.668	19.63	2.145
3	30.997	19.39	2.161
Qmax(1) =			
	1.000 *	1.000 *	343.395) +
	0.954 *	1.000 *	32.668) +
	0.946 *	1.000 *	30.997) + = 403.878

$Q_{max}(2) =$
 1.049 * 0.926 * 343.395) +
 1.000 * 1.000 * 32.668) +
 0.992 * 1.000 * 30.997) + = 397.121
 $Q_{max}(3) =$
 1.057 * 0.915 * 343.395) +
 1.008 * 0.988 * 32.668) +
 1.000 * 1.000 * 30.997) + = 395.682

Total of 3 streams to confluence:

Flow rates before confluence point:

343.395 32.668 30.997

Maximum flow rates at confluence using above data:

403.878 397.121 395.682

Area of streams before confluence:

170.149 16.500 16.500

Effective area values after confluence:

203.149 190.611 188.502

Results of confluence:

Total flow rate = 403.878(CFS)

Time of concentration = 21.190 min.

Effective stream area after confluence = 203.149(Ac.)

Stream Area average Pervious fraction(A_p) = 0.111

Stream Area average soil loss rate(F_m) = 0.083(In/Hr)

Study area (this main stream) = 203.15(Ac.)

++++++
 Process from Point/Station 57.000 to Point/Station 63.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1041.300(Ft.)
 Downstream point/station elevation = 1039.500(Ft.)
 Pipe length = 560.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 403.878(CFS)
 Given pipe size = 92.00(In.)
 Calculated individual pipe flow = 403.878(CFS)
 Normal flow depth in pipe = 66.66(In.)
 Flow top width inside pipe = 82.20(In.)
 Critical Depth = 62.03(In.)
 Pipe flow velocity = 11.27(Ft/s)
 Travel time through pipe = 0.83 min.
 Time of concentration (TC) = 22.02 min.
 End of computations, Total Study Area = 209.59 (Ac.)
 The following figures may
 be used for a unit hydrograph study of the same area.
 Note: These figures do not consider reduced effective area
 effects caused by confluences in the rational equation.

Area averaged pervious area fraction(A_p) = 0.111
 Area averaged SCS curve number = 53.8

LINE "DZ-1"

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
 Rational Hydrology Study Date: 01/13/05

FONTANA / LINE DZ-1 HYDROLOGY
 25 YEAR STORM
 JN 04339

Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 25.0
 10 Year storm 1 hour rainfall = 0.930(In.)
 100 Year storm 1 hour rainfall = 1.350(In.)
 Computed rainfall intensity:
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)
 Slope used for rainfall intensity curve b = 0.6000
 Soil antecedent moisture condition (AMC) = 2

 Process from Point/Station 300.000 to Point/Station 301.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1068.100(Ft.)
 Bottom (of initial area) elevation = 1063.100(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.902 min.
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875
 Subarea runoff = 11.541(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

 Process from Point/Station 301.000 to Point/Station 302.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1063.100(Ft.)
 End of street segment elevation = 1060.000(Ft.)
 Length of street segment = 620.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 28.277(CFS)
 Depth of flow = 0.703(Ft.), Average velocity = 3.027(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 1.81(Ft.)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 30.392(Ft.)
 Flow velocity = 3.03(Ft/s)
 Travel time = 3.41 min. TC = 17.32 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073(In/Hr)
 Rainfall intensity = 2.313(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.871
 Subarea runoff = 27.756(CFS) for 14.500(Ac.)
 Total runoff = 39.297(CFS)
 Effective area this stream = 19.50(Ac.)
 Total Study Area (Main Stream No. 1) = 19.50(Ac.)
 Area averaged Fm value = 0.073(In/Hr)
 Street flow at end of street = 39.297(CFS)
 Half street flow at end of street = 39.297(CFS)
 Depth of flow = 0.789(Ft.), Average velocity = 3.146(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 6.12(Ft.)
 Flow width (from curb towards crown) = 34.707(Ft.)

++++++
 Process from Point/Station 302.000 to Point/Station 65.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1055.000(Ft.)
 Downstream point/station elevation = 1051.700(Ft.)
 Pipe length = 660.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 39.297(CFS)
 Given pipe size = 36.00(In.)
 Calculated individual pipe flow = 39.297(CFS)
 Normal flow depth in pipe = 25.13(In.)
 Flow top width inside pipe = 33.06(In.)
 Critical Depth = 24.50(In.)
 Pipe flow velocity = 7.47(Ft/s)
 Travel time through pipe = 1.47 min.
 Time of concentration (TC) = 18.79 min.


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+++++
Process from Point/Station      65.000 to Point/Station      65.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 19.500(Ac.)
 Runoff from this stream = 39.297(CFS)
 Time of concentration = 18.79 min.
 Rainfall intensity = 2.202(In/Hr)
 Area averaged loss rate (Fm) = 0.0734(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

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+++++
Process from Point/Station      303.000 to Point/Station      304.000
**** INITIAL AREA EVALUATION ****

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RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1064.500(Ft.)
 Bottom (of initial area) elevation = 1060.000(Ft.)
 Difference in elevation = 4.500(Ft.)
 Slope = 0.00450 s(%)= 0.45
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 18.168 min.
 Rainfall intensity = 2.247(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.753
 Subarea runoff = 13.535(CFS)
 Total initial stream area = 8.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

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+++++
Process from Point/Station      304.000 to Point/Station      304.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 8.000(Ac.)
 Runoff from this stream = 13.535(CFS)
 Time of concentration = 18.17 min.
 Rainfall intensity = 2.247(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	39.297	18.79	2.202
2	13.535	18.17	2.247

$Q_{\max}(1) =$
 $1.000 * 1.000 * 39.297) +$
 $0.976 * 1.000 * 13.535) + = 52.509$
 $Q_{\max}(2) =$
 $1.021 * 0.967 * 39.297) +$
 $1.000 * 1.000 * 13.535) + = 52.334$

Total of 2 streams to confluence:

Flow rates before confluence point:

39.297 13.535

Maximum flow rates at confluence using above data:

52.509 52.334

Area of streams before confluence:

19.500 8.000

Effective area values after confluence:

27.500 26.856

Results of confluence:

Total flow rate = 52.509(CFS)

Time of concentration = 18.789 min.

Effective stream area after confluence = 27.500(Ac.)

Stream Area average Pervious fraction(A_p) = 0.216

Stream Area average soil loss rate(F_m) = 0.159(In/Hr)

Study area (this main stream) = 27.50(Ac.)

++++++
 Process from Point/Station 65.000 to Point/Station 66.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1051.700(Ft.)
 Downstream point/station elevation = 1048.400(Ft.)
 Pipe length = 660.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 52.509(CFS)
 Given pipe size = 48.00(In.)
 Calculated individual pipe flow = 52.509(CFS)
 Normal flow depth in pipe = 24.47(In.)
 Flow top width inside pipe = 47.99(In.)
 Critical Depth = 26.14(In.)
 Pipe flow velocity = 8.15(Ft/s)
 Travel time through pipe = 1.35 min.
 Time of concentration (TC) = 20.14 min.

++++++
 Process from Point/Station 66.000 to Point/Station 66.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 27.500(Ac.)
 Runoff from this stream = 52.509(CFS)
 Time of concentration = 20.14 min.
 Rainfall intensity = 2.112(In/Hr)
 Area averaged loss rate (F_m) = 0.1588(In/Hr)
 Area averaged Pervious ratio (A_p) = 0.2164

++++++
 Process from Point/Station 305.000 to Point/Station 306.000
 **** INITIAL AREA EVALUATION ****

SCHOOL subarea

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.6000 Max loss rate(Fm)= 0.440(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1062.000(Ft.)
 Bottom (of initial area) elevation = 1055.400(Ft.)
 Difference in elevation = 6.600(Ft.)
 Slope = 0.00660 s(%)= 0.66
 $TC = k(0.412)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.823 min.
 Rainfall intensity = 2.273(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.726
 Subarea runoff = 13.193(CFS)
 Total initial stream area = 8.000(Ac.)
 Pervious area fraction = 0.600
 Initial area Fm value = 0.440(In/Hr)

++++++
 Process from Point/Station 306.000 to Point/Station 306.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 8.000(Ac.)
 Runoff from this stream = 13.193(CFS)
 Time of concentration = 17.82 min.
 Rainfall intensity = 2.273(In/Hr)
 Area averaged loss rate (Fm) = 0.4404(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.6000

++++++
 Process from Point/Station 307.000 to Point/Station 308.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1070.100(Ft.)
 Bottom (of initial area) elevation = 1065.100(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%)= 0.50
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 8.588(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

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Process from Point/Station      308.000 to Point/Station      309.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

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Top of street segment elevation = 1065.100(Ft.)
End of street segment elevation = 1062.700(Ft.)
Length of street segment = 650.000(Ft.)
Height of curb above gutter flowline = 8.0(In.)
Width of half street (curb to crown) = 20.000(Ft.)
Distance from crown to crossfall grade break = 18.500(Ft.)
Slope from gutter to grade break (v/hz) = 0.020
Slope from grade break to crown (v/hz) = 0.020
Street flow is on [2] side(s) of the street
Distance from curb to property line = 10.000(Ft.)
Slope from curb to property line (v/hz) = 0.020
Gutter width = 1.500(Ft.)
Gutter hike from flowline = 1.500(In.)
Manning's N in gutter = 0.0150
Manning's N from gutter to grade break = 0.0150
Manning's N from grade break to crown = 0.0150
Estimated mean flow rate at midpoint of street = 17.176(CFS)
Depth of flow = 0.499(Ft.), Average velocity = 2.073(Ft/s)
Note: depth of flow exceeds top of street crown.
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width = 20.000(Ft.)
Flow velocity = 2.07(Ft/s)
Travel time = 5.23 min. TC = 23.02 min.
Adding area flow to street
RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 56.00
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
Rainfall intensity = 1.950(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method)(Q=KCIA) is C = 0.731
Subarea runoff = 12.777(CFS) for 10.000(Ac.)
Total runoff = 21.365(CFS)
Effective area this stream = 15.00(Ac.)
Total Study Area (Main Stream No. 1) = 50.50(Ac.)
Area averaged Fm value = 0.367(In/Hr)
Street flow at end of street = 21.365(CFS)
Half street flow at end of street = 10.682(CFS)
Depth of flow = 0.528(Ft.), Average velocity = 2.260(Ft/s)
Note: depth of flow exceeds top of street crown.
Flow width (from curb towards crown)= 20.000(Ft.)

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Process from Point/Station      309.000 to Point/Station      310.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

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Top of street segment elevation = 1062.700(Ft.)
End of street segment elevation = 1055.400(Ft.)
Length of street segment = 1450.000(Ft.)
Height of curb above gutter flowline = 8.0(In.)
Width of half street (curb to crown) = 20.000(Ft.)
Distance from crown to crossfall grade break = 18.500(Ft.)

```

Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 32.047(CFS)
 Depth of flow = 0.566(Ft.), Average velocity = 2.915(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 2.92(Ft/s)
 Travel time = 8.29 min. TC = 31.31 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 1.621(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.696
 Subarea runoff = 12.494(CFS) for 15.000(Ac.)
 Total runoff = 33.859(CFS)
 Effective area this stream = 30.00(Ac.)
 Total Study Area (Main Stream No. 1) = 65.50(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 33.859(CFS)
 Half street flow at end of street = 16.929(CFS)
 Depth of flow = 0.576(Ft.), Average velocity = 2.980(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++
 Process from Point/Station 310.000 to Point/Station 310.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 30.000(Ac.)
 Runoff from this stream = 33.859(CFS)
 Time of concentration = 31.31 min.
 Rainfall intensity = 1.621(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	52.509	20.14	2.112
2	13.193	17.82	2.273
3	33.859	31.31	1.621
Qmax(1) =			

	1.000 *	1.000 *	52.509) +	
	0.912 *	1.000 *	13.193) +	
	1.392 *	0.643 *	33.859) + =	94.859
Qmax(2) =				
	1.082 *	0.885 *	52.509) +	
	1.000 *	1.000 *	13.193) +	
	1.520 *	0.569 *	33.859) + =	92.783
Qmax(3) =				
	0.749 *	1.000 *	52.509) +	
	0.644 *	1.000 *	13.193) +	
	1.000 *	1.000 *	33.859) + =	81.665

Total of 3 streams to confluence:

Flow rates before confluence point:

52.509 13.193 33.859

Maximum flow rates at confluence using above data:

94.859 92.783 81.665

Area of streams before confluence:

27.500 8.000 30.000

Effective area values after confluence:

54.799 49.419 65.500

Results of confluence:

Total flow rate = 94.859(CFS)

Time of concentration = 20.139 min.

Effective stream area after confluence = 54.799(Ac.)

Stream Area average Pervious fraction(Ap) = 0.393

Stream Area average soil loss rate(Fm) = 0.289(In/Hr)

Study area (this main stream) = 65.50(Ac.)

+++++
 Process from Point/Station 66.000 to Point/Station 67.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1048.400(Ft.)
 Downstream point/station elevation = 1044.600(Ft.)
 Pipe length = 760.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 94.859(CFS)
 Given pipe size = 54.00(In.)
 Calculated individual pipe flow = 94.859(CFS)
 Normal flow depth in pipe = 32.72(In.)
 Flow top width inside pipe = 52.77(In.)
 Critical Depth = 34.30(In.)
 Pipe flow velocity = 9.41(Ft/s)
 Travel time through pipe = 1.35 min.
 Time of concentration (TC) = 21.49 min.

+++++
 Process from Point/Station 67.000 to Point/Station 67.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 54.799(Ac.)
 Runoff from this stream = 94.859(CFS)
 Time of concentration = 21.49 min.
 Rainfall intensity = 2.032(In/Hr)
 Area averaged loss rate (Fm) = 0.2885(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.3931

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+++++
Process from Point/Station      311.000 to Point/Station      312.000
**** INITIAL AREA EVALUATION ****

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RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 56.00
Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1062.400(Ft.)
Bottom (of initial area) elevation = 1057.400(Ft.)
Difference in elevation = 5.000(Ft.)
Slope = 0.00500 s(%)= 0.50
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 17.789 min.
Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
Subarea runoff = 13.741(CFS)
Total initial stream area = 8.000(Ac.)
Pervious area fraction = 0.500
Initial area Fm value = 0.367(In/Hr)

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Process from Point/Station      312.000 to Point/Station      313.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

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Top of street segment elevation = 1057.400(Ft.)
End of street segment elevation = 1052.600(Ft.)
Length of street segment = 960.000(Ft.)
Height of curb above gutter flowline = 8.0(In.)
Width of half street (curb to crown) = 20.000(Ft.)
Distance from crown to crossfall grade break = 18.500(Ft.)
Slope from gutter to grade break (v/hz) = 0.020
Slope from grade break to crown (v/hz) = 0.020
Street flow is on [2] side(s) of the street
Distance from curb to property line = 10.000(Ft.)
Slope from curb to property line (v/hz) = 0.020
Gutter width = 1.500(Ft.)
Gutter hike from flowline = 1.500(In.)
Manning's N in gutter = 0.0150
Manning's N from gutter to grade break = 0.0150
Manning's N from grade break to crown = 0.0150
Estimated mean flow rate at midpoint of street = 20.611(CFS)
Depth of flow = 0.502(Ft.), Average velocity = 2.442(Ft/s)
Note: depth of flow exceeds top of street crown.
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width = 20.000(Ft.)
Flow velocity = 2.44(Ft/s)
Travel time = 6.55 min.      TC = 24.34 min.
Adding area flow to street
SCHOOL subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 56.00

```

Pervious ratio(A_p) = 0.6000 Max loss rate(F_m) = 0.440(In/Hr)
 Rainfall intensity = 1.885(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) ($Q=KCIA$) is $C = 0.707$
 Subarea runoff = 7.592(CFS) for 8.000(Ac.)
 Total runoff = 21.333(CFS)
 Effective area this stream = 16.00(Ac.)
 Total Study Area (Main Stream No. 1) = 81.50(Ac.)
 Area averaged F_m value = 0.404(In/Hr)
 Street flow at end of street = 21.333(CFS)
 Half street flow at end of street = 10.666(CFS)
 Depth of flow = 0.507(Ft.), Average velocity = 2.475(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000(Ft.)

++++++
 Process from Point/Station 313.000 to Point/Station 313.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 16.000(Ac.)
 Runoff from this stream = 21.333(CFS)
 Time of concentration = 24.34 min.
 Rainfall intensity = 1.885(In/Hr)
 Area averaged loss rate (F_m) = 0.4037(In/Hr)
 Area averaged Pervious ratio (A_p) = 0.5500
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	94.859	21.49	2.032
2	21.333	24.34	1.885
Qmax(1) =			
	1.000 *	1.000 *	94.859) +
	1.099 *	0.883 *	21.333) + = 115.552
Qmax(2) =			
	0.916 *	1.000 *	94.859) +
	1.000 *	1.000 *	21.333) + = 108.212

Total of 2 streams to confluence:

Flow rates before confluence point:

94.859 21.333

Maximum flow rates at confluence using above data:

115.552 108.212

Area of streams before confluence:

54.799 16.000

Effective area values after confluence:

68.921 70.799

Results of confluence:

Total flow rate = 115.552(CFS)

Time of concentration = 21.485 min.

Effective stream area after confluence = 68.921(Ac.)

Stream Area average Pervious fraction(A_p) = 0.429

Stream Area average soil loss rate(F_m) = 0.315(In/Hr)

Study area (this main stream) = 70.80(Ac.)

+++++

Process from Point/Station 67.000 to Point/Station 68.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1044.600(Ft.)
 Downstream point/station elevation = 1040.800(Ft.)
 Pipe length = 760.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 115.552(CFS)
 Given pipe size = 60.00(In.)
 Calculated individual pipe flow = 115.552(CFS)
 Normal flow depth in pipe = 34.45(In.)
 Flow top width inside pipe = 59.34(In.)
 Critical Depth = 36.80(In.)
 Pipe flow velocity = 9.91(Ft/s)
 Travel time through pipe = 1.28 min.
 Time of concentration (TC) = 22.76 min.

+++++
 Process from Point/Station 68.000 to Point/Station 68.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
 Effective stream flow area = 68.921(Ac.)
 Total study area this main stream = 81.500(Ac.)
 Runoff from this stream = 115.552(CFS)
 Time of concentration = 22.76 min.
 Rainfall intensity = 1.962(In/Hr)
 Area averaged loss rate (Fm) = 0.3146(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.4286
 Program is now starting with Main Stream No. 2

+++++
 Process from Point/Station 314.000 to Point/Station 315.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1079.500(Ft.)
 Bottom (of initial area) elevation = 1074.500(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%)= 0.50
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 8.588(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

+++++

Process from Point/Station 315.000 to Point/Station 318.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1074.500(Ft.)
 End of street segment elevation = 1069.500(Ft.)
 Length of street segment = 1000.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 15.888(CFS)
 Depth of flow = 0.465(Ft.), Average velocity = 2.269(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 18.520(Ft.)
 Flow velocity = 2.27(Ft/s)
 Travel time = 7.35 min. TC = 25.13 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 1.849(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.721
 Subarea runoff = 9.421(CFS) for 8.500(Ac.)
 Total runoff = 18.009(CFS)
 Effective area this stream = 13.50(Ac.)
 Total Study Area (Main Stream No. 2) = 13.50(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 18.009(CFS)
 Half street flow at end of street = 9.005(CFS)
 Depth of flow = 0.484(Ft.), Average velocity = 2.340(Ft/s)
 Flow width (from curb towards crown)= 19.433(Ft.)

+++++
 Process from Point/Station 318.000 to Point/Station 318.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
 Stream flow area = 13.500(Ac.)
 Runoff from this stream = 18.009(CFS)
 Time of concentration = 25.13 min.
 Rainfall intensity = 1.849(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000

+++++

Process from Point/Station 316.000 to Point/Station 317.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1079.500(Ft.)
 Bottom (of initial area) elevation = 1074.500(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 8.588(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

+++++
 Process from Point/Station 317.000 to Point/Station 318.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1074.500(Ft.)
 End of street segment elevation = 1069.500(Ft.)
 Length of street segment = 1000.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 16.317(CFS)
 Depth of flow = 0.469(Ft.), Average velocity = 2.284(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 18.711(Ft.)
 Flow velocity = 2.28(Ft/s)
 Travel time = 7.30 min. TC = 25.09 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 1.851(In/Hr) for a 25.0 year storm

Effective runoff coefficient used for area, (total area with modified rational method) ($Q=KCIA$) is $C = 0.722$
 Subarea runoff = 10.115(CFS) for 9.000(Ac.)
 Total runoff = 18.703(CFS)
 Effective area this stream = 14.00(Ac.)
 Total Study Area (Main Stream No. 2) = 27.50(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 18.703(CFS)
 Half street flow at end of street = 9.351(CFS)
 Depth of flow = 0.489(Ft.), Average velocity = 2.362(Ft/s)
 Flow width (from curb towards crown) = 19.717(Ft.)

+++++
 Process from Point/Station 318.000 to Point/Station 318.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 14.000(Ac.)
 Runoff from this stream = 18.703(CFS)
 Time of concentration = 25.09 min.
 Rainfall intensity = 1.851(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	18.009	25.13	1.849
2	18.703	25.09	1.851
Qmax(1) =			
	1.000 *	1.000 *	18.009) +
	0.999 *	1.000 *	18.703) + = 36.685
Qmax(2) =			
	1.001 *	0.998 *	18.009) +
	1.000 *	1.000 *	18.703) + = 36.703

Total of 2 streams to confluence:
 Flow rates before confluence point:
 18.009 18.703

Maximum flow rates at confluence using above data:
 36.685 36.703

Area of streams before confluence:
 13.500 14.000

Effective area values after confluence:
 27.500 27.474

Results of confluence:

Total flow rate = 36.703(CFS)
 Time of concentration = 25.087 min.
 Effective stream area after confluence = 27.474(Ac.)
 Stream Area average Pervious fraction(Ap) = 0.500
 Stream Area average soil loss rate(Fm) = 0.367(In/Hr)
 Study area (this main stream) = 27.50(Ac.)

+++++
 Process from Point/Station 318.000 to Point/Station 319.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1069.500(Ft.)
 End of street segment elevation = 1063.000(Ft.)
 Length of street segment = 1300.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 49.061(CFS)
 Depth of flow = 0.648(Ft.), Average velocity = 3.444(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 3.44(Ft/s)
 Travel time = 6.29 min. TC = 31.38 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367(In/Hr)
 Rainfall intensity = 1.619(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.696
 Subarea runoff = 15.091(CFS) for 18.500(Ac.)
 Total runoff = 51.795(CFS)
 Effective area this stream = 45.97(Ac.)
 Total Study Area (Main Stream No. 2) = 46.00(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 51.795(CFS)
 Half street flow at end of street = 25.897(CFS)
 Depth of flow = 0.659(Ft.), Average velocity = 3.519(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000(Ft.)

++++++
 Process from Point/Station 319.000 to Point/Station 68.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1054.800(Ft.)
 Downstream point/station elevation = 1041.800(Ft.)
 Pipe length = 900.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 51.795(CFS)
 Given pipe size = 48.00(In.)
 Calculated individual pipe flow = 51.795(CFS)
 Normal flow depth in pipe = 18.02(In.)
 Flow top width inside pipe = 46.49(In.)
 Critical Depth = 25.91(In.)
 Pipe flow velocity = 12.01(Ft/s)
 Travel time through pipe = 1.25 min.

Time of concentration (TC) = 32.63 min.

+++++
 Process from Point/Station 68.000 to Point/Station 68.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Effective stream flow area = 45.974 (Ac.)
 Total study area this main stream = 46.000 (Ac.)
 Runoff from this stream = 51.795 (CFS)
 Time of concentration = 32.63 min.
 Rainfall intensity = 1.581 (In/Hr)
 Area averaged loss rate (Fm) = 0.3670 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	115.552	22.76	1.962
2	51.795	32.63	1.581

Qmax(1) =
 1.000 * 1.000 * 115.552) +
 1.314 * 0.698 * 51.795) + = 163.034
 Qmax(2) =
 0.769 * 1.000 * 115.552) +
 1.000 * 1.000 * 51.795) + = 140.618

Total of 2 main streams to confluence:

Flow rates before confluence point:

116.552 52.795

Maximum flow rates at confluence using above data:

163.034 140.618

Effective Area of streams before confluence:

68.921 45.974

Effective area values after confluence:

100.998 114.895

Results of confluence:

Total flow rate = 163.034 (CFS)

Time of concentration = 22.764 min.

Effective stream area after confluence = 100.998 (Ac.)

Stream Area average Pervious fraction (Ap) = 0.457

Stream Area average soil loss rate (Fm) = 0.336 (In/Hr)

Stream effective area = 114.90 (Ac.)

+++++
 Process from Point/Station 68.000 to Point/Station 68.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 100.998 (Ac.)

Runoff from this stream = 163.034 (CFS)

Time of concentration = 22.76 min.

Rainfall intensity = 1.962 (In/Hr)

Area averaged loss rate (Fm) = 0.3355 (In/Hr)

Area averaged Pervious ratio (Ap) = 0.4572

+++++
 Process from Point/Station 320.000 to Point/Station 321.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1057.100(Ft.)
 Bottom (of initial area) elevation = 1052.100(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%)= 0.50
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 11.164(CFS)
 Total initial stream area = 6.500(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

+++++
 Process from Point/Station 321.000 to Point/Station 321.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 6.500(Ac.)
 Runoff from this stream = 11.164(CFS)
 Time of concentration = 17.79 min.
 Rainfall intensity = 2.275(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000

+++++
 Process from Point/Station 322.000 to Point/Station 323.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1057.100(Ft.)
 Bottom (of initial area) elevation = 1052.100(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%)= 0.50
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$

Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 8.588(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

+++++
 Process from Point/Station 323.000 to Point/Station 323.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3

Stream flow area = 5.000(Ac.)
 Runoff from this stream = 8.588(CFS)
 Time of concentration = 17.79 min.
 Rainfall intensity = 2.275(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	163.034	22.76	1.962
2	11.164	17.79	2.275
3	8.588	17.79	2.275
Qmax(1) =			
	1.000 *	1.000 *	163.034) +
	0.836 *	1.000 *	11.164) +
	0.836 *	1.000 *	8.588) + = 179.547
Qmax(2) =			
	1.192 *	0.781 *	163.034) +
	1.000 *	1.000 *	11.164) +
	1.000 *	1.000 *	8.588) + = 171.663
Qmax(3) =			
	1.192 *	0.781 *	163.034) +
	1.000 *	1.000 *	11.164) +
	1.000 *	1.000 *	8.588) + = 171.663

Total of 3 streams to confluence:
 Flow rates before confluence point:
 163.034 11.164 8.588
 Maximum flow rates at confluence using above data:
 179.547 171.663 171.663
 Area of streams before confluence:
 100.998 6.500 5.000
 Effective area values after confluence:
 112.498 90.426 90.426
 Results of confluence:
 Total flow rate = 179.547(CFS)
 Time of concentration = 22.764 min.
 Effective stream area after confluence = 112.498(Ac.)
 Stream Area average Pervious fraction(Ap) = 0.462
 Stream Area average soil loss rate(Fm) = 0.339(In/Hr)
 Study area (this main stream) = 112.50(Ac.)

+++++

Process from Point/Station 68.000 to Point/Station 69.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1040.800(Ft.)
 Downstream point/station elevation = 1038.800(Ft.)
 Pipe length = 400.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 179.547(CFS)
 Given pipe size = 84.00(In.)
 Calculated individual pipe flow = 179.547(CFS)
 Normal flow depth in pipe = 36.80(In.)
 Flow top width inside pipe = 83.35(In.)
 Critical Depth = 41.80(In.)
 Pipe flow velocity = 11.06(Ft/s)
 Travel time through pipe = 0.60 min.
 Time of concentration (TC) = 23.37 min.

+++++
 Process from Point/Station 69.000 to Point/Station 69.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 112.498(Ac.)
 Runoff from this stream = 179.547(CFS)
 Time of concentration = 23.37 min.
 Rainfall intensity = 1.932(In/Hr)
 Area averaged loss rate (Fm) = 0.3387(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.4615

+++++
 Process from Point/Station 324.000 to Point/Station 325.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1055.000(Ft.)
 Bottom (of initial area) elevation = 1050.000(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 13.741(CFS)
 Total initial stream area = 8.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

+++++
 Process from Point/Station 325.000 to Point/Station 325.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 8.000(Ac.)
 Runoff from this stream = 13.741(CFS)
 Time of concentration = 17.79 min.
 Rainfall intensity = 2.275(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000

+++++
 Process from Point/Station 326.000 to Point/Station 327.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1055.000(Ft.)
 Bottom (of initial area) elevation = 1050.000(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%)= 0.50
 $TC = k(0.389) * [(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 12.023(CFS)
 Total initial stream area = 7.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

+++++
 Process from Point/Station 327.000 to Point/Station 327.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 7.000(Ac.)
 Runoff from this stream = 12.023(CFS)
 Time of concentration = 17.79 min.
 Rainfall intensity = 2.275(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	179.547	23.37	1.932
2	13.741	17.79	2.275
3	12.023	17.79	2.275

Qmax(1) =
 $1.000 * 1.000 * 179.547) +$
 $0.820 * 1.000 * 13.741) +$
 $0.820 * 1.000 * 12.023) + = 200.674$

Qmax(2) =

1.216 * 0.761 * 179.547) +
 1.000 * 1.000 * 13.741) +
 1.000 * 1.000 * 12.023) + = 191.922
 Qmax(3) =
 1.216 * 0.761 * 179.547) +
 1.000 * 1.000 * 13.741) +
 1.000 * 1.000 * 12.023) + = 191.922

Total of 3 streams to confluence:

Flow rates before confluence point:

179.547 13.741 12.023

Maximum flow rates at confluence using above data:

200.674 191.922 191.922

Area of streams before confluence:

112.498 8.000 7.000

Effective area values after confluence:

127.498 100.646 100.646

Results of confluence:

Total flow rate = 200.674(CFS)

Time of concentration = 23.366 min.

Effective stream area after confluence = 127.498(Ac.)

Stream Area average Pervious fraction(Ap) = 0.466

Stream Area average soil loss rate(Fm) = 0.342(In/Hr)

Study area (this main stream) = 127.50(Ac.)

++++++
 Process from Point/Station 69.000 to Point/Station 70.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1038.800(Ft.)
 Downstream point/station elevation = 1034.600(Ft.)
 Pipe length = 880.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 200.674(CFS)
 Given pipe size = 96.00(In.)
 Calculated individual pipe flow = 200.674(CFS)
 Normal flow depth in pipe = 37.22(In.)
 Flow top width inside pipe = 93.55(In.)
 Critical Depth = 42.53(In.)
 Pipe flow velocity = 11.14(Ft/s)
 Travel time through pipe = 1.32 min.
 Time of concentration (TC) = 24.68 min.

++++++
 Process from Point/Station 70.000 to Point/Station 70.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 127.498(Ac.)
 Runoff from this stream = 200.674(CFS)
 Time of concentration = 24.68 min.
 Rainfall intensity = 1.869(In/Hr)
 Area averaged loss rate (Fm) = 0.3421(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.4661

++++++
 Process from Point/Station 328.000 to Point/Station 329.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1057.800(Ft.)
 Bottom (of initial area) elevation = 1052.800(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 8.588(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

++++++
 Process from Point/Station 329.000 to Point/Station 330.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1052.800(Ft.)
 End of street segment elevation = 1048.800(Ft.)
 Length of street segment = 800.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 18.893(CFS)
 Depth of flow = 0.491(Ft.), Average velocity = 2.368(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 19.793(Ft.)
 Flow velocity = 2.37(Ft/s)
 Travel time = 5.63 min. TC = 23.42 min.

Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 1.929(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.729
 Subarea runoff = 15.316(CFS) for 12.000(Ac.)

Total runoff = 23.904 (CFS)
 Effective area this stream = 17.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 89.50 (Ac.)
 Area averaged Fm value = 0.367 (In/Hr)
 Street flow at end of street = 23.904 (CFS)
 Half street flow at end of street = 11.952 (CFS)
 Depth of flow = 0.522 (Ft.), Average velocity = 2.590 (Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000 (Ft.)

++++++
 Process from Point/Station 330.000 to Point/Station 331.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1048.800 (Ft.)
 End of street segment elevation = 1045.500 (Ft.)
 Length of street segment = 660.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 20.000 (Ft.)
 Distance from crown to crossfall grade break = 18.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500 (Ft.)
 Gutter hike from flowline = 1.500 (In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 35.856 (CFS)
 Depth of flow = 0.586 (Ft.), Average velocity = 3.042 (Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000 (Ft.)
 Flow velocity = 3.04 (Ft/s)
 Travel time = 3.62 min. TC = 27.04 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367 (In/Hr)
 Rainfall intensity = 1.770 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.713
 Subarea runoff = 19.031 (CFS) for 17.000 (Ac.)
 Total runoff = 42.935 (CFS)
 Effective area this stream = 34.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 106.50 (Ac.)
 Area averaged Fm value = 0.367 (In/Hr)
 Street flow at end of street = 42.935 (CFS)
 Half street flow at end of street = 21.467 (CFS)
 Depth of flow = 0.620 (Ft.), Average velocity = 3.267 (Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000 (Ft.)

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Process from Point/Station      331.000 to Point/Station      70.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****

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Upstream point/station elevation = 1038.600(Ft.)
Downstream point/station elevation = 1034.600(Ft.)
Pipe length = 800.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 42.935(CFS)
Given pipe size = 42.00(In.)
Calculated individual pipe flow = 42.935(CFS)
Normal flow depth in pipe = 23.53(In.)
Flow top width inside pipe = 41.69(In.)
Critical Depth = 24.51(In.)
Pipe flow velocity = 7.74(Ft/s)
Travel time through pipe = 1.72 min.
Time of concentration (TC) = 28.76 min.

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Process from Point/Station      70.000 to Point/Station      70.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 2
Stream flow area = 34.000(Ac.)
Runoff from this stream = 42.935(CFS)
Time of concentration = 28.76 min.
Rainfall intensity = 1.706(In/Hr)
Area averaged loss rate (Fm) = 0.3670(In/Hr)
Area averaged Pervious ratio (Ap) = 0.5000

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Process from Point/Station      332.000 to Point/Station      333.000
**** INITIAL AREA EVALUATION ****

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RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 56.00
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1053.200(Ft.)
Bottom (of initial area) elevation = 1048.200(Ft.)
Difference in elevation = 5.000(Ft.)
Slope = 0.00500 s(%)= 0.50
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 17.789 min.
Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
Subarea runoff = 8.588(CFS)
Total initial stream area = 5.000(Ac.)
Pervious area fraction = 0.500
Initial area Fm value = 0.367(In/Hr)

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Process from Point/Station      333.000 to Point/Station      334.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

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Top of street segment elevation = 1048.200(Ft.)
 End of street segment elevation = 1045.600(Ft.)
 Length of street segment = 520.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 15.458(CFS)
 Depth of flow = 0.462(Ft.), Average velocity = 2.254(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 18.326(Ft.)
 Flow velocity = 2.25(Ft/s)
 Travel time = 3.85 min. TC = 21.63 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 2.023(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area,(total area with modified
 rational method)(Q=KCIA) is C = 0.737
 Subarea runoff = 10.791(CFS) for 8.000(Ac.)
 Total runoff = 19.379(CFS)
 Effective area this stream = 13.00(Ac.)
 Total Study Area (Main Stream No. 1) = 119.50(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 19.379(CFS)
 Half street flow at end of street = 9.689(CFS)
 Depth of flow = 0.495(Ft.), Average velocity = 2.383(Ft/s)
 Flow width (from curb towards crown)= 19.986(Ft.)

++++++
 Process from Point/Station 334.000 to Point/Station 334.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 13.000(Ac.)
 Runoff from this stream = 19.379(CFS)
 Time of concentration = 21.63 min.
 Rainfall intensity = 2.023(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000

++++++
 Process from Point/Station 335.000 to Point/Station 336.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1053.200(Ft.)
 Bottom (of initial area) elevation = 1048.200(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%)= 0.50
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 10.306(CFS)
 Total initial stream area = 6.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

++++++
 Process from Point/Station 336.000 to Point/Station 337.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1048.200(Ft.)
 End of street segment elevation = 1045.600(Ft.)
 Length of street segment = 520.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 21.470(CFS)
 Depth of flow = 0.508(Ft.), Average velocity = 2.482(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 2.48(Ft/s)
 Travel time = 3.49 min. TC = 21.28 min.
 Adding area flow to street

RESIDENTIAL(5 - 7 dwl/acre)

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 2.043(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified

rational method) ($Q=KCIA$) is $C = 0.738$
 Subarea runoff = 18.361(CFS) for 13.000(Ac.)
 Total runoff = 28.667(CFS)
 Effective area this stream = 19.00(Ac.)
 Total Study Area (Main Stream No. 1) = 138.50(Ac.)
 Area averaged F_m value = 0.367(In/Hr)
 Street flow at end of street = 28.667(CFS)
 Half street flow at end of street = 14.333(CFS)
 Depth of flow = 0.549(Ft.), Average velocity = 2.783(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000(Ft.)

+++++
 Process from Point/Station 337.000 to Point/Station 337.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 4

Stream flow area = 19.000(Ac.)
 Runoff from this stream = 28.667(CFS)
 Time of concentration = 21.28 min.
 Rainfall intensity = 2.043(In/Hr)
 Area averaged loss rate (F_m) = 0.3670(In/Hr)
 Area averaged Pervious ratio (A_p) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	200.674	24.68	1.869
2	42.935	28.76	1.706
3	19.379	21.63	2.023
4	28.667	21.28	2.043
Qmax(1) =			
	1.000 *	1.000 *	200.674) +
	1.122 *	0.858 *	42.935) +
	0.907 *	1.000 *	19.379) +
	0.896 *	1.000 *	28.667) + = 285.304
Qmax(2) =			
	0.893 *	1.000 *	200.674) +
	1.000 *	1.000 *	42.935) +
	0.808 *	1.000 *	19.379) +
	0.799 *	1.000 *	28.667) + = 260.649
Qmax(3) =			
	1.101 *	0.876 *	200.674) +
	1.237 *	0.752 *	42.935) +
	1.000 *	1.000 *	19.379) +
	0.988 *	1.000 *	28.667) + = 281.275
Qmax(4) =			
	1.114 *	0.862 *	200.674) +
	1.252 *	0.740 *	42.935) +
	1.012 *	0.984 *	19.379) +
	1.000 *	1.000 *	28.667) + = 280.471

Total of 4 streams to confluence:

Flow rates before confluence point:
 200.674 42.935 19.379 28.667
 Maximum flow rates at confluence using above data:
 285.304 260.649 281.275 280.471
 Area of streams before confluence:

127.498	34.000	13.000	19.000
Effective area values after confluence:			
188.681	193.498	169.329	166.874

Results of confluence:

Total flow rate = 285.304 (CFS)
 Time of concentration = 24.684 min.
 Effective stream area after confluence = 188.681 (Ac.)
 Stream Area average Pervious fraction (Ap) = 0.478
 Stream Area average soil loss rate (Fm) = 0.351 (In/Hr)
 Study area (this main stream) = 193.50 (Ac.)

+++++
 Process from Point/Station 70.000 to Point/Station 71.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1034.600 (Ft.)
 Downstream point/station elevation = 1030.600 (Ft.)
 Pipe length = 800.00 (Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 285.304 (CFS)
 Given pipe size = 102.00 (In.)
 Calculated individual pipe flow = 285.304 (CFS)
 Normal flow depth in pipe = 43.36 (In.)
 Flow top width inside pipe = 100.85 (In.)
 Critical Depth = 50.20 (In.)
 Pipe flow velocity = 12.41 (Ft/s)
 Travel time through pipe = 1.07 min.
 Time of concentration (TC) = 25.76 min.

+++++
 Process from Point/Station 71.000 to Point/Station 71.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 188.681 (Ac.)
 Runoff from this stream = 285.304 (CFS)
 Time of concentration = 25.76 min.
 Rainfall intensity = 1.822 (In/Hr)
 Area averaged loss rate (Fm) = 0.3506 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.4776

+++++
 Process from Point/Station 338.000 to Point/Station 339.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 56.00
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.073 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000 (Ft.)
 Top (of initial area) elevation = 1056.000 (Ft.)
 Bottom (of initial area) elevation = 1051.000 (Ft.)
 Difference in elevation = 5.000 (Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$

Initial area time of concentration = 13.902 min.
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875
 Subarea runoff = 11.541(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

+++++
 Process from Point/Station 339.000 to Point/Station 340.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1051.000(Ft.)
 End of street segment elevation = 1048.600(Ft.)
 Length of street segment = 480.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 21.929(CFS)
 Depth of flow = 0.511(Ft.), Average velocity = 2.503(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 2.50(Ft/s)
 Travel time = 3.20 min. TC = 17.10 min.
 Adding area flow to street

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.330(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.872
 Subarea runoff = 16.893(CFS) for 9.000(Ac.)
 Total runoff = 28.434(CFS)
 Effective area this stream = 14.00(Ac.)
 Total Study Area (Main Stream No. 1) = 152.50(Ac.)
 Area averaged Fm value = 0.073(In/Hr)
 Street flow at end of street = 28.434(CFS)
 Half street flow at end of street = 14.217(CFS)
 Depth of flow = 0.548(Ft.), Average velocity = 2.775(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++
 Process from Point/Station 340.000 to Point/Station 340.000

**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 14.000 (Ac.)

Runoff from this stream = 28.434 (CFS)

Time of concentration = 17.10 min.

Rainfall intensity = 2.330 (In/Hr)

Area averaged loss rate (Fm) = 0.0734 (In/Hr)

Area averaged Pervious ratio (Ap) = 0.1000

Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	285.304	25.76	1.822
---	---------	-------	-------

2	28.434	17.10	2.330
---	--------	-------	-------

Qmax(1) =

1.000 * 1.000 * 285.304) +
0.775 * 1.000 * 28.434) + = 307.340

Qmax(2) =

1.345 * 0.664 * 285.304) +
1.000 * 1.000 * 28.434) + = 283.184

Total of 2 streams to confluence:

Flow rates before confluence point:

285.304 28.434

Maximum flow rates at confluence using above data:

307.340 283.184

Area of streams before confluence:

188.681 14.000

Effective area values after confluence:

202.681 139.253

Results of confluence:

Total flow rate = 307.340 (CFS)

Time of concentration = 25.758 min.

Effective stream area after confluence = 202.681 (Ac.)

Stream Area average Pervious fraction (Ap) = 0.452

Stream Area average soil loss rate (Fm) = 0.331 (In/Hr)

Study area (this main stream) = 202.68 (Ac.)

End of computations, Total Study Area = 234.00 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction (Ap) = 0.450

Area averaged SCS curve number = 56.0

LINE "P3"

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
 Rational Hydrology Study Date: 01/13/05

FONTANA / LINE P3 HYDROLOGY
 25 YEAR STORM
 JN 04339

Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 25.0
 10 Year storm 1 hour rainfall = 0.930(In.)
 100 Year storm 1 hour rainfall = 1.350(In.)
 Computed rainfall intensity:
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)
 Slope used for rainfall intensity curve b = 0.6000
 Soil antecedent moisture condition (AMC) = 2

+++++
 Process from Point/Station 409.000 to Point/Station 410.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1860.000(Ft.)
 Bottom (of initial area) elevation = 1460.000(Ft.)
 Difference in elevation = 400.000(Ft.)
 Slope = 0.40000 s(%)= 40.00
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.994 min.
 Rainfall intensity = 3.216(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.787
 Subarea runoff = 18.984(CFS)
 Total initial stream area = 7.500(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

+++++
 Process from Point/Station 410.000 to Point/Station 411.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 42.397(CFS)
 Depth of flow = 0.229(Ft.), Average velocity = 9.149(Ft/s)
 ***** Irregular Channel Data *****

```

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              20.00
      2              20.00              0.00
      3              40.00              0.00
      4              60.00              20.00
Manning's 'N' friction factor = 0.035
-----

```

```

Sub-Channel flow = 42.397(CFS)
'      ' flow top width = 20.458(Ft.)
'      ' velocity = 9.149(Ft/s)
'      ' area = 4.634(Sq.Ft)
'      ' Froude number = 3.387

```

```

Upstream point elevation = 1460.000(Ft.)
Downstream point elevation = 1300.000(Ft.)
Flow length = 470.000(Ft.)
Travel time = 0.86 min.
Time of concentration = 10.85 min.
Depth of flow = 0.229(Ft.)
Average velocity = 9.149(Ft/s)
Total irregular channel flow = 42.397(CFS)
Irregular channel normal depth above invert elev. = 0.229(Ft.)
Average velocity of channel(s) = 9.149(Ft/s)

```

```

Sub-Channel No. 1 Critical depth = 0.516(Ft.)
'      '      ' Critical flow top width = 21.031(Ft.)
'      '      ' Critical flow velocity = 4.008(Ft/s)
'      '      ' Critical flow area = 10.578(Sq.Ft)

```

```

Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404(In/Hr)
Rainfall intensity = 3.061(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.781
Subarea runoff = 43.205(CFS) for 18.500(Ac.)
Total runoff = 62.188(CFS)
Effective area this stream = 26.00(Ac.)
Total Study Area (Main Stream No. 1) = 26.00(Ac.)
Area averaged Fm value = 0.404(In/Hr)

```

```

+++++
Process from Point/Station 411.000 to Point/Station 412.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

```

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-----
Estimated mean flow rate at midpoint of channel = 86.107(CFS)
Depth of flow = 0.421(Ft.), Average velocity = 10.005(Ft/s)
***** Irregular Channel Data *****
-----

```

```

Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              20.00
      2              20.00              0.00

```

3	40.00	0.00
4	60.00	20.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 86.107 (CFS)
 ' ' flow top width = 20.843 (Ft.)
 ' ' velocity = 10.005 (Ft/s)
 ' ' area = 8.607 (Sq.Ft)
 ' ' Froude number = 2.744

Upstream point elevation = 1300.000 (Ft.)
 Downstream point elevation = 1180.000 (Ft.)
 Flow length = 650.000 (Ft.)
 Travel time = 1.08 min.
 Time of concentration = 11.93 min.
 Depth of flow = 0.421 (Ft.)
 Average velocity = 10.005 (Ft/s)
 Total irregular channel flow = 86.107 (CFS)
 Irregular channel normal depth above invert elev. = 0.421 (Ft.)
 Average velocity of channel(s) = 10.005 (Ft/s)

Sub-Channel No. 1 Critical depth = 0.820 (Ft.)
 ' ' Critical flow top width = 21.641 (Ft.)
 ' ' Critical flow velocity = 5.042 (Ft/s)
 ' ' Critical flow area = 17.079 (Sq.Ft)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Rainfall intensity = 2.891 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.774
 Subarea runoff = 40.807 (CFS) for 20.000 (Ac.)
 Total runoff = 102.995 (CFS)
 Effective area this stream = 46.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 46.00 (Ac.)
 Area averaged Fm value = 0.404 (In/Hr)

+++++
 Process from Point/Station 412.000 to Point/Station 77.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1152.000 (Ft.)
 Downstream point/station elevation = 1122.500 (Ft.)
 Pipe length = 450.00 (Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 102.995 (CFS)
 Given pipe size = 30.00 (In.)
 Calculated individual pipe flow = 102.995 (CFS)
 Normal flow depth in pipe = 24.09 (In.)
 Flow top width inside pipe = 23.86 (In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 24.39 (Ft/s)
 Travel time through pipe = 0.31 min.
 Time of concentration (TC) = 12.24 min.


```

+++++
Process from Point/Station      77.000 to Point/Station      77.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 1

```

Stream flow area =      46.000(Ac.)
Runoff from this stream =    102.995(CFS)
Time of concentration =    12.24 min.
Rainfall intensity =      2.848(In/Hr)
Area averaged loss rate (Fm) =    0.4035(In/Hr)
Area averaged Pervious ratio (Ap) = 1.0000

```

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+++++
Process from Point/Station      413.000 to Point/Station      414.000
**** INITIAL AREA EVALUATION ****

```

RESIDENTIAL(5 - 7 dwl/acre)

```

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 56.00
Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)
Initial subarea data:
Initial area flow distance =    500.000(Ft.)
Top (of initial area) elevation = 1163.300(Ft.)
Bottom (of initial area) elevation = 1129.000(Ft.)
Difference in elevation =    34.300(Ft.)
Slope =    0.06860  s(%)=      6.86
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    7.985 min.
Rainfall intensity =      3.679(In/Hr) for a    25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.810
Subarea runoff =    13.416(CFS)
Total initial stream area =      4.500(Ac.)
Pervious area fraction = 0.500
Initial area Fm value =    0.367(In/Hr)

```

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+++++
Process from Point/Station      414.000 to Point/Station      414.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 2

```

Stream flow area =      4.500(Ac.)
Runoff from this stream =    13.416(CFS)
Time of concentration =    7.98 min.
Rainfall intensity =      3.679(In/Hr)
Area averaged loss rate (Fm) =    0.3670(In/Hr)
Area averaged Pervious ratio (Ap) = 0.5000
Summary of stream data:

```

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	102.995	12.24	2.848
2	13.416	7.98	3.679

Qmax(1) =

$$\begin{array}{rcl} 1.000 * & 1.000 * & 102.995) + \\ 0.749 * & 1.000 * & 13.416) + = & 113.041 \\ Q_{max}(2) = & & \\ 1.340 * & 0.652 * & 102.995) + \\ 1.000 * & 1.000 * & 13.416) + = & 103.473 \end{array}$$

Total of 2 streams to confluence:

Flow rates before confluence point:

102.995 13.416

Maximum flow rates at confluence using above data:

113.041 103.473

Area of streams before confluence:

46.000 4.500

Effective area values after confluence:

50.500 34.507

Results of confluence:

Total flow rate = 113.041(CFS)

Time of concentration = 12.241 min.

Effective stream area after confluence = 50.500(Ac.)

Stream Area average Pervious fraction(Ap) = 0.955

Stream Area average soil loss rate(Fm) = 0.400(In/Hr)

Study area (this main stream) = 50.50(Ac.)

++++++
 Process from Point/Station 77.000 to Point/Station 78.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1122.500(Ft.)
 Downstream point/station elevation = 1090.500(Ft.)
 Pipe length = 550.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 113.041(CFS)
 Given pipe size = 39.00(In.)
 Calculated individual pipe flow = 113.041(CFS)
 Normal flow depth in pipe = 21.05(In.)
 Flow top width inside pipe = 38.88(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 24.77(Ft/s)
 Travel time through pipe = 0.37 min.
 Time of concentration (TC) = 12.61 min.

++++++
 Process from Point/Station 78.000 to Point/Station 78.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 50.500(Ac.)
 Runoff from this stream = 113.041(CFS)
 Time of concentration = 12.61 min.
 Rainfall intensity = 2.797(In/Hr)
 Area averaged loss rate (Fm) = 0.4003(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.9554

++++++
 Process from Point/Station 415.000 to Point/Station 416.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 550.000(Ft.)
 Top (of initial area) elevation = 1129.000(Ft.)
 Bottom (of initial area) elevation = 1097.000(Ft.)
 Difference in elevation = 32.000(Ft.)
 Slope = 0.05818 s(%)= 5.82
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 8.573 min.
 Rainfall intensity = 3.526(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.806
 Subarea runoff = 19.901(CFS)
 Total initial stream area = 7.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

++++++
 Process from Point/Station 416.000 to Point/Station 416.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 7.000(Ac.)
 Runoff from this stream = 19.901(CFS)
 Time of concentration = 8.57 min.
 Rainfall intensity = 3.526(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000

++++++
 Process from Point/Station 417.000 to Point/Station 418.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 650.000(Ft.)
 Top (of initial area) elevation = 1420.000(Ft.)
 Bottom (of initial area) elevation = 1120.000(Ft.)
 Difference in elevation = 300.000(Ft.)
 Slope = 0.46154 s(%)= 46.15
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 8.175 min.
 Rainfall intensity = 3.628(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.800
 Subarea runoff = 29.020(CFS)
 Total initial stream area = 10.000(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

+++++
 Process from Point/Station 418.000 to Point/Station 418.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3

Stream flow area = 10.000(Ac.)
 Runoff from this stream = 29.020(CFS)
 Time of concentration = 8.17 min.
 Rainfall intensity = 3.628(In/Hr)
 Area averaged loss rate (Fm) = 0.4035(In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	113.041	12.61	2.797
2	19.901	8.57	3.526
3	29.020	8.17	3.628

Qmax(1) =
 1.000 * 1.000 * 113.041) +
 0.769 * 1.000 * 19.901) +
 0.742 * 1.000 * 29.020) + = 149.893

Qmax(2) =
 1.304 * 0.680 * 113.041) +
 1.000 * 1.000 * 19.901) +
 0.968 * 1.000 * 29.020) + = 148.217

Qmax(3) =
 1.347 * 0.648 * 113.041) +
 1.032 * 0.954 * 19.901) +
 1.000 * 1.000 * 29.020) + = 147.290

Total of 3 streams to confluence:

Flow rates before confluence point:

113.041 19.901 29.020

Maximum flow rates at confluence using above data:

149.893 148.217 147.290

Area of streams before confluence:

50.500 7.000 10.000

Effective area values after confluence:

67.500 51.331 49.411

Results of confluence:

Total flow rate = 149.893(CFS)

Time of concentration = 12.611 min.

Effective stream area after confluence = 67.500(Ac.)

Stream Area average Pervious fraction(Ap) = 0.915

Stream Area average soil loss rate(Fm) = 0.397(In/Hr)

Study area (this main stream) = 67.50(Ac.)

+++++
 Process from Point/Station 78.000 to Point/Station 79.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1090.500(Ft.)

Downstream point/station elevation = 1060.200(Ft.)

Pipe length = 900.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 149.893(CFS)

Given pipe size = 48.00(In.)

Calculated individual pipe flow = 149.893(CFS)

Normal flow depth in pipe = 25.92(In.)
 Flow top width inside pipe = 47.85(In.)
 Critical Depth = 43.16(In.)
 Pipe flow velocity = 21.64(Ft/s)
 Travel time through pipe = 0.69 min.
 Time of concentration (TC) = 13.30 min.

++++++
 Process from Point/Station 79.000 to Point/Station 79.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 67.500(Ac.)
 Runoff from this stream = 149.893(CFS)
 Time of concentration = 13.30 min.
 Rainfall intensity = 2.709(In/Hr)
 Area averaged loss rate (Fm) = 0.3973(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.9148

++++++
 Process from Point/Station 400.000 to Point/Station 420.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1850.000(Ft.)
 Bottom (of initial area) elevation = 1320.000(Ft.)
 Difference in elevation = 530.000(Ft.)
 Slope = 0.53000 s(%)= 53.00
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.447 min.
 Rainfall intensity = 3.326(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.791
 Subarea runoff = 24.990(CFS)
 Total initial stream area = 9.500(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 420.000 to Point/Station 421.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 37.485(CFS)
 Depth of flow = 0.883(Ft.), Average velocity = 12.826(Ft/s)
 ***** Irregular Channel Data *****

Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	20.00
2	100.00	0.00
3	150.00	20.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 37.485(CFS)
 ' ' flow top width = 6.621(Ft.)
 ' ' velocity = 12.826(Ft/s)
 ' ' area = 2.923(Sq.Ft)
 ' ' Froude number = 3.402

Upstream point elevation = 1320.000(Ft.)
 Downstream point elevation = 1140.000(Ft.)
 Flow length = 630.000(Ft.)
 Travel time = 0.82 min.
 Time of concentration = 10.27 min.
 Depth of flow = 0.883(Ft.)
 Average velocity = 12.826(Ft/s)
 Total irregular channel flow = 37.485(CFS)
 Irregular channel normal depth above invert elev. = 0.883(Ft.)
 Average velocity of channel(s) = 12.826(Ft/s)

Sub-Channel No. 1 Critical depth = 1.438(Ft.)
 ' ' Critical flow top width = 10.781(Ft.)
 ' ' Critical flow velocity = 4.837(Ft/s)
 ' ' Critical flow area = 7.749(Sq.Ft)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404(In/Hr)
 Rainfall intensity = 3.165(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.785
 Subarea runoff = 22.224(CFS) for 9.500(Ac.)
 Total runoff = 47.214(CFS)
 Effective area this stream = 19.00(Ac.)
 Total Study Area (Main Stream No. 1) = 86.50(Ac.)
 Area averaged Fm value = 0.404(In/Hr)

+++++
 Process from Point/Station 421.000 to Point/Station 422.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 63.366(CFS)
 Depth of flow = 1.089(Ft.), Average velocity = 8.545(Ft/s)
 ***** Irregular Channel Data *****

Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 20.00
 2 100.00 0.00
 3 250.00 20.00
 Manning's 'N' friction factor = 0.035

Sub-Channel flow = 63.366(CFS)
 ' ' flow top width = 13.616(Ft.)
 ' ' velocity = 8.545(Ft/s)
 ' ' area = 7.416(Sq.Ft)

Froude number = 2.040

Upstream point elevation = 1140.000(Ft.)
 Downstream point elevation = 1064.000(Ft.)
 Flow length = 820.000(Ft.)
 Travel time = 1.60 min.
 Time of concentration = 11.87 min.
 Depth of flow = 1.089(Ft.)
 Average velocity = 8.545(Ft/s)
 Total irregular channel flow = 63.366(CFS)
 Irregular channel normal depth above invert elev. = 1.089(Ft.)
 Average velocity of channel(s) = 8.545(Ft/s)

Sub-Channel No. 1 Critical depth = 1.453(Ft.)
 Critical flow top width = 18.164(Ft.)
 Critical flow velocity = 4.801(Ft/s)
 Critical flow area = 13.197(Sq.Ft)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404(In/Hr)
 Rainfall intensity = 2.901(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.775
 Subarea runoff = 24.721(CFS) for 13.000(Ac.)
 Total runoff = 71.935(CFS)
 Effective area this stream = 32.00(Ac.)
 Total Study Area (Main Stream No. 1) = 99.50(Ac.)
 Area averaged Fm value = 0.404(In/Hr)

 Process from Point/Station 422.000 to Point/Station 422.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 32.000(Ac.)
 Runoff from this stream = 71.935(CFS)
 Time of concentration = 11.87 min.
 Rainfall intensity = 2.901(In/Hr)
 Area averaged loss rate (Fm) = 0.4035(In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	149.893	13.30	2.709
2	71.935	11.87	2.901
Qmax(1) =			
	1.000 *	1.000 *	149.893) +
	0.923 *	1.000 *	71.935) + = 216.282
Qmax(2) =			
	1.083 *	0.892 *	149.893) +
	1.000 *	1.000 *	71.935) + = 216.754

Total of 2 streams to confluence:
 Flow rates before confluence point:
 149.893 71.935
 Maximum flow rates at confluence using above data:
 216.282 216.754
 Area of streams before confluence:
 67.500 32.000
 Effective area values after confluence:
 99.500 92.201
 Results of confluence:
 Total flow rate = 216.754 (CFS)
 Time of concentration = 11.865 min.
 Effective stream area after confluence = 92.201 (Ac.)
 Stream Area average Pervious fraction (Ap) = 0.942
 Stream Area average soil loss rate (Fm) = 0.399 (In/Hr)
 Study area (this main stream) = 99.50 (Ac.)

+++++
 Process from Point/Station 79.000 to Point/Station 80.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1052.000 (Ft.)
 Downstream point/station elevation = 1040.200 (Ft.)
 Pipe length = 440.00 (Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 216.754 (CFS)
 Given pipe size = 54.00 (In.)
 Calculated individual pipe flow = 216.754 (CFS)
 Normal flow depth in pipe = 32.44 (In.)
 Flow top width inside pipe = 52.89 (In.)
 Critical Depth = 49.65 (In.)
 Pipe flow velocity = 21.72 (Ft/s)
 Travel time through pipe = 0.34 min.
 Time of concentration (TC) = 12.20 min.

+++++
 Process from Point/Station 80.000 to Point/Station 80.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 92.201 (Ac.)
 Runoff from this stream = 216.754 (CFS)
 Time of concentration = 12.20 min.
 Rainfall intensity = 2.853 (In/Hr)
 Area averaged loss rate (Fm) = 0.3993 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.9422

+++++
 Process from Point/Station 423.000 to Point/Station 424.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 56.00
 Pervious ratio (Ap) = 0.5000 Max loss rate (Fm) = 0.367 (In/Hr)

Initial subarea data:

Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1102.500(Ft.)
 Bottom (of initial area) elevation = 1060.500(Ft.)
 Difference in elevation = 42.000(Ft.)
 Slope = 0.04200 s(%) = 4.20
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 11.623 min.
 Rainfall intensity = 2.937(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.788
 Subarea runoff = 20.821(CFS)
 Total initial stream area = 9.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

++++++
 Process from Point/Station 424.000 to Point/Station 425.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1060.500(Ft.)
 End of street segment elevation = 1049.000(Ft.)
 Length of street segment = 800.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 38.172(CFS)
 Depth of flow = 0.514(Ft.), Average velocity = 4.288(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 4.29(Ft/s)
 Travel time = 3.11 min. TC = 14.73 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367(In/Hr)
 Rainfall intensity = 2.548(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.770
 Subarea runoff = 26.288(CFS) for 15.000(Ac.)
 Total runoff = 47.109(CFS)
 Effective area this stream = 24.00(Ac.)
 Total Study Area (Main Stream No. 1) = 123.50(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 47.109(CFS)
 Half street flow at end of street = 23.555(CFS)

Depth of flow = 0.544(Ft.), Average velocity = 4.661(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000(Ft.)

+++++
 Process from Point/Station 425.000 to Point/Station 425.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 24.000(Ac.)
 Runoff from this stream = 47.109(CFS)
 Time of concentration = 14.73 min.
 Rainfall intensity = 2.548(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	216.754	12.20	2.853
2	47.109	14.73	2.548
Qmax(1) =			
	1.000 *	1.000 *	216.754) +
	1.140 *	0.828 *	47.109) + = 261.229
Qmax(2) =			
	0.876 *	1.000 *	216.754) +
	1.000 *	1.000 *	47.109) + = 236.929

Total of 2 streams to confluence:

Flow rates before confluence point:

216.754 47.109

Maximum flow rates at confluence using above data:

261.229 236.929

Area of streams before confluence:

92.201 24.000

Effective area values after confluence:

112.080 116.201

Results of confluence:

Total flow rate = 261.229(CFS)

Time of concentration = 12.203 min.

Effective stream area after confluence = 112.080(Ac.)

Stream Area average Pervious fraction(Ap) = 0.851

Stream Area average soil loss rate(Fm) = 0.393(In/Hr)

Study area (this main stream) = 116.20(Ac.)

End of computations, Total Study Area = 123.50 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.856

Area averaged SCS curve number = 71.7

LINE "P2"

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
 Rational Hydrology Study Date: 01/13/05

FONTANA / LINE P2 HYDROLOGY
 25 YEAR STORM
 JN 04339

Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 25.0
 10 Year storm 1 hour rainfall = 0.930(In.)
 100 Year storm 1 hour rainfall = 1.350(In.)
 Computed rainfall intensity:
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)
 Slope used for rainfall intensity curve b = 0.6000
 Soil antecedent moisture condition (AMC) = 2

+++++
 Process from Point/Station 500.000 to Point/Station 501.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1620.000(Ft.)
 Bottom (of initial area) elevation = 1350.000(Ft.)
 Difference in elevation = 270.000(Ft.)
 Slope = 0.27000 s(%)= 27.00
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 10.812 min.
 Rainfall intensity = 3.068(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.782
 Subarea runoff = 14.387(CFS)
 Total initial stream area = 6.000(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

+++++
 Process from Point/Station 501.000 to Point/Station 502.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 25.177(CFS)
 Depth of flow = 0.658(Ft.), Average velocity = 11.641(Ft/s)
 ***** Irregular Channel Data *****

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-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              20.00
      2             100.00              0.00
      3             200.00             20.00
Manning's 'N' friction factor = 0.035
-----

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Sub-Channel flow = 25.177(CFS)
'   '   flow top width = 6.577(Ft.)
'   '   velocity= 11.641(Ft/s)
'   '   area = 2.163(Sq.Ft)
'   '   Froude number = 3.578

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Upstream point elevation = 1350.000(Ft.)
Downstream point elevation = 1180.000(Ft.)
Flow length = 500.000(Ft.)
Travel time = 0.72 min.
Time of concentration = 11.53 min.
Depth of flow = 0.658(Ft.)
Average velocity = 11.641(Ft/s)
Total irregular channel flow = 25.177(CFS)
Irregular channel normal depth above invert elev. = 0.658(Ft.)
Average velocity of channel(s) = 11.641(Ft/s)

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Sub-Channel No. 1 Critical depth = 1.094(Ft.)
'   '   '   Critical flow top width = 10.938(Ft.)
'   '   '   Critical flow velocity= 4.209(Ft/s)
'   '   '   Critical flow area = 5.981(Sq.Ft)

```

```

Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Rainfall intensity = 2.952(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.777
Subarea runoff = 20.017(CFS) for 9.000(Ac.)
Total runoff = 34.404(CFS)
Effective area this stream = 15.00(Ac.)
Total Study Area (Main Stream No. 1) = 15.00(Ac.)
Area averaged Fm value = 0.404(In/Hr)

```

```

+++++
Process from Point/Station 502.000 to Point/Station 83.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****

```

```

Upstream point/station elevation = 1167.600(Ft.)
Downstream point/station elevation = 1126.000(Ft.)
Pipe length = 660.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 34.404(CFS)
Given pipe size = 24.00(In.)
Calculated individual pipe flow = 34.404(CFS)
Normal flow depth in pipe = 13.48(In.)
Flow top width inside pipe = 23.82(In.)
Critical depth could not be calculated.

```

Pipe flow velocity = 18.94 (Ft/s)
 Travel time through pipe = 0.58 min.
 Time of concentration (TC) = 12.11 min.

+++++
 Process from Point/Station 83.000 to Point/Station 83.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 15.000 (Ac.)
 Runoff from this stream = 34.404 (CFS)
 Time of concentration = 12.11 min.
 Rainfall intensity = 2.866 (In/Hr)
 Area averaged loss rate (Fm) = 0.4035 (In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000

+++++
 Process from Point/Station 503.000 to Point/Station 504.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000 (Ft.)
 Top (of initial area) elevation = 1520.000 (Ft.)
 Bottom (of initial area) elevation = 1180.000 (Ft.)
 Difference in elevation = 340.000 (Ft.)
 Slope = 0.34000 s(%) = 34.00
 $TC = k(0.525) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 10.324 min.
 Rainfall intensity = 3.154 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.785
 Subarea runoff = 24.752 (CFS)
 Total initial stream area = 10.000 (Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404 (In/Hr)

+++++
 Process from Point/Station 504.000 to Point/Station 505.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1167.600 (Ft.)
 End of street segment elevation = 1126.000 (Ft.)
 Length of street segment = 660.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 20.000 (Ft.)
 Distance from crown to crossfall grade break = 18.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500 (Ft.)

Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 27.228(CFS)
 Depth of flow = 0.374(Ft.), Average velocity = 6.735(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 13.965(Ft.)
 Flow velocity = 6.73(Ft/s)
 Travel time = 1.63 min. TC = 11.96 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 2.888(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.776
 Subarea runoff = 2.143(CFS) for 2.000(Ac.)
 Total runoff = 26.896(CFS)
 Effective area this stream = 12.00(Ac.)
 Total Study Area (Main Stream No. 1) = 27.00(Ac.)
 Area averaged Fm value = 0.397(In/Hr)
 Street flow at end of street = 26.896(CFS)
 Half street flow at end of street = 13.448(CFS)
 Depth of flow = 0.373(Ft.), Average velocity = 6.714(Ft/s)
 Flow width (from curb towards crown)= 13.898(Ft.)

++++++
 Process from Point/Station 505.000 to Point/Station 505.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 12.000(Ac.)
 Runoff from this stream = 26.896(CFS)
 Time of concentration = 11.96 min.
 Rainfall intensity = 2.888(In/Hr)
 Area averaged loss rate (Fm) = 0.3974(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.9167
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	34.404	12.11	2.866
2	26.896	11.96	2.888
Qmax(1) =			
	1.000 *	1.000 *	34.404) +
	0.991 *	1.000 *	26.896) + = 61.067
Qmax(2) =			
	1.009 *	0.988 *	34.404) +
	1.000 *	1.000 *	26.896) + = 61.170

Total of 2 streams to confluence:
 Flow rates before confluence point:
 34.404 26.896

Maximum flow rates at confluence using above data:

61.067 61.170

Area of streams before confluence:

15.000 12.000

Effective area values after confluence:

27.000 26.814

Results of confluence:

Total flow rate = 61.170 (CFS)

Time of concentration = 11.958 min.

Effective stream area after confluence = 26.814 (Ac.)

Stream Area average Pervious fraction (Ap) = 0.963

Stream Area average soil loss rate (Fm) = 0.401 (In/Hr)

Study area (this main stream) = 27.00 (Ac.)

Process from Point/Station 83.000 to Point/Station 85.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1126.000 (Ft.)
Downstream point/station elevation = 1092.300 (Ft.)
Pipe length = 450.00 (Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 61.170 (CFS)
Given pipe size = 36.00 (In.)
Calculated individual pipe flow = 61.170 (CFS)
Normal flow depth in pipe = 14.36 (In.)
Flow top width inside pipe = 35.25 (In.)
Critical Depth = 30.26 (In.)
Pipe flow velocity = 23.26 (Ft/s)
Travel time through pipe = 0.32 min.
Time of concentration (TC) = 12.28 min.

Process from Point/Station 85.000 to Point/Station 85.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1

Effective stream flow area = 26.814 (Ac.)

Total study area this main stream = 27.000 (Ac.)

Runoff from this stream = 61.170 (CFS)

Time of concentration = 12.28 min.

Rainfall intensity = 2.842 (In/Hr)

Area averaged loss rate (Fm) = 0.4008 (In/Hr)

Area averaged Pervious ratio (Ap) = 0.9630

Program is now starting with Main Stream No. 2

Process from Point/Station 506.000 to Point/Station 507.000
**** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000

SCS curve number for soil (AMC 2) = 78.00

Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)

Initial subarea data:

Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 2040.000(Ft.)
 Bottom (of initial area) elevation = 1680.000(Ft.)
 Difference in elevation = 360.000(Ft.)
 Slope = 0.36000 s(%) = 36.00
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 10.207 min.
 Rainfall intensity = 3.175(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.786
 Subarea runoff = 19.958(CFS)
 Total initial stream area = 8.000(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 507.000 to Point/Station 508.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

 Estimated mean flow rate at midpoint of channel = 34.927(CFS)
 Depth of flow = 0.950(Ft.), Average velocity = 15.488(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	20.00
2	50.00	0.00
3	100.00	20.00

 Manning's 'N' friction factor = 0.035

 Sub-Channel flow = 34.927(CFS)

'	'	flow top width = 4.749(Ft.)
'	'	velocity = 15.488(Ft/s)
'	'	area = 2.255(Sq.Ft)
'	'	Froude number = 3.961

Upstream point elevation = 1680.000(Ft.)
 Downstream point elevation = 1450.000(Ft.)
 Flow length = 580.000(Ft.)
 Travel time = 0.62 min.
 Time of concentration = 10.83 min.
 Depth of flow = 0.950(Ft.)
 Average velocity = 15.488(Ft/s)
 Total irregular channel flow = 34.927(CFS)
 Irregular channel normal depth above invert elev. = 0.950(Ft.)
 Average velocity of channel(s) = 15.488(Ft/s)

Sub-Channel No. 1 Critical depth = 1.641(Ft.)

'	'	'	Critical flow top width = 8.203(Ft.)
'	'	'	Critical flow velocity = 5.190(Ft/s)
'	'	'	Critical flow area = 6.729(Sq.Ft)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404(In/Hr)
 Rainfall intensity = 3.064(In/Hr) for a 25.0 year storm

Effective runoff coefficient used for area, (total area with modified
rational method) ($Q=KCIA$) is $C = 0.781$
Subarea runoff = 27.938 (CFS) for 12.000 (Ac.)
Total runoff = 47.896 (CFS)
Effective area this stream = 20.00 (Ac.)
Total Study Area (Main Stream No. 2) = 20.00 (Ac.)
Area averaged Fm value = 0.404 (In/Hr)

+++++
Process from Point/Station 508.000 to Point/Station 509.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 80.825 (CFS)
Depth of flow = 1.362 (Ft.), Average velocity = 17.418 (Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 20.00
2 50.00 0.00
3 100.00 20.00
Manning's 'N' friction factor = 0.035

Sub-Channel flow = 80.825 (CFS)
' ' flow top width = 6.812 (Ft.)
' ' velocity = 17.418 (Ft/s)
' ' area = 4.640 (Sq.Ft)
' ' Froude number = 3.719

Upstream point elevation = 1450.000 (Ft.)
Downstream point elevation = 1140.000 (Ft.)
Flow length = 1000.000 (Ft.)
Travel time = 0.96 min.
Time of concentration = 11.79 min.
Depth of flow = 1.362 (Ft.)
Average velocity = 17.418 (Ft/s)
Total irregular channel flow = 80.825 (CFS)
Irregular channel normal depth above invert elev. = 1.362 (Ft.)
Average velocity of channel(s) = 17.418 (Ft/s)

Sub-Channel No. 1 Critical depth = 2.313 (Ft.)
' ' ' Critical flow top width = 11.563 (Ft.)
' ' ' Critical flow velocity = 6.046 (Ft/s)
' ' ' Critical flow area = 13.369 (Sq.Ft)

Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil (AMC 2) = 78.00
Pervious ratio (A_p) = 1.0000 Max loss rate (F_m) = 0.404 (In/Hr)
Rainfall intensity = 2.913 (In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) ($Q=KCIA$) is $C = 0.775$
Subarea runoff = 59.369 (CFS) for 27.500 (Ac.)
Total runoff = 107.265 (CFS)
Effective area this stream = 47.50 (Ac.)
Total Study Area (Main Stream No. 2) = 47.50 (Ac.)

Area averaged Fm value = 0.404(In/Hr)

+++++
 Process from Point/Station 509.000 to Point/Station 509.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
 Stream flow area = 47.500(Ac.)
 Runoff from this stream = 107.265(CFS)
 Time of concentration = 11.79 min.
 Rainfall intensity = 2.913(In/Hr)
 Area averaged loss rate (Fm) = 0.4035(In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000

+++++
 Process from Point/Station 510.000 to Point/Station 511.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1560.000(Ft.)
 Bottom (of initial area) elevation = 1180.000(Ft.)
 Difference in elevation = 380.000(Ft.)
 Slope = 0.38000 s(%) = 38.00
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 10.097 min.
 Rainfall intensity = 3.196(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.786
 Subarea runoff = 23.877(CFS)
 Total initial stream area = 9.500(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

+++++
 Process from Point/Station 511.000 to Point/Station 512.000
 **** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 1180.000(Ft.)
 Downstream point elevation = 1140.000(Ft.)
 Channel length thru subarea = 530.000(Ft.)
 Channel base width = 0.000(Ft.)
 Slope or 'Z' of left channel bank = 1.500
 Slope or 'Z' of right channel bank = 1.500
 Estimated mean flow rate at midpoint of channel = 54.666(CFS)
 Manning's 'N' = 0.015
 Maximum depth of channel = 2.000(Ft.)
 Flow(q) thru subarea = 54.666(CFS)
 Depth of flow = 1.389(Ft.), Average velocity = 18.883(Ft/s)
 Channel flow top width = 4.168(Ft.)
 Flow Velocity = 18.88(Ft/s)
 Travel time = 0.47 min.

Time of concentration = 10.57 min.
 Critical depth = 2.375 (Ft.)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Rainfall intensity = 3.110 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.783
 Subarea runoff = 58.956 (CFS) for 24.500 (Ac.)
 Total runoff = 82.833 (CFS)
 Effective area this stream = 34.00 (Ac.)
 Total Study Area (Main Stream No. 2) = 81.50 (Ac.)
 Area averaged Fm value = 0.404 (In/Hr)

++++++
 Process from Point/Station 512.000 to Point/Station 512.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2

Stream flow area = 34.000 (Ac.)
 Runoff from this stream = 82.833 (CFS)
 Time of concentration = 10.57 min.
 Rainfall intensity = 3.110 (In/Hr)
 Area averaged loss rate (Fm) = 0.4035 (In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	107.265	11.79	2.913
2	82.833	10.57	3.110
Qmax(1) =			
	1.000 *	1.000 *	107.265) +
	0.927 *	1.000 *	82.833) + = 184.044
Qmax(2) =			
	1.079 *	0.896 *	107.265) +
	1.000 *	1.000 *	82.833) + = 186.550

Total of 2 streams to confluence:

Flow rates before confluence point:

107.265 82.833

Maximum flow rates at confluence using above data:

184.044 186.550

Area of streams before confluence:

47.500 34.000

Effective area values after confluence:

81.500 76.572

Results of confluence:

Total flow rate = 186.550 (CFS)

Time of concentration = 10.565 min.

Effective stream area after confluence = 76.572 (Ac.)

Stream Area average Pervious fraction (Ap) = 1.000

Stream Area average soil loss rate (Fm) = 0.404 (In/Hr)

Study area (this main stream) = 81.50 (Ac.)

+++++
 Process from Point/Station 512.000 to Point/Station 84.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1137.500 (Ft.)
 Downstream point/station elevation = 1110.000 (Ft.)
 Pipe length = 450.00 (Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 186.550 (CFS)
 Given pipe size = 30.00 (In.)
 NOTE: Normal flow is pressure flow in user selected pipe size.
 The approximate hydraulic grade line above the pipe invert is
 99.193 (Ft.) at the headworks or inlet of the pipe(s)
 Pipe friction loss = 93.053 (Ft.)
 Minor friction loss = 33.640 (Ft.) K-factor = 1.50
 Pipe flow velocity = 38.00 (Ft/s)
 Travel time through pipe = 0.20 min.
 Time of concentration (TC) = 10.76 min.

+++++
 Process from Point/Station 84.000 to Point/Station 84.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
 Stream flow area = 76.572 (Ac.)
 Runoff from this stream = 186.550 (CFS)
 Time of concentration = 10.76 min.
 Rainfall intensity = 3.076 (In/Hr)
 Area averaged loss rate (Fm) = 0.4035 (In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000

+++++
 Process from Point/Station 513.000 to Point/Station 514.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000 (Ft.)
 Top (of initial area) elevation = 1770.000 (Ft.)
 Bottom (of initial area) elevation = 1460.000 (Ft.)
 Difference in elevation = 310.000 (Ft.)
 Slope = 0.31000 s(%) = 31.00
 $TC = k(0.525) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 10.517 min.
 Rainfall intensity = 3.119 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.784
 Subarea runoff = 17.108 (CFS)
 Total initial stream area = 7.000 (Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404 (In/Hr)

 Process from Point/Station 514.000 to Point/Station 515.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 25.662(CFS)
 Depth of flow = 0.584(Ft.), Average velocity = 10.023(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 20.00
 2 150.00 0.00
 3 300.00 20.00
 Manning's 'N' friction factor = 0.035

 Sub-Channel flow = 25.662(CFS)
 ' ' flow top width = 8.764(Ft.)
 ' ' velocity = 10.023(Ft/s)
 ' ' area = 2.560(Sq.Ft)
 ' ' Froude number = 3.268

Upstream point elevation = 1460.000(Ft.)
 Downstream point elevation = 1140.000(Ft.)
 Flow length = 1100.000(Ft.)
 Travel time = 1.83 min.
 Time of concentration = 12.35 min.
 Depth of flow = 0.584(Ft.)
 Average velocity = 10.023(Ft/s)
 Total irregular channel flow = 25.662(CFS)
 Irregular channel normal depth above invert elev. = 0.584(Ft.)
 Average velocity of channel(s) = 10.023(Ft/s)

Sub-Channel No. 1 Critical depth = 0.938(Ft.)
 ' ' Critical flow top width = 14.063(Ft.)
 ' ' Critical flow velocity = 3.893(Ft/s)
 ' ' Critical flow area = 6.592(Sq.Ft)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404(In/Hr)
 Rainfall intensity = 2.833(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.772
 Subarea runoff = 13.503(CFS) for 7.000(Ac.)
 Total runoff = 30.611(CFS)
 Effective area this stream = 14.00(Ac.)
 Total Study Area (Main Stream No. 2) = 95.50(Ac.)
 Area averaged Fm value = 0.404(In/Hr)

 Process from Point/Station 515.000 to Point/Station 84.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

 Upstream point/station elevation = 1119.100(Ft.)

Downstream point/station elevation = 1111.400(Ft.)
 Pipe length = 280.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 30.611(CFS)
 Given pipe size = 18.00(In.)
 NOTE: Normal flow is pressure flow in user selected pipe size.
 The approximate hydraulic grade line above the pipe invert is
 23.058(Ft.) at the headworks or inlet of the pipe(s)
 Pipe friction loss = 23.769(Ft.)
 Minor friction loss = 6.989(Ft.) K-factor = 1.50
 Pipe flow velocity = 17.32(Ft/s)
 Travel time through pipe = 0.27 min.
 Time of concentration (TC) = 12.62 min.

++++++
 Process from Point/Station 84.000 to Point/Station 84.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2

Stream flow area = 14.000(Ac.)
 Runoff from this stream = 30.611(CFS)
 Time of concentration = 12.62 min.
 Rainfall intensity = 2.796(In/Hr)
 Area averaged loss rate (Fm) = 0.4035(In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	186.550	10.76	3.076
2	30.611	12.62	2.796
Qmax(1) =			
	1.000 *	1.000 *	186.550) +
	1.117 *	0.853 *	30.611) + = 215.717
Qmax(2) =			
	0.895 *	1.000 *	186.550) +
	1.000 *	1.000 *	30.611) + = 197.640

Total of 2 streams to confluence:

Flow rates before confluence point:

186.550 30.611

Maximum flow rates at confluence using above data:

215.717 197.640

Area of streams before confluence:

76.572 14.000

Effective area values after confluence:

88.515 90.572

Results of confluence:

Total flow rate = 215.717(CFS)

Time of concentration = 10.762 min.

Effective stream area after confluence = 88.515(Ac.)

Stream Area average Pervious fraction(Ap) = 1.000

Stream Area average soil loss rate(Fm) = 0.404(In/Hr)

Study area (this main stream) = 90.57(Ac.)

++++++
 Process from Point/Station 84.000 to Point/Station 85.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1110.700(Ft.)
 Downstream point/station elevation = 1092.300(Ft.)
 Pipe length = 600.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 215.717(CFS)
 Given pipe size = 30.00(In.)
 NOTE: Normal flow is pressure flow in user selected pipe size.
 The approximate hydraulic grade line above the pipe invert is
 192.481(Ft.) at the headworks or inlet of the pipe(s)
 Pipe friction loss = 165.899(Ft.)
 Minor friction loss = 44.981(Ft.) K-factor = 1.50
 Pipe flow velocity = 43.95(Ft/s)
 Travel time through pipe = 0.23 min.
 Time of concentration (TC) = 10.99 min.

++++++
 Process from Point/Station 85.000 to Point/Station 85.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Effective stream flow area = 88.515(Ac.)
 Total study area this main stream = 95.500(Ac.)
 Runoff from this stream = 215.717(CFS)
 Time of concentration = 10.99 min.
 Rainfall intensity = 3.038(In/Hr)
 Area averaged loss rate (Fm) = 0.4035(In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000
 Program is now starting with Main Stream No. 3

++++++
 Process from Point/Station 516.000 to Point/Station 517.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1148.000(Ft.)
 Bottom (of initial area) elevation = 1101.000(Ft.)
 Difference in elevation = 47.000(Ft.)
 Slope = 0.04700 s(%)= 4.70
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 11.364 min.
 Rainfall intensity = 2.977(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.789
 Subarea runoff = 16.446(CFS)
 Total initial stream area = 7.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

++++++
 Process from Point/Station 517.000 to Point/Station 517.000

**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 3
 Effective stream flow area = 7.000 (Ac.)
 Total study area this main stream = 7.000 (Ac.)
 Runoff from this stream = 16.446 (CFS)
 Time of concentration = 11.36 min.
 Rainfall intensity = 2.977 (In/Hr)
 Area averaged loss rate (Fm) = 0.3670 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	61.170	12.28	2.842
2	215.717	10.99	3.038
3	16.446	11.36	2.977

Qmax(1) =
 1.000 * 1.000 * 61.170) +
 0.926 * 1.000 * 215.717) +
 0.948 * 1.000 * 16.446) + = 276.451

Qmax(2) =
 1.080 * 0.895 * 61.170) +
 1.000 * 1.000 * 215.717) +
 1.023 * 0.967 * 16.446) + = 291.121

Qmax(3) =
 1.055 * 0.925 * 61.170) +
 0.977 * 1.000 * 215.717) +
 1.000 * 1.000 * 16.446) + = 286.961

Total of 3 main streams to confluence:

Flow rates before confluence point:

62.170 216.717 17.446

Maximum flow rates at confluence using above data:

276.451 291.121 286.961

Effective Area of streams before confluence:

26.814 88.515 7.000

Effective area values after confluence:

122.329 119.281 120.329

Results of confluence:

Total flow rate = 291.121 (CFS)

Time of concentration = 10.990 min.

Effective stream area after confluence = 119.281 (Ac.)

Stream Area average Pervious fraction (Ap) = 0.963

Stream Area average soil loss rate (Fm) = 0.401 (In/Hr)

Stream effective area = 122.33 (Ac.)

+++++
 Process from Point/Station 85.000 to Point/Station 86.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1092.300 (Ft.)

Downstream point/station elevation = 1059.300 (Ft.)

Pipe length = 950.00 (Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 291.121 (CFS)

Given pipe size = 39.00(In.)
 NOTE: Normal flow is pressure flow in user selected pipe size.
 The approximate hydraulic grade line above the pipe invert is
 113.743(Ft.) at the headworks or inlet of the pipe(s)
 Pipe friction loss = 118.059(Ft.)
 Minor friction loss = 28.684(Ft.) K-factor = 1.50
 Pipe flow velocity = 35.09(Ft/s)
 Travel time through pipe = 0.45 min.
 Time of concentration (TC) = 11.44 min.

+++++
 Process from Point/Station 86.000 to Point/Station 86.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 119.281(Ac.)
 Runoff from this stream = 291.121(CFS)
 Time of concentration = 11.44 min.
 Rainfall intensity = 2.965(In/Hr)
 Area averaged loss rate (Fm) = 0.4008(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.9633

+++++
 Process from Point/Station 518.000 to Point/Station 519.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1148.000(Ft.)
 Bottom (of initial area) elevation = 1101.000(Ft.)
 Difference in elevation = 47.000(Ft.)
 Slope = 0.04700 s(%) = 4.70
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 11.364 min.
 Rainfall intensity = 2.977(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.789
 Subarea runoff = 19.970(CFS)
 Total initial stream area = 8.500(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

+++++
 Process from Point/Station 519.000 to Point/Station 520.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1101.000(Ft.)
 End of street segment elevation = 1066.500(Ft.)
 Length of street segment = 900.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)

Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 29.954(CFS)
 Depth of flow = 0.414(Ft.), Average velocity = 5.714(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 15.968(Ft.)
 Flow velocity = 5.71(Ft/s)
 Travel time = 2.62 min. TC = 13.99 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 2.628(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.774
 Subarea runoff = 14.629(CFS) for 8.500(Ac.)
 Total runoff = 34.599(CFS)
 Effective area this stream = 17.00(Ac.)
 Total Study Area (Main Stream No. 1) = 24.00(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 34.599(CFS)
 Half street flow at end of street = 17.299(CFS)
 Depth of flow = 0.433(Ft.), Average velocity = 5.921(Ft/s)
 Flow width (from curb towards crown)= 16.884(Ft.)

++++++
 Process from Point/Station 520.000 to Point/Station 520.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 17.000(Ac.)
 Runoff from this stream = 34.599(CFS)
 Time of concentration = 13.99 min.
 Rainfall intensity = 2.628(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000

++++++
 Process from Point/Station 521.000 to Point/Station 522.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00

Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1111.000(Ft.)
 Bottom (of initial area) elevation = 1101.000(Ft.)
 Difference in elevation = 10.000(Ft.)
 Slope = 0.01000 s(%)= 1.00
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 15.486 min.
 Rainfall intensity = 2.473(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.766
 Subarea runoff = 10.424(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

++++++
 Process from Point/Station 522.000 to Point/Station 523.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1101.000(Ft.)
 End of street segment elevation = 1066.500(Ft.)
 Length of street segment = 900.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 26.533(CFS)
 Depth of flow = 0.400(Ft.), Average velocity = 5.547(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 15.233(Ft.)
 Flow velocity = 5.55(Ft/s)
 Travel time = 2.70 min. TC = 18.19 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 2.245(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.753
 Subarea runoff = 27.609(CFS) for 17.000(Ac.)
 Total runoff = 38.033(CFS)
 Effective area this stream = 22.50(Ac.)
 Total Study Area (Main Stream No. 1) = 46.50(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 38.033(CFS)
 Half street flow at end of street = 19.016(CFS)

Depth of flow = 0.445(Ft.), Average velocity = 6.060(Ft/s)
 Flow width (from curb towards crown)= 17.511(Ft.)

 Process from Point/Station 523.000 to Point/Station 523.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3

Stream flow area = 22.500(Ac.)
 Runoff from this stream = 38.033(CFS)
 Time of concentration = 18.19 min.
 Rainfall intensity = 2.245(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000

Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	291.121	11.44	2.965
2	34.599	13.99	2.628
3	38.033	18.19	2.245
Qmax(1) =			
	1.000 *	1.000 *	291.121) +
	1.149 *	0.818 *	34.599) +
	1.383 *	0.629 *	38.033) + = 356.728
Qmax(2) =			
	0.869 *	1.000 *	291.121) +
	1.000 *	1.000 *	34.599) +
	1.204 *	0.769 *	38.033) + = 322.681
Qmax(3) =			
	0.719 *	1.000 *	291.121) +
	0.831 *	1.000 *	34.599) +
	1.000 *	1.000 *	38.033) + = 276.134

Total of 3 streams to confluence:

Flow rates before confluence point:

291.121 34.599 38.033

Maximum flow rates at confluence using above data:

356.728 322.681 276.134

Area of streams before confluence:

119.281 17.000 22.500

Effective area values after confluence:

147.337 153.584 158.781

Results of confluence:

Total flow rate = 356.728(CFS)

Time of concentration = 11.441 min.

Effective stream area after confluence = 147.337(Ac.)

Stream Area average Pervious fraction(Ap) = 0.848

Stream Area average soil loss rate(Fm) = 0.392(In/Hr)

Study area (this main stream) = 158.78(Ac.)

 Process from Point/Station 86.000 to Point/Station 87.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1059.300(Ft.)

Downstream point/station elevation = 1053.200(Ft.)

Pipe length = 445.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 356.728(CFS)
 Given pipe size = 48.00(In.)
 NOTE: Normal flow is pressure flow in user selected pipe size.
 The approximate hydraulic grade line above the pipe invert is
 40.106(Ft.) at the headworks or inlet of the pipe(s)
 Pipe friction loss = 27.436(Ft.)
 Minor friction loss = 18.770(Ft.) K-factor = 1.50
 Pipe flow velocity = 28.39(Ft/s)
 Travel time through pipe = 0.26 min.
 Time of concentration (TC) = 11.70 min.

++++++
 Process from Point/Station 87.000 to Point/Station 87.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 147.337(Ac.)
 Runoff from this stream = 356.728(CFS)
 Time of concentration = 11.70 min.
 Rainfall intensity = 2.925(In/Hr)
 Area averaged loss rate (Fm) = 0.3924(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.8480

++++++
 Process from Point/Station 524.000 to Point/Station 525.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 750.000(Ft.)
 Top (of initial area) elevation = 1072.300(Ft.)
 Bottom (of initial area) elevation = 1065.000(Ft.)
 Difference in elevation = 7.300(Ft.)
 Slope = 0.00973 s(%)= 0.97
 $TC = k(0.525) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 18.730 min.
 Rainfall intensity = 2.206(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.735
 Subarea runoff = 14.601(CFS)
 Total initial stream area = 9.000(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 525.000 to Point/Station 525.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 9.000(Ac.)
 Runoff from this stream = 14.601(CFS)
 Time of concentration = 18.73 min.

Rainfall intensity = 2.206(In/Hr)
 Area averaged loss rate (Fm) = 0.4035(In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	356.728	11.70	2.925
2	14.601	18.73	2.206

Qmax(1) =
 1.000 * 1.000 * 356.728) +
 1.399 * 0.625 * 14.601) + = 369.491

Qmax(2) =
 0.716 * 1.000 * 356.728) +
 1.000 * 1.000 * 14.601) + = 270.033

Total of 2 streams to confluence:

Flow rates before confluence point:

356.728 14.601

Maximum flow rates at confluence using above data:

369.491 270.033

Area of streams before confluence:

147.337 9.000

Effective area values after confluence:

152.960 156.337

Results of confluence:

Total flow rate = 369.491(CFS)

Time of concentration = 11.702 min.

Effective stream area after confluence = 152.960(Ac.)

Stream Area average Pervious fraction(Ap) = 0.857

Stream Area average soil loss rate(Fm) = 0.393(In/Hr)

Study area (this main stream) = 156.34(Ac.)

+++++
 Process from Point/Station 87.000 to Point/Station 88.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1050.900(Ft.)
 Downstream point/station elevation = 1033.600(Ft.)
 Pipe length = 370.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 369.491(CFS)
 Given pipe size = 54.00(In.)
 Calculated individual pipe flow = 369.491(CFS)
 Normal flow depth in pipe = 38.91(In.)
 Flow top width inside pipe = 48.47(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 30.11(Ft/s)
 Travel time through pipe = 0.20 min.
 Time of concentration (TC) = 11.91 min.

+++++
 Process from Point/Station 88.000 to Point/Station 88.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 152.960(Ac.)
 Runoff from this stream = 369.491(CFS)

Time of concentration = 11.91 min.
 Rainfall intensity = 2.895(In/Hr)
 Area averaged loss rate (Fm) = 0.3930(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.8568

+++++
 Process from Point/Station 526.000 to Point/Station 527.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1065.000(Ft.)
 Bottom (of initial area) elevation = 1060.000(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%)= 0.50
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 11.164(CFS)
 Total initial stream area = 6.500(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

+++++
 Process from Point/Station 527.000 to Point/Station 527.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 6.500(Ac.)
 Runoff from this stream = 11.164(CFS)
 Time of concentration = 17.79 min.
 Rainfall intensity = 2.275(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000

+++++
 Process from Point/Station 528.000 to Point/Station 529.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1065.000(Ft.)
 Bottom (of initial area) elevation = 1060.000(Ft.)

Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.389) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 11.164(CFS)
 Total initial stream area = 6.500(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

++++++
 Process from Point/Station 529.000 to Point/Station 529.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3

Stream flow area = 6.500(Ac.)
 Runoff from this stream = 11.164(CFS)
 Time of concentration = 17.79 min.
 Rainfall intensity = 2.275(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	369.491	11.91	2.895
2	11.164	17.79	2.275
3	11.164	17.79	2.275

Qmax(1) =
 1.000 * 1.000 * 369.491) +
 1.325 * 0.669 * 11.164) +
 1.325 * 0.669 * 11.164) + = 389.290

Qmax(2) =
 0.752 * 1.000 * 369.491) +
 1.000 * 1.000 * 11.164) +
 1.000 * 1.000 * 11.164) + = 300.304

Qmax(3) =
 0.752 * 1.000 * 369.491) +
 1.000 * 1.000 * 11.164) +
 1.000 * 1.000 * 11.164) + = 300.304

Total of 3 streams to confluence:

Flow rates before confluence point:

369.491 11.164 11.164

Maximum flow rates at confluence using above data:

389.290 300.304 300.304

Area of streams before confluence:

152.960 6.500 6.500

Effective area values after confluence:

161.661 165.960 165.960

Results of confluence:

Total flow rate = 389.290(CFS)

Time of concentration = 11.907 min.

Effective stream area after confluence = 161.661(Ac.)

Stream Area average Pervious fraction(Ap) = 0.829

Stream Area average soil loss rate(Fm) = 0.391(In/Hr)

Study area (this main stream) = 165.96(Ac.)

End of computations, Total Study Area = 191.00 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction(A_p) = 0.839

Area averaged SCS curve number = 70.9

LINE 'P1'

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
Rational Hydrology Study Date: 01/13/05-----
FONTANA / LINE P1 HYDROLOGY
25 YEAR STORM
JN 04339

Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 25.0
10 Year storm 1 hour rainfall = 0.930(In.)
100 Year storm 1 hour rainfall = 1.350(In.)
Computed rainfall intensity:
Storm year = 25.00 1 hour rainfall = 1.097 (In.)
Slope used for rainfall intensity curve b = 0.6000
Soil antecedent moisture condition (AMC) = 2++++
Process from Point/Station 400.000 to Point/Station 401.000
**** INITIAL AREA EVALUATION ****-----
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1850.000(Ft.)
Bottom (of initial area) elevation = 1300.000(Ft.)
Difference in elevation = 550.000(Ft.)
Slope = 0.55000 s(%)= 55.00
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
Initial area time of concentration = 9.377 min.
Rainfall intensity = 3.341(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.791
Subarea runoff = 15.863(CFS)
Total initial stream area = 6.000(Ac.)
Pervious area fraction = 1.000
Initial area Fm value = 0.404(In/Hr)++++
Process from Point/Station 401.000 to Point/Station 402.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****-----
Estimated mean flow rate at midpoint of channel = 28.422(CFS)
Depth of flow = 0.589(Ft.), Average velocity = 9.365(Ft/s)
***** Irregular Channel Data *****

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-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              20.00
      2             150.00              0.00
      3             350.00             20.00
Manning's 'N' friction factor = 0.035
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```

```

Sub-Channel flow = 28.422(CFS)
'      ' flow top width = 10.306(Ft.)
'      ' velocity= 9.366(Ft/s)
'      ' area = 3.035(Sq.Ft)
'      ' Froude number = 3.042

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```

Upstream point elevation = 1300.000(Ft.)
Downstream point elevation = 1087.000(Ft.)
Flow length = 850.000(Ft.)
Travel time = 1.51 min.
Time of concentration = 10.89 min.
Depth of flow = 0.589(Ft.)
Average velocity = 9.365(Ft/s)
Total irregular channel flow = 28.422(CFS)
Irregular channel normal depth above invert elev. = 0.589(Ft.)
Average velocity of channel(s) = 9.365(Ft/s)

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Sub-Channel No. 1 Critical depth = 0.922(Ft.)
'      '      ' Critical flow top width = 16.133(Ft.)
'      '      ' Critical flow velocity= 3.822(Ft/s)
'      '      ' Critical flow area = 7.436(Sq.Ft)

```

```

Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Rainfall intensity = 3.054(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method)(Q=KCIA) is C = 0.781
Subarea runoff = 21.117(CFS) for 9.500(Ac.)
Total runoff = 36.980(CFS)
Effective area this stream = 15.50(Ac.)
Total Study Area (Main Stream No. 1) = 15.50(Ac.)
Area averaged Fm value = 0.404(In/Hr)

```

```

*****
Process from Point/Station 402.000 to Point/Station 75.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****

```

```

Upstream point/station elevation = 1080.000(Ft.)
Downstream point/station elevation = 1077.000(Ft.)
Pipe length = 550.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 36.980(CFS)
Given pipe size = 36.00(In.)
Calculated individual pipe flow = 36.980(CFS)
Normal flow depth in pipe = 23.27(In.)
Flow top width inside pipe = 34.42(In.)
Critical Depth = 23.74(In.)

```

Pipe flow velocity = 7.65(Ft/s)
 Travel time through pipe = 1.20 min.
 Time of concentration (TC) = 12.09 min.

+++++
 Process from Point/Station 75.000 to Point/Station 75.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 1
 Effective stream flow area = 15.500(Ac.)
 Total study area this main stream = 15.500(Ac.)
 Runoff from this stream = 36.980(CFS)
 Time of concentration = 12.09 min.
 Rainfall intensity = 2.869(In/Hr)
 Area averaged loss rate (Fm) = 0.4035(In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000
 Program is now starting with Main Stream No. 2

+++++
 Process from Point/Station 403.000 to Point/Station 404.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1600.000(Ft.)
 Bottom (of initial area) elevation = 1140.000(Ft.)
 Difference in elevation = 460.000(Ft.)
 Slope = 0.46000 s(%)= 46.00
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.719 min.
 Rainfall intensity = 3.270(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.789
 Subarea runoff = 14.191(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

+++++
 Process from Point/Station 404.000 to Point/Station 405.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 25.801(CFS)
 Depth of flow = 0.623(Ft.), Average velocity = 6.651(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	20.00
2	200.00	0.00
3	400.00	20.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 25.801(CFS)
 ' ' flow top width = 12.457(Ft.)
 ' ' velocity = 6.651(Ft/s)
 ' ' area = 3.879(Sq.Ft)
 ' ' Froude number = 2.100

Upstream point elevation = 1140.000(Ft.)
 Downstream point elevation = 1085.000(Ft.)
 Flow length = 470.000(Ft.)
 Travel time = 1.18 min.
 Time of concentration = 10.90 min.
 Depth of flow = 0.623(Ft.)
 Average velocity = 6.651(Ft/s)
 Total irregular channel flow = 25.801(CFS)
 Irregular channel normal depth above invert elev. = 0.623(Ft.)
 Average velocity of channel(s) = 6.651(Ft/s)

Sub-Channel No. 1 Critical depth = 0.836(Ft.)
 ' ' Critical flow top width = 16.719(Ft.)
 ' ' Critical flow velocity = 3.692(Ft/s)
 ' ' Critical flow area = 6.988(Sq.Ft)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404(In/Hr)
 Rainfall intensity = 3.053(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.781
 Subarea runoff = 20.390(CFS) for 9.000(Ac.)
 Total runoff = 34.581(CFS)
 Effective area this stream = 14.50(Ac.)
 Total Study Area (Main Stream No. 2) = 14.50(Ac.)
 Area averaged Fm value = 0.404(In/Hr)

 Process from Point/Station 405.000 to Point/Station 75.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1078.000(Ft.)
 Downstream point/station elevation = 1077.000(Ft.)
 Pipe length = 150.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 34.581(CFS)
 Given pipe size = 36.00(In.)
 Calculated individual pipe flow = 34.581(CFS)
 Normal flow depth in pipe = 20.84(In.)
 Flow top width inside pipe = 35.55(In.)
 Critical Depth = 22.92(In.)
 Pipe flow velocity = 8.16(Ft/s)
 Travel time through pipe = 0.31 min.
 Time of concentration (TC) = 11.20 min.

Process from Point/Station 75.000 to Point/Station 75.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 2
 Effective stream flow area = 14.500 (Ac.)
 Total study area this main stream = 14.500 (Ac.)
 Runoff from this stream = 34.581 (CFS)
 Time of concentration = 11.20 min.
 Rainfall intensity = 3.003 (In/Hr)
 Area averaged loss rate (Fm) = 0.4035 (In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000
 Program is now starting with Main Stream No. 3

+++++
 Process from Point/Station 406.000 to Point/Station 408.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000 (Ft.)
 Top (of initial area) elevation = 1065.000 (Ft.)
 Bottom (of initial area) elevation = 1055.000 (Ft.)
 Difference in elevation = 10.000 (Ft.)
 Slope = 0.01000 s(%) = 1.00
 $TC = k(0.389) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 15.486 min.
 Rainfall intensity = 2.473 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.766
 Subarea runoff = 14.214 (CFS)
 Total initial stream area = 7.500 (Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367 (In/Hr)

+++++
 Process from Point/Station 408.000 to Point/Station 408.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 3 in normal stream number 1
 Stream flow area = 7.500 (Ac.)
 Runoff from this stream = 14.214 (CFS)
 Time of concentration = 15.49 min.
 Rainfall intensity = 2.473 (In/Hr)
 Area averaged loss rate (Fm) = 0.3670 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000

+++++
 Process from Point/Station 407.000 to Point/Station 408.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1065.000(Ft.)
 Bottom (of initial area) elevation = 1055.000(Ft.)
 Difference in elevation = 10.000(Ft.)
 Slope = 0.01000 s(%)= 1.00
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 15.486 min.
 Rainfall intensity = 2.473(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.766
 Subarea runoff = 11.371(CFS)
 Total initial stream area = 6.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

++++++
 Process from Point/Station 408.000 to Point/Station 408.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 3 in normal stream number 2
 Stream flow area = 6.000(Ac.)
 Runoff from this stream = 11.371(CFS)
 Time of concentration = 15.49 min.
 Rainfall intensity = 2.473(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	14.214	15.49	2.473
2	11.371	15.49	2.473
Qmax(1) =			
	1.000 *	1.000 *	14.214) +
	1.000 *	1.000 *	11.371) + = 25.585
Qmax(2) =			
	1.000 *	1.000 *	14.214) +
	1.000 *	1.000 *	11.371) + = 25.585

Total of 2 streams to confluence:

Flow rates before confluence point:

14.214 11.371

Maximum flow rates at confluence using above data:

25.585 25.585

Area of streams before confluence:

7.500 6.000

Effective area values after confluence:

13.500 13.500

Results of confluence:

Total flow rate = 25.585(CFS)

Time of concentration = 15.486 min.

Effective stream area after confluence = 13.500(Ac.)

Stream Area average Pervious fraction(Ap) = 0.500

Stream Area average soil loss rate(Fm) = 0.367(In/Hr)
 Study area (this main stream) = 13.50(Ac.)

+++++
 Process from Point/Station 408.000 to Point/Station 408.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:

In Main Stream number: 3
 Effective stream flow area = 13.500(Ac.)
 Total study area this main stream = 13.500(Ac.)
 Runoff from this stream = 25.585(CFS)
 Time of concentration = 15.49 min.
 Rainfall intensity = 2.473(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	36.980	12.09	2.869
2	34.581	11.20	3.003
3	25.585	15.49	2.473
Qmax(1) =			
	1.000 *	1.000 *	36.980) +
	0.948 *	1.000 *	34.581) +
	1.188 *	0.781 *	25.585) + = 93.508
Qmax(2) =			
	1.054 *	0.927 *	36.980) +
	1.000 *	1.000 *	34.581) +
	1.252 *	0.723 *	25.585) + = 93.883
Qmax(3) =			
	0.839 *	1.000 *	36.980) +
	0.796 *	1.000 *	34.581) +
	1.000 *	1.000 *	25.585) + = 84.149

Total of 3 main streams to confluence:

Flow rates before confluence point:

37.980 35.581 26.585

Maximum flow rates at confluence using above data:

93.508 93.883 84.149

Effective Area of streams before confluence:

15.500 14.500 13.500

Effective area values after confluence:

40.538 38.630 43.500

Results of confluence:

Total flow rate = 93.883(CFS)

Time of concentration = 11.203 min.

Effective stream area after confluence = 38.630(Ac.)

Stream Area average Pervious fraction(Ap) = 0.845

Stream Area average soil loss rate(Fm) = 0.392(In/Hr)

Stream effective area = 43.50(Ac.)

+++++
 Process from Point/Station 75.000 to Point/Station 76.000

**** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1075.000(Ft.)
 Downstream point/station elevation = 1047.000(Ft.)
 Pipe length = 550.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 93.883(CFS)
 Given pipe size = 42.00(In.)
 Calculated individual pipe flow = 93.883(CFS)
 Normal flow depth in pipe = 18.82(In.)
 Flow top width inside pipe = 41.77(In.)
 Critical Depth = 35.93(In.)
 Pipe flow velocity = 22.47(Ft/s)
 Travel time through pipe = 0.41 min.
 Time of concentration (TC) = 11.61 min.

+++++
 Process from Point/Station 76.000 to Point/Station 80.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1047.000(Ft.)
 Downstream point/station elevation = 1041.300(Ft.)
 Pipe length = 1000.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 93.883(CFS)
 Given pipe size = 54.00(In.)
 Calculated individual pipe flow = 93.883(CFS)
 Normal flow depth in pipe = 31.17(In.)
 Flow top width inside pipe = 53.35(In.)
 Critical Depth = 34.13(In.)
 Pipe flow velocity = 9.88(Ft/s)
 Travel time through pipe = 1.69 min.
 Time of concentration (TC) = 13.30 min.

+++++
 Process from Point/Station 80.000 to Point/Station 80.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 38.630(Ac.)
 Runoff from this stream = 93.883(CFS)
 Time of concentration = 13.30 min.
 Rainfall intensity = 2.709(In/Hr)
 Area averaged loss rate (Fm) = 0.3922(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.8448

+++++
 Process from Point/Station 80.000 to Point/Station 80.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Soil classification AP and SCS values input by user
 USER INPUT of soil data for subarea
 SCS curve number for soil(AMC 2) = 74.46
 Pervious ratio(Ap) = 0.8510 Max loss rate(Fm)= 0.393(In/Hr)
 Rainfall intensity = 2.853(In/Hr) for a 25.0 year storm
 User specified values are as follows:
 TC = 12.20 min. Rain intensity = 2.85(In/Hr)
 Total area this stream = 112.08(Ac.)
 Total Study Area (Main Stream No. 1) = 125.58(Ac.)
 Total runoff = 261.23(CFS)

+++++
 Process from Point/Station 80.000 to Point/Station 80.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 112.080(Ac.)
 Runoff from this stream = 261.230(CFS)
 Time of concentration = 12.20 min.
 Rainfall intensity = 2.853(In/Hr)
 Area averaged loss rate (Fm) = 0.3930(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.8510
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	93.883	13.30	2.709
2	261.230	12.20	2.853

Qmax(1) =

1.000 * 1.000 * 93.883) +
 0.942 * 1.000 * 261.230) + = 339.845

Qmax(2) =

1.062 * 0.917 * 93.883) +
 1.000 * 1.000 * 261.230) + = 352.705

Total of 2 streams to confluence:

Flow rates before confluence point:

93.883 261.230

Maximum flow rates at confluence using above data:

339.845 352.705

Area of streams before confluence:

38.630 112.080

Effective area values after confluence:

150.710 147.521

Results of confluence:

Total flow rate = 352.705(CFS)

Time of concentration = 12.200 min.

Effective stream area after confluence = 147.521(Ac.)

Stream Area average Pervious fraction(Ap) = 0.849

Stream Area average soil loss rate(Fm) = 0.393(In/Hr)

Study area (this main stream) = 150.71(Ac.)

+++++
 Process from Point/Station 80.000 to Point/Station 88.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1037.200(Ft.)
 Downstream point/station elevation = 1031.600(Ft.)
 Pipe length = 1450.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 352.705(CFS)
 Given pipe size = 90.00(In.)
 Calculated individual pipe flow = 352.705(CFS)
 Normal flow depth in pipe = 57.56(In.)
 Flow top width inside pipe = 86.42(In.)
 Critical Depth = 58.29(In.)
 Pipe flow velocity = 11.82(Ft/s)
 Travel time through pipe = 2.04 min.

Time of concentration (TC) = 14.24 min.

+++++
Process from Point/Station 88.000 to Point/Station 88.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 147.521(Ac.)
Runoff from this stream = 352.705(CFS)
Time of concentration = 14.24 min.
Rainfall intensity = 2.600(In/Hr)
Area averaged loss rate (Fm) = 0.3928(In/Hr)
Area averaged Pervious ratio (Ap) = 0.8494

+++++
Process from Point/Station 88.000 to Point/Station 88.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Soil classification AP and SCS values input by user
USER INPUT of soil data for subarea
SCS curve number for soil(AMC 2) = 73.85
Pervious ratio(Ap) = 0.8290 Max loss rate(Fm)= 0.391(In/Hr)
Rainfall intensity = 2.895(In/Hr) for a 25.0 year storm
User specified values are as follows:
TC = 11.91 min. Rain intensity = 2.89(In/Hr)
Total area this stream = 161.66(Ac.)
Total Study Area (Main Stream No. 1) = 287.24(Ac.)
Total runoff = 389.29(CFS)

+++++
Process from Point/Station 88.000 to Point/Station 88.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 161.660(Ac.)
Runoff from this stream = 389.290(CFS)
Time of concentration = 11.91 min.
Rainfall intensity = 2.895(In/Hr)
Area averaged loss rate (Fm) = 0.3910(In/Hr)
Area averaged Pervious ratio (Ap) = 0.8290
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	352.705	14.24	2.600
2	389.290	11.91	2.895

Qmax(1) =
1.000 * 1.000 * 352.705) +
0.882 * 1.000 * 389.290) + = 696.160

Qmax(2) =
1.134 * 0.836 * 352.705) +
1.000 * 1.000 * 389.290) + = 723.574

Total of 2 streams to confluence:
Flow rates before confluence point:
352.705 389.290

Maximum flow rates at confluence using above data:
 696.160 723.574
 Area of streams before confluence:
 147.521 161.660
 Effective area values after confluence:
 309.181 285.002
 Results of confluence:
 Total flow rate = 723.574 (CFS)
 Time of concentration = 11.910 min.
 Effective stream area after confluence = 285.002 (Ac.)
 Stream Area average Pervious fraction (Ap) = 0.839
 Stream Area average soil loss rate (Fm) = 0.392 (In/Hr)
 Study area (this main stream) = 309.18 (Ac.)

 Process from Point/Station 88.000 to Point/Station 89.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1031.100 (Ft.)
 Downstream point/station elevation = 1028.800 (Ft.)
 Pipe length = 550.00 (Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 723.574 (CFS)
 Given pipe size = 96.00 (In.)
 NOTE: Normal flow is pressure flow in user selected pipe size.
 The approximate hydraulic grade line above the pipe invert is
 5.987 (Ft.) at the headworks or inlet of the pipe(s)
 Pipe friction loss = 3.460 (Ft.)
 Minor friction loss = 4.826 (Ft.) K-factor = 1.50
 Pipe flow velocity = 14.40 (Ft/s)
 Travel time through pipe = 0.64 min.
 Time of concentration (TC) = 12.55 min.

 Process from Point/Station 89.000 to Point/Station 89.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 285.002 (Ac.)
 Runoff from this stream = 723.574 (CFS)
 Time of concentration = 12.55 min.
 Rainfall intensity = 2.806 (In/Hr)
 Area averaged loss rate (Fm) = 0.3919 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.8387

 Process from Point/Station 513.000 to Point/Station 530.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000 (Ft.)
 Top (of initial area) elevation = 1770.000 (Ft.)

Bottom (of initial area) elevation = 1380.000(Ft.)
 Difference in elevation = 390.000(Ft.)
 Slope = 0.39000 s(%) = 39.00
 $TC = k(0.525) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 10.045 min.
 Rainfall intensity = 3.206(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.787
 Subarea runoff = 15.134(CFS)
 Total initial stream area = 6.000(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 530.000 to Point/Station 531.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

 Estimated mean flow rate at midpoint of channel = 23.962(CFS)
 Depth of flow = 0.429(Ft.), Average velocity = 8.665(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	10.00
2	150.00	0.00
3	300.00	10.00

 Manning's 'N' friction factor = 0.035

Sub-Channel flow = 23.962(CFS)
 ' ' flow top width = 12.881(Ft.)
 ' ' velocity = 8.665(Ft/s)
 ' ' area = 2.765(Sq.Ft)
 ' ' Froude number = 3.296

Upstream point elevation = 1380.000(Ft.)
 Downstream point elevation = 1120.000(Ft.)
 Flow length = 800.000(Ft.)
 Travel time = 1.54 min.
 Time of concentration = 11.58 min.
 Depth of flow = 0.429(Ft.)
 Average velocity = 8.665(Ft/s)
 Total irregular channel flow = 23.962(CFS)
 Irregular channel normal depth above invert elev. = 0.429(Ft.)
 Average velocity of channel(s) = 8.665(Ft/s)

Sub-Channel No. 1 Critical depth = 0.691(Ft.)

' ' ' Critical flow top width = 20.742(Ft.)
' ' ' Critical flow velocity = 3.342(Ft/s)
' ' ' Critical flow area = 7.171(Sq.Ft)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404(In/Hr)
 Rainfall intensity = 2.943(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.777

Subarea runoff = 14.582(CFS) for 7.000(Ac.)
 Total runoff = 29.716(CFS)
 Effective area this stream = 13.00(Ac.)
 Total Study Area (Main Stream No. 1) = 300.24(Ac.)
 Area averaged Fm value = 0.404(In/Hr)

+++++
 Process from Point/Station 531.000 to Point/Station 532.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1120.000(Ft.)
 End of street segment elevation = 1056.000(Ft.)
 Length of street segment = 1800.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 48.003(CFS)
 Depth of flow = 0.484(Ft.), Average velocity = 6.240(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 19.430(Ft.)
 Flow velocity = 6.24(Ft/s)
 Travel time = 4.81 min. TC = 16.39 min.
 Adding area flow to street
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 2.390(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.748
 Subarea runoff = 22.129(CFS) for 16.000(Ac.)
 Total runoff = 51.845(CFS)
 Effective area this stream = 29.00(Ac.)
 Total Study Area (Main Stream No. 1) = 316.24(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Street flow at end of street = 51.845(CFS)
 Half street flow at end of street = 25.923(CFS)
 Depth of flow = 0.495(Ft.), Average velocity = 6.362(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++
 Process from Point/Station 532.000 to Point/Station 532.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 29.000 (Ac.)
 Runoff from this stream = 51.845 (CFS)
 Time of concentration = 16.39 min.
 Rainfall intensity = 2.390 (In/Hr)
 Area averaged loss rate (Fm) = 0.4035 (In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000

 Process from Point/Station 533.000 to Point/Station 534.000
 ***** INITIAL AREA EVALUATION *****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 56.00
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.073 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000 (Ft.)
 Top (of initial area) elevation = 1064.100 (Ft.)
 Bottom (of initial area) elevation = 1059.100 (Ft.)
 Difference in elevation = 5.000 (Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.902 min.
 Rainfall intensity = 2.638 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875
 Subarea runoff = 15.004 (CFS)
 Total initial stream area = 6.500 (Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073 (In/Hr)

 Process from Point/Station 534.000 to Point/Station 535.000
 ***** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION *****

Top of street segment elevation = 1059.300 (Ft.)
 End of street segment elevation = 1056.200 (Ft.)
 Length of street segment = 330.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 20.000 (Ft.)
 Distance from crown to crossfall grade break = 18.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500 (Ft.)
 Gutter hike from flowline = 1.500 (In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 21.352 (CFS)
 Depth of flow = 0.463 (Ft.), Average velocity = 3.095 (Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 18.380 (Ft.)
 Flow velocity = 3.09 (Ft/s)
 Travel time = 1.78 min. TC = 15.68 min.

Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.454(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.873
 Subarea runoff = 10.712(CFS) for 5.500(Ac.)
 Total runoff = 25.715(CFS)
 Effective area this stream = 12.00(Ac.)
 Total Study Area (Main Stream No. 1) = 328.24(Ac.)
 Area averaged Fm value = 0.073(In/Hr)
 Street flow at end of street = 25.715(CFS)
 Half street flow at end of street = 12.858(CFS)
 Depth of flow = 0.490(Ft.), Average velocity = 3.240(Ft/s)
 Flow width (from curb towards crown)= 19.740(Ft.)

+++++
 Process from Point/Station 535.000 to Point/Station 535.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3

Stream flow area = 12.000(Ac.)
 Runoff from this stream = 25.715(CFS)
 Time of concentration = 15.68 min.
 Rainfall intensity = 2.454(In/Hr)
 Area averaged loss rate (Fm) = 0.0734(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	723.574	12.55	2.806
2	51.845	16.39	2.390
3	25.715	15.68	2.454
Qmax(1) =			
	1.000 *	1.000 *	723.574) +
	1.209 *	0.765 *	51.845) +
	1.147 *	0.800 *	25.715) + = 795.178
Qmax(2) =			
	0.828 *	1.000 *	723.574) +
	1.000 *	1.000 *	51.845) +
	0.973 *	1.000 *	25.715) + = 675.821
Qmax(3) =			
	0.855 *	1.000 *	723.574) +
	1.032 *	0.957 *	51.845) +
	1.000 *	1.000 *	25.715) + = 695.223

Total of 3 streams to confluence:

Flow rates before confluence point:

723.574 51.845 25.715

Maximum flow rates at confluence using above data:

795.178 675.821 695.223

Area of streams before confluence:

285.002	29.000	12.000
Effective area values after confluence:		
316.803	326.002	324.742

Results of confluence:

Total flow rate = 795.178(CFS)

Time of concentration = 12.547 min.

Effective stream area after confluence = 316.803(Ac.)

Stream Area average Pervious fraction(A_p) = 0.826

Stream Area average soil loss rate(F_m) = 0.381(In/Hr)

Study area (this main stream) = 326.00(Ac.)

End of computations, Total Study Area = 358.24 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction(A_p) = 0.827

Area averaged SCS curve number = 73.5

LINE "SIERRA AVE

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
 Rational Hydrology Study Date: 01/13/05

FONTANA / LINE SIERRA AVENUE HYDROLOGY
 25 YEAR STORM
 JN 04339

Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 25.0
 10 Year storm 1 hour rainfall = 0.930(In.)
 100 Year storm 1 hour rainfall = 1.350(In.)
 Computed rainfall intensity:
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)
 Slope used for rainfall intensity curve b = 0.6000
 Soil antecedent moisture condition (AMC) = 2

 Process from Point/Station 200.000 to Point/Station 201.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1103.000(Ft.)
 Bottom (of initial area) elevation = 1098.000(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%)= 0.50
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.902 min.
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.867
 Subarea runoff = 12.575(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.098(In/Hr)

 Process from Point/Station 201.000 to Point/Station 202.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1098.000(Ft.)
 End of street segment elevation = 1091.600(Ft.)
 Length of street segment = 670.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 23.435(CFS)
 Depth of flow = 0.475(Ft.), Average velocity = 3.187(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 18.988(Ft.)
 Flow velocity = 3.19(Ft/s)
 Travel time = 3.50 min. TC = 17.41 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.305(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.868
 Subarea runoff = 17.435(CFS) for 9.500(Ac.)
 Total runoff = 30.010(CFS)
 Effective area this stream = 15.00(Ac.)
 Total Study Area (Main Stream No. 1) = 15.00(Ac.)
 Area averaged Fm value = 0.082(In/Hr)
 Street flow at end of street = 30.010(CFS)
 Half street flow at end of street = 15.005(CFS)
 Depth of flow = 0.509(Ft.), Average velocity = 3.445(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

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 Process from Point/Station 202.000 to Point/Station 60.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1084.600(Ft.)
 Downstream point/station elevation = 1078.400(Ft.)
 Pipe length = 555.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 30.010(CFS)
 Given pipe size = 42.00(In.)
 Calculated individual pipe flow = 30.010(CFS)
 Normal flow depth in pipe = 15.26(In.)
 Flow top width inside pipe = 40.40(In.)
 Critical Depth = 20.31(In.)
 Pipe flow velocity = 9.50(Ft/s)
 Travel time through pipe = 0.97 min.
 Time of concentration (TC) = 18.38 min.

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Process from Point/Station 60.000 to Point/Station 60.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 15.000(Ac.)
 Runoff from this stream = 30.010(CFS)
 Time of concentration = 18.38 min.
 Rainfall intensity = 2.231(In/Hr)
 Area averaged loss rate (Fm) = 0.0823(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

 Process from Point/Station 203.000 to Point/Station 204.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1103.000(Ft.)
 Bottom (of initial area) elevation = 1096.000(Ft.)
 Difference in elevation = 7.000(Ft.)
 Slope = 0.00700 s(%)= 0.70
 $TC = k(0.304) * [(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 12.997 min.
 Rainfall intensity = 2.747(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.868
 Subarea runoff = 15.497(CFS)
 Total initial stream area = 6.500(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.098(In/Hr)

 Process from Point/Station 204.000 to Point/Station 205.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1096.000(Ft.)
 End of street segment elevation = 1090.500(Ft.)
 Length of street segment = 675.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 25.630(CFS)
 Depth of flow = 0.499(Ft.), Average velocity = 3.085(Ft/s)

Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 3.08(Ft/s)
 Travel time = 3.65 min. TC = 16.64 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Rainfall intensity = 2.368(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.863
 Subarea runoff = 15.151(CFS) for 8.500(Ac.)
 Total runoff = 30.648(CFS)
 Effective area this stream = 15.00(Ac.)
 Total Study Area (Main Stream No. 1) = 30.00(Ac.)
 Area averaged Fm value = 0.098(In/Hr)
 Street flow at end of street = 30.648(CFS)
 Half street flow at end of street = 15.324(CFS)
 Depth of flow = 0.523(Ft.), Average velocity = 3.312(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

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 Process from Point/Station 205.000 to Point/Station 205.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 15.000(Ac.)
 Runoff from this stream = 30.648(CFS)
 Time of concentration = 16.64 min.
 Rainfall intensity = 2.368(In/Hr)
 Area averaged loss rate (Fm) = 0.0978(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	30.010	18.38	2.231
2	30.648	16.64	2.368
Qmax(1) =			
	1.000 *	1.000 *	30.010) +
	0.940 *	1.000 *	30.648) + = 58.812
Qmax(2) =			
	1.064 *	0.906 *	30.010) +
	1.000 *	1.000 *	30.648) + = 59.555

Total of 2 streams to confluence:

Flow rates before confluence point:

30.010 30.648

Maximum flow rates at confluence using above data:

58.812 59.555

Area of streams before confluence:

15.000 15.000

Effective area values after confluence:

30.000 28.584

Results of confluence:

Total flow rate = 59.555(CFS)

Time of concentration = 16.645 min.

Effective stream area after confluence = 28.584(Ac.)

Stream Area average Pervious fraction(Ap) = 0.100

Stream Area average soil loss rate(Fm) = 0.090(In/Hr)

Study area (this main stream) = 30.00(Ac.)

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Process from Point/Station 60.000 to Point/Station 61.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1078.400(Ft.)
Downstream point/station elevation = 1076.700(Ft.)
Pipe length = 500.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 59.555(CFS)
Given pipe size = 42.00(In.)
Calculated individual pipe flow = 59.555(CFS)
Normal flow depth in pipe = 35.06(In.)
Flow top width inside pipe = 31.19(In.)
Critical Depth = 29.01(In.)
Pipe flow velocity = 6.95(Ft/s)
Travel time through pipe = 1.20 min.
Time of concentration (TC) = 17.84 min.

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Process from Point/Station 61.000 to Point/Station 61.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 28.584(Ac.)
Runoff from this stream = 59.555(CFS)
Time of concentration = 17.84 min.
Rainfall intensity = 2.271(In/Hr)
Area averaged loss rate (Fm) = 0.0901(In/Hr)
Area averaged Pervious ratio (Ap) = 0.1000

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Process from Point/Station 206.000 to Point/Station 207.000
**** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 32.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1103.000(Ft.)
Bottom (of initial area) elevation = 1097.000(Ft.)
Difference in elevation = 6.000(Ft.)
Slope = 0.00600 s(%)= 0.60
TC = k(0.304)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 13.404 min.

Rainfall intensity = 2.697(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.867
 Subarea runoff = 14.033(CFS)
 Total initial stream area = 6.000(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.098(In/Hr)

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 Process from Point/Station 207.000 to Point/Station 208.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1097.000(Ft.)
 End of street segment elevation = 1089.300(Ft.)
 Length of street segment = 775.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 25.728(CFS)
 Depth of flow = 0.486(Ft.), Average velocity = 3.310(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 19.533(Ft.)
 Flow velocity = 3.31(Ft/s)
 Travel time = 3.90 min. TC = 17.31 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Rainfall intensity = 2.313(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.862
 Subarea runoff = 17.869(CFS) for 10.000(Ac.)
 Total runoff = 31.903(CFS)
 Effective area this stream = 16.00(Ac.)
 Total Study Area (Main Stream No. 1) = 46.00(Ac.)
 Area averaged Fm value = 0.098(In/Hr)
 Street flow at end of street = 31.903(CFS)
 Half street flow at end of street = 15.951(CFS)
 Depth of flow = 0.515(Ft.), Average velocity = 3.572(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

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 Process from Point/Station 208.000 to Point/Station 208.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 16.000(Ac.)
 Runoff from this stream = 31.903(CFS)
 Time of concentration = 17.31 min.
 Rainfall intensity = 2.313(In/Hr)
 Area averaged loss rate (Fm) = 0.0978(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	59.555	17.84	2.271
2	31.903	17.31	2.313

Qmax(1) =
 1.000 * 1.000 * 59.555) +
 0.981 * 1.000 * 31.903) + = 90.852

Qmax(2) =
 1.019 * 0.970 * 59.555) +
 1.000 * 1.000 * 31.903) + = 90.778

Total of 2 streams to confluence:
 Flow rates before confluence point:
 59.555 31.903
 Maximum flow rates at confluence using above data:
 90.852 90.778
 Area of streams before confluence:
 28.584 16.000
 Effective area values after confluence:
 44.584 43.723
 Results of confluence:
 Total flow rate = 90.852(CFS)
 Time of concentration = 17.844 min.
 Effective stream area after confluence = 44.584(Ac.)
 Stream Area average Pervious fraction(Ap) = 0.100
 Stream Area average soil loss rate(Fm) = 0.093(In/Hr)
 Study area (this main stream) = 44.58(Ac.)

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 Process from Point/Station 61.000 to Point/Station 62.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1076.700(Ft.)
 Downstream point/station elevation = 1065.000(Ft.)
 Pipe length = 1320.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 90.852(CFS)
 Given pipe size = 48.00(In.)
 Calculated individual pipe flow = 90.852(CFS)
 Normal flow depth in pipe = 28.78(In.)
 Flow top width inside pipe = 47.04(In.)
 Critical Depth = 34.69(In.)
 Pipe flow velocity = 11.54(Ft/s)
 Travel time through pipe = 1.91 min.
 Time of concentration (TC) = 19.75 min.

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 Process from Point/Station 62.000 to Point/Station 62.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 44.584 (Ac.)
 Runoff from this stream = 90.852 (CFS)
 Time of concentration = 19.75 min.
 Rainfall intensity = 2.137 (In/Hr)
 Area averaged loss rate (Fm) = 0.0928 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

 Process from Point/Station 209.000 to Point/Station 210.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 32.00
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.098 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000 (Ft.)
 Top (of initial area) elevation = 1090.500 (Ft.)
 Bottom (of initial area) elevation = 1084.500 (Ft.)
 Difference in elevation = 6.000 (Ft.)
 Slope = 0.00600 s(%) = 0.60
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.404 min.
 Rainfall intensity = 2.697 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.867
 Subarea runoff = 12.864 (CFS)
 Total initial stream area = 5.500 (Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.098 (In/Hr)

 Process from Point/Station 210.000 to Point/Station 211.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1084.500 (Ft.)
 End of street segment elevation = 1076.500 (Ft.)
 Length of street segment = 875.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 20.000 (Ft.)
 Distance from crown to crossfall grade break = 18.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500 (Ft.)
 Gutter hike from flowline = 1.500 (In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 25.728 (CFS)
 Depth of flow = 0.492 (Ft.), Average velocity = 3.208 (Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 19.846 (Ft.)

Flow velocity = 3.21(Ft/s)
 Travel time = 4.55 min. TC = 17.95 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.263(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.868
 Subarea runoff = 19.533(CFS) for 11.000(Ac.)
 Total runoff = 32.397(CFS)
 Effective area this stream = 16.50(Ac.)
 Total Study Area (Main Stream No. 1) = 62.50(Ac.)
 Area averaged Fm value = 0.082(In/Hr)
 Street flow at end of street = 32.397(CFS)
 Half street flow at end of street = 16.198(CFS)
 Depth of flow = 0.523(Ft.), Average velocity = 3.505(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

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 Process from Point/Station 211.000 to Point/Station 211.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 16.500(Ac.)
 Runoff from this stream = 32.397(CFS)
 Time of concentration = 17.95 min.
 Rainfall intensity = 2.263(In/Hr)
 Area averaged loss rate (Fm) = 0.0815(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

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 Process from Point/Station 212.000 to Point/Station 213.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1092.600(Ft.)
 Bottom (of initial area) elevation = 1086.000(Ft.)
 Difference in elevation = 6.600(Ft.)
 Slope = 0.00660 s(%)= 0.66
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.151 min.
 Rainfall intensity = 2.728(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.868
 Subarea runoff = 11.834(CFS)
 Total initial stream area = 5.000(Ac.)

Pervious area fraction = 0.100
 Initial area Fm value = 0.098 (In/Hr)

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 Process from Point/Station 213.000 to Point/Station 214.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1086.000 (Ft.)
 End of street segment elevation = 1076.500 (Ft.)
 Length of street segment = 1000.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 20.000 (Ft.)
 Distance from crown to crossfall grade break = 18.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500 (Ft.)
 Gutter hike from flowline = 1.500 (In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 23.668 (CFS)
 Depth of flow = 0.477 (Ft.), Average velocity = 3.188 (Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 19.081 (Ft.)
 Flow velocity = 3.19 (Ft/s)
 Travel time = 5.23 min. TC = 18.38 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.098 (In/Hr)
 Rainfall intensity = 2.231 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.861
 Subarea runoff = 16.968 (CFS) for 10.000 (Ac.)
 Total runoff = 28.802 (CFS)
 Effective area this stream = 15.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 77.50 (Ac.)
 Area averaged Fm value = 0.098 (In/Hr)
 Street flow at end of street = 28.802 (CFS)
 Half street flow at end of street = 14.401 (CFS)
 Depth of flow = 0.504 (Ft.), Average velocity = 3.384 (Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000 (Ft.)

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 Process from Point/Station 214.000 to Point/Station 214.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 15.000 (Ac.)
 Runoff from this stream = 28.802 (CFS)
 Time of concentration = 18.38 min.

Rainfall intensity = 2.231(In/Hr)
 Area averaged loss rate (Fm) = 0.0978(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	90.852	19.75	2.137
2	32.397	17.95	2.263
3	28.802	18.38	2.231
Qmax(1) =			
	1.000 *	1.000 *	90.852) +
	0.942 *	1.000 *	32.397) +
	0.956 *	1.000 *	28.802) + = 148.904
Qmax(2) =			
	1.062 *	0.909 *	90.852) +
	1.000 *	1.000 *	32.397) +
	1.015 *	0.977 *	28.802) + = 148.612
Qmax(3) =			
	1.046 *	0.931 *	90.852) +
	0.985 *	1.000 *	32.397) +
	1.000 *	1.000 *	28.802) + = 149.169

Total of 3 streams to confluence:

Flow rates before confluence point:

90.852 32.397 28.802

Maximum flow rates at confluence using above data:

148.904 148.612 149.169

Area of streams before confluence:

44.584 16.500 15.000

Effective area values after confluence:

76.084 71.669 72.987

Results of confluence:

Total flow rate = 149.169(CFS)

Time of concentration = 18.379 min.

Effective stream area after confluence = 72.987(Ac.)

Stream Area average Pervious fraction(Ap) = 0.100

Stream Area average soil loss rate(Fm) = 0.091(In/Hr)

Study area (this main stream) = 76.08(Ac.)

++++++
 Process from Point/Station 62.000 to Point/Station 63.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1065.000(Ft.)
 Downstream point/station elevation = 1042.200(Ft.)
 Pipe length = 1320.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 149.169(CFS)
 Given pipe size = 54.00(In.)
 Calculated individual pipe flow = 149.169(CFS)
 Normal flow depth in pipe = 29.44(In.)
 Flow top width inside pipe = 53.78(In.)
 Critical Depth = 42.99(In.)
 Pipe flow velocity = 16.83(Ft/s)
 Travel time through pipe = 1.31 min.
 Time of concentration (TC) = 19.69 min.

```

+++++
Process from Point/Station      63.000 to Point/Station      63.000
**** CONFLUENCE OF MINOR STREAMS ****

```

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 72.987(Ac.)
 Runoff from this stream = 149.169(CFS)
 Time of concentration = 19.69 min.
 Rainfall intensity = 2.141(In/Hr)
 Area averaged loss rate (Fm) = 0.0914(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

```

+++++
Process from Point/Station      215.000 to Point/Station      216.000
**** INITIAL AREA EVALUATION ****

```

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1074.600(Ft.)
 Bottom (of initial area) elevation = 1071.000(Ft.)
 Difference in elevation = 3.600(Ft.)
 Slope = 0.00360 s(%)= 0.36
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 14.846 min.
 Rainfall intensity = 2.536(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.874
 Subarea runoff = 12.191(CFS)
 Total initial stream area = 5.500(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

```

+++++
Process from Point/Station      216.000 to Point/Station      217.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

```

Top of street segment elevation = 1071.000(Ft.)
 End of street segment elevation = 1063.700(Ft.)
 Length of street segment = 875.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 24.382(CFS)

Depth of flow = 0.491(Ft.), Average velocity = 3.058(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 19.786(Ft.)
 Flow velocity = 3.06(Ft/s)
 Travel time = 4.77 min. TC = 19.61 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.146(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.869
 Subarea runoff = 18.586(CFS) for 11.000(Ac.)
 Total runoff = 30.776(CFS)
 Effective area this stream = 16.50(Ac.)
 Total Study Area (Main Stream No. 1) = 94.00(Ac.)
 Area averaged Fm value = 0.073(In/Hr)
 Street flow at end of street = 30.776(CFS)
 Half street flow at end of street = 15.388(CFS)
 Depth of flow = 0.522(Ft.), Average velocity = 3.341(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++
 Process from Point/Station 217.000 to Point/Station 217.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 16.500(Ac.)
 Runoff from this stream = 30.776(CFS)
 Time of concentration = 19.61 min.
 Rainfall intensity = 2.146(In/Hr)
 Area averaged loss rate (Fm) = 0.0734(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

++++++
 Process from Point/Station 63.000 to Point/Station 63.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Soil classification AP and SCS values input by user
 USER INPUT of soil data for subarea
 SCS curve number for soil(AMC 2) = 54.95
 Pervious ratio(Ap) = 0.1110 Max loss rate(Fm)= 0.083(In/Hr)
 Rainfall intensity = 2.049(In/Hr) for a 25.0 year storm
 User specified values are as follows:
 TC = 21.19 min. Rain intensity = 2.05(In/Hr)
 Total area this stream = 203.15(Ac.)
 Total Study Area (Main Stream No. 1) = 297.15(Ac.)
 Total runoff = 403.88(CFS)

++++++
 Process from Point/Station 63.000 to Point/Station 63.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3

Stream flow area = 203.150(Ac.)

Runoff from this stream = 403.880(CFS)

Time of concentration = 21.19 min.

Rainfall intensity = 2.049(In/Hr)

Area averaged loss rate (Fm) = 0.0830(In/Hr)

Area averaged Pervious ratio (Ap) = 0.1110

Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	149.169	19.69	2.141
---	---------	-------	-------

2	30.776	19.61	2.146
---	--------	-------	-------

3	403.880	21.19	2.049
---	---------	-------	-------

Qmax(1) =

1.000 *	1.000 *	149.169) +	
0.998 *	1.000 *	30.776) +	
1.047 *	0.929 *	403.880) + =	572.752

Qmax(2) =

1.002 *	0.996 *	149.169) +	
1.000 *	1.000 *	30.776) +	
1.049 *	0.926 *	403.880) + =	572.081

Qmax(3) =

0.955 *	1.000 *	149.169) +	
0.953 *	1.000 *	30.776) +	
1.000 *	1.000 *	403.880) + =	575.650

Total of 3 streams to confluence:

Flow rates before confluence point:

149.169	30.776	403.880
---------	--------	---------

Maximum flow rates at confluence using above data:

572.752	572.081	575.650
---------	---------	---------

Area of streams before confluence:

72.987	16.500	203.150
--------	--------	---------

Effective area values after confluence:

278.220	277.266	292.637
---------	---------	---------

Results of confluence:

Total flow rate = 575.650(CFS)

Time of concentration = 21.190 min.

Effective stream area after confluence = 292.637(Ac.)

Stream Area average Pervious fraction(Ap) = 0.108

Stream Area average soil loss rate(Fm) = 0.085(In/Hr)

Study area (this main stream) = 292.64(Ac.)

+++++
 Process from Point/Station 63.000 to Point/Station 64.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1039.100(Ft.)

Downstream point/station elevation = 1033.800(Ft.)

Pipe length = 1320.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 575.650(CFS)

Given pipe size = 90.00(In.)

NOTE: Normal flow is pressure flow in user selected pipe size.

The approximate hydraulic grade line above the pipe invert is

6.071(Ft.) at the headworks or inlet of the pipe(s)

Pipe friction loss = 7.416(Ft.)

Minor friction loss = 3.955(Ft.) K-factor = 1.50

Pipe flow velocity = 13.03(Ft/s)
 Travel time through pipe = 1.69 min.
 Time of concentration (TC) = 22.88 min.

+++++
 Process from Point/Station 64.000 to Point/Station 64.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 292.637(Ac.)
 Runoff from this stream = 575.650(CFS)
 Time of concentration = 22.88 min.
 Rainfall intensity = 1.957(In/Hr)
 Area averaged loss rate (Fm) = 0.0845(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1076

+++++
 Process from Point/Station 218.000 to Point/Station 219.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1065.500(Ft.)
 Bottom (of initial area) elevation = 1059.000(Ft.)
 Difference in elevation = 6.500(Ft.)
 Slope = 0.00650 s(%)= 0.65
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 16.880 min.
 Rainfall intensity = 2.348(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.759
 Subarea runoff = 8.915(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

+++++
 Process from Point/Station 219.000 to Point/Station 220.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1059.000(Ft.)
 End of street segment elevation = 1056.500(Ft.)
 Length of street segment = 500.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)

Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 16.048(CFS)
 Depth of flow = 0.467(Ft.), Average velocity = 2.274(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 18.592(Ft.)
 Flow velocity = 2.27(Ft/s)
 Travel time = 3.66 min. TC = 20.54 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367(In/Hr)
 Rainfall intensity = 2.087(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.742
 Subarea runoff = 11.210(CFS) for 8.000(Ac.)
 Total runoff = 20.126(CFS)
 Effective area this stream = 13.00(Ac.)
 Total Study Area (Main Stream No. 1) = 310.15(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 20.126(CFS)
 Half street flow at end of street = 10.063(CFS)
 Depth of flow = 0.499(Ft.), Average velocity = 2.419(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000(Ft.)

++++++
 Process from Point/Station 220.000 to Point/Station 221.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1056.500(Ft.)
 End of street segment elevation = 1051.200(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 30.188(CFS)
 Depth of flow = 0.658(Ft.), Average velocity = 3.776(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 28.148(Ft.)
 Flow velocity = 3.78(Ft/s)
 Travel time = 2.91 min. TC = 23.46 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 1.927(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.729
 Subarea runoff = 16.391(CFS) for 13.000(Ac.)
 Total runoff = 36.516(CFS)
 Effective area this stream = 26.00(Ac.)
 Total Study Area (Main Stream No. 1) = 323.15(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 36.516(CFS)
 Half street flow at end of street = 36.516(CFS)
 Depth of flow = 0.708(Ft.), Average velocity = 3.842(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 2.06(Ft.)
 Flow width (from curb towards crown)= 30.644(Ft.)

++++++
 Process from Point/Station 221.000 to Point/Station 221.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 26.000(Ac.)
 Runoff from this stream = 36.516(CFS)
 Time of concentration = 23.46 min.
 Rainfall intensity = 1.927(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	575.650	22.88	1.957
2	36.516	23.46	1.927
Qmax(1) =	1.000 *	1.000 *	575.650) +
	1.019 *	0.975 *	36.516) + = 611.929
Qmax(2) =	0.984 *	1.000 *	575.650) +
	1.000 *	1.000 *	36.516) + = 603.223

Total of 2 streams to confluence:

Flow rates before confluence point:

575.650 36.516

Maximum flow rates at confluence using above data:

611.929 603.223

Area of streams before confluence:

292.637 26.000

Effective area values after confluence:

317.996 318.637

Results of confluence:

Total flow rate = 611.929(CFS)

Time of concentration = 22.878 min.

Effective stream area after confluence = 317.996(Ac.)

Stream Area average Pervious fraction(Ap) = 0.140
 Stream Area average soil loss rate(Fm) = 0.108(In/Hr)
 Study area (this main stream) = 318.64(Ac.)

+++++
 Process from Point/Station 64.000 to Point/Station 71.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1033.800(Ft.)
 Downstream point/station elevation = 1030.000(Ft.)
 Pipe length = 660.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 611.929(CFS)
 Given pipe size = 90.00(In.)
 Calculated individual pipe flow = 611.929(CFS)
 Normal flow depth in pipe = 78.75(In.)
 Flow top width inside pipe = 59.53(In.)
 Critical Depth = 76.01(In.)
 Pipe flow velocity = 14.94(Ft/s)
 Travel time through pipe = 0.74 min.
 Time of concentration (TC) = 23.61 min.

+++++
 Process from Point/Station 71.000 to Point/Station 71.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 317.996(Ac.)
 Runoff from this stream = 611.929(CFS)
 Time of concentration = 23.61 min.
 Rainfall intensity = 1.920(In/Hr)
 Area averaged loss rate (Fm) = 0.1076(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1397

+++++
 Process from Point/Station 71.000 to Point/Station 71.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Soil classification AP and SCS values input by user
 USER INPUT of soil data for subarea
 SCS curve number for soil(AMC 2) = 56.12
 Pervious ratio(Ap) = 0.4520 Max loss rate(Fm)= 0.331(In/Hr)
 Rainfall intensity = 1.822(In/Hr) for a 25.0 year storm
 User specified values are as follows:
 TC = 25.76 min. Rain intensity = 1.82(In/Hr)
 Total area this stream = 202.68(Ac.)
 Total Study Area (Main Stream No. 1) = 525.83(Ac.)
 Total runoff = 307.34(CFS)

+++++
 Process from Point/Station 71.000 to Point/Station 71.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 202.680(Ac.)
 Runoff from this stream = 307.340(CFS)
 Time of concentration = 25.76 min.
 Rainfall intensity = 1.822(In/Hr)

Area averaged loss rate (Fm) = 0.3310(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.4520
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	611.929	23.61	1.920
2	307.340	25.76	1.822

Qmax(1) =
 1.000 * 1.000 * 611.929) +
 1.065 * 0.917 * 307.340) + = 912.114

Qmax(2) =
 0.946 * 1.000 * 611.929) +
 1.000 * 1.000 * 307.340) + = 886.319

Total of 2 streams to confluence:

Flow rates before confluence point:

611.929 307.340

Maximum flow rates at confluence using above data:

912.114 886.319

Area of streams before confluence:

317.996 202.680

Effective area values after confluence:

503.799 520.676

Results of confluence:

Total flow rate = 912.114(CFS)

Time of concentration = 23.615 min.

Effective stream area after confluence = 503.799(Ac.)

Stream Area average Pervious fraction(Ap) = 0.261

Stream Area average soil loss rate(Fm) = 0.195(In/Hr)

Study area (this main stream) = 520.68(Ac.)

+++++
 Process from Point/Station 71.000 to Point/Station 89.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1030.000(Ft.)
 Downstream point/station elevation = 1025.000(Ft.)
 Pipe length = 680.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 912.114(CFS)
 Given pipe size = 108.00(In.)
 Calculated individual pipe flow = 912.114(CFS)
 Normal flow depth in pipe = 76.59(In.)
 Flow top width inside pipe = 98.09(In.)
 Critical Depth = 89.02(In.)
 Pipe flow velocity = 18.90(Ft/s)
 Travel time through pipe = 0.60 min.
 Time of concentration (TC) = 24.21 min.

+++++
 Process from Point/Station 89.000 to Point/Station 89.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 503.799(Ac.)
 Runoff from this stream = 912.114(CFS)
 Time of concentration = 24.21 min.

Rainfall intensity = 1.891(In/Hr)
 Area averaged loss rate (Fm) = 0.1946(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.2612

+++++
 Process from Point/Station 89.000 to Point/Station 89.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Soil classification AP and SCS values input by user
 USER INPUT of soil data for subarea
 SCS curve number for soil(AMC 2) = 74.49
 Pervious ratio(Ap) = 0.8260 Max loss rate(Fm)= 0.381(In/Hr)
 Rainfall intensity = 2.805(In/Hr) for a 25.0 year storm
 User specified values are as follows:
 TC = 12.55 min. Rain intensity = 2.81(In/Hr)
 Total area this stream = 316.80(Ac.)
 Total Study Area (Main Stream No. 1) = 842.63(Ac.)
 Total runoff = 795.18(CFS)

+++++
 Process from Point/Station 89.000 to Point/Station 89.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 316.800(Ac.)
 Runoff from this stream = 795.180(CFS)
 Time of concentration = 12.55 min.
 Rainfall intensity = 2.805(In/Hr)
 Area averaged loss rate (Fm) = 0.3810(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.8260
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	912.114	24.21	1.891
2	795.180	12.55	2.805
Qmax(1) =			
	1.000 *	1.000 *	912.114) +
	0.623 *	1.000 *	795.180) + = 1407.437
Qmax(2) =			
	1.539 *	0.518 *	912.114) +
	1.000 *	1.000 *	795.180) + = 1522.641

Total of 2 streams to confluence:
 Flow rates before confluence point:
 912.114 795.180
 Maximum flow rates at confluence using above data:
 1407.437 1522.641
 Area of streams before confluence:
 503.799 316.800
 Effective area values after confluence:
 820.599 577.909
 Results of confluence:
 Total flow rate = 1522.641(CFS)
 Time of concentration = 12.550 min.
 Effective stream area after confluence = 577.909(Ac.)
 Stream Area average Pervious fraction(Ap) = 0.479

Stream Area average soil loss rate(Fm) = 0.267(In/Hr)
Study area (this main stream) = 820.60(Ac.)
End of computations, Total Study Area = 842.63 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.
Note: These figures do not consider reduced effective area
effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.473
Area averaged SCS curve number = 61.1

LINE "DZ-4"

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
 Rational Hydrology Study Date: 08/03/04

 FONTANA / LINE DZ-4 HYDROLOGY
 25 YEAR STORM
 JN 04339

 Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

 Rational hydrology study storm event year is 25.0
 10 Year storm 1 hour rainfall = 0.930(In.)
 100 Year storm 1 hour rainfall = 1.350(In.)
 Computed rainfall intensity:
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)
 Slope used for rainfall intensity curve b = 0.6000
 Soil antecedent moisture condition (AMC) = 2

 Process from Point/Station 600.000 to Point/Station 601.000
 **** INITIAL AREA EVALUATION ****

 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1065.000(Ft.)
 Bottom (of initial area) elevation = 1060.000(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.902 min.
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875
 Subarea runoff = 11.541(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

 Process from Point/Station 601.000 to Point/Station 602.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

 Top of street segment elevation = 1060.000(Ft.)
 End of street segment elevation = 1058.300(Ft.)

Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 17.312(CFS)
 Depth of flow = 0.476(Ft.), Average velocity = 2.344(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 19.032(Ft.)
 Flow velocity = 2.34(Ft/s)
 Travel time = 2.35 min. TC = 16.25 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)
 Rainfall intensity = 2.402(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.873
 Subarea runoff = 9.420(CFS) for 5.000(Ac.)
 Total runoff = 20.962(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 10.00(Ac.)
 Area averaged Fm value = 0.073(In/Hr)
 Street flow at end of street = 20.962(CFS)
 Half street flow at end of street = 10.481(CFS)
 Depth of flow = 0.503(Ft.), Average velocity = 2.480(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++
 Process from Point/Station 602.000 to Point/Station 603.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1058.300(Ft.)
 End of street segment elevation = 1055.000(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)

Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 31.443 (CFS)
 Depth of flow = 0.564 (Ft.), Average velocity = 2.888 (Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000 (Ft.)
 Flow velocity = 2.89 (Ft/s)
 Travel time = 3.81 min. TC = 20.06 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 56.00
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.073 (In/Hr)
 Rainfall intensity = 2.117 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.869
 Subarea runoff = 15.828 (CFS) for 10.000 (Ac.)
 Total runoff = 36.790 (CFS)
 Effective area this stream = 20.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 20.00 (Ac.)
 Area averaged Fm value = 0.073 (In/Hr)
 Street flow at end of street = 36.790 (CFS)
 Half street flow at end of street = 18.395 (CFS)
 Depth of flow = 0.591 (Ft.), Average velocity = 3.073 (Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000 (Ft.)

++++++
 Process from Point/Station 603.000 to Point/Station 607.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1055.000 (Ft.)
 End of street segment elevation = 1052.000 (Ft.)
 Length of street segment = 660.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 42.000 (Ft.)
 Distance from crown to crossfall grade break = 40.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500 (Ft.)
 Gutter hike from flowline = 1.500 (In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 36.790 (CFS)
 Depth of flow = 0.784 (Ft.), Average velocity = 2.991 (Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 5.89 (Ft.)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 34.469 (Ft.)
 Flow velocity = 2.99 (Ft/s)

Travel time = 3.68 min. TC = 23.74 min.

Adding area flow to street

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 56.00

Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073(In/Hr)

Rainfall intensity = 1.914(In/Hr) for a 25.0 year storm

Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.865

Subarea runoff = 0.000(CFS) for 0.000(Ac.)

Total runoff = 36.790(CFS)

Effective area this stream = 20.00(Ac.)

Total Study Area (Main Stream No. 1) = 20.00(Ac.)

Area averaged Fm value = 0.073(In/Hr)

Street flow at end of street = 36.790(CFS)

Half street flow at end of street = 36.790(CFS)

Depth of flow = 0.784(Ft.), Average velocity = 2.991(Ft/s)

Warning: depth of flow exceeds top of curb

Distance that curb overflow reaches into property = 5.89(Ft.)

Flow width (from curb towards crown) = 34.469(Ft.)

Process from Point/Station 607.000 to Point/Station 607.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 20.000(Ac.)

Runoff from this stream = 36.790(CFS)

Time of concentration = 23.74 min.

Rainfall intensity = 1.914(In/Hr)

Area averaged loss rate (Fm) = 0.0734(In/Hr)

Area averaged Pervious ratio (Ap) = 0.1000

Process from Point/Station 604.000 to Point/Station 605.000
**** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 56.00

Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073(In/Hr)

Initial subarea data:

Initial area flow distance = 1000.000(Ft.)

Top (of initial area) elevation = 1062.900(Ft.)

Bottom (of initial area) elevation = 1057.900(Ft.)

Difference in elevation = 5.000(Ft.)

Slope = 0.00500 s(%) = 0.50

TC = $k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$

Initial area time of concentration = 13.902 min.

Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm

Effective runoff coefficient used for area (Q=KCIA) is C = 0.875

Subarea runoff = 11.541(CFS)

Total initial stream area = 5.000 (Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073 (In/Hr)

 Process from Point/Station 605.000 to Point/Station 606.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1057.900 (Ft.)
 End of street segment elevation = 1055.900 (Ft.)
 Length of street segment = 330.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 20.000 (Ft.)
 Distance from crown to crossfall grade break = 18.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500 (Ft.)
 Gutter hike from flowline = 1.500 (In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 17.312 (CFS)
 Depth of flow = 0.464 (Ft.), Average velocity = 2.492 (Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 18.447 (Ft.)
 Flow velocity = 2.49 (Ft/s)
 Travel time = 2.21 min. TC = 16.11 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 56.00
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.073 (In/Hr)
 Rainfall intensity = 2.415 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.873
 Subarea runoff = 9.532 (CFS) for 5.000 (Ac.)
 Total runoff = 21.074 (CFS)
 Effective area this stream = 10.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 30.00 (Ac.)
 Area averaged Fm value = 0.073 (In/Hr)
 Street flow at end of street = 21.074 (CFS)
 Half street flow at end of street = 10.537 (CFS)
 Depth of flow = 0.493 (Ft.), Average velocity = 2.616 (Ft/s)
 Flow width (from curb towards crown) = 19.892 (Ft.)

 Process from Point/Station 606.000 to Point/Station 607.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1055.900 (Ft.)
 End of street segment elevation = 1052.000 (Ft.)
 Length of street segment = 660.000 (Ft.)

Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 31.611(CFS)
 Depth of flow = 0.551(Ft.), Average velocity = 3.043(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 3.04(Ft/s)
 Travel time = 3.61 min. TC = 19.72 min.
 Adding area flow to street
 CONDOMINIUM subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm) = 0.257(In/Hr)
 Rainfall intensity = 2.139(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.831
 Subarea runoff = 14.451(CFS) for 10.000(Ac.)
 Total runoff = 35.524(CFS)
 Effective area this stream = 20.00(Ac.)
 Total Study Area (Main Stream No. 1) = 40.00(Ac.)
 Area averaged Fm value = 0.165(In/Hr)
 Street flow at end of street = 35.524(CFS)
 Half street flow at end of street = 17.762(CFS)
 Depth of flow = 0.570(Ft.), Average velocity = 3.187(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000(Ft.)

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 Process from Point/Station 607.000 to Point/Station 607.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 20.000(Ac.)
 Runoff from this stream = 35.524(CFS)
 Time of concentration = 19.72 min.
 Rainfall intensity = 2.139(In/Hr)
 Area averaged loss rate (Fm) = 0.1651(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.2250
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	36.790	23.74	1.914
2	35.524	19.72	2.139

Qmax(1) =

1.000 *	1.000 *	36.790) +	
0.886 *	1.000 *	35.524) + =	68.267

Qmax(2) =

1.122 *	0.831 *	36.790) +	
1.000 *	1.000 *	35.524) + =	69.831

Total of 2 streams to confluence:

Flow rates before confluence point:

36.790 35.524

Maximum flow rates at confluence using above data:

68.267 69.831

Area of streams before confluence:

20.000 20.000

Effective area values after confluence:

40.000 36.620

Results of confluence:

Total flow rate = 69.831(CFS)

Time of concentration = 19.724 min.

Effective stream area after confluence = 36.620(Ac.)

Stream Area average Pervious fraction(Ap) = 0.163

Stream Area average soil loss rate(Fm) = 0.119(In/Hr)

Study area (this main stream) = 40.00(Ac.)

 Process from Point/Station 607.000 to Point/Station 45.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1047.000(Ft.)
 Downstream point/station elevation = 1041.000(Ft.)
 Pipe length = 660.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 69.831(CFS)
 Given pipe size = 42.00(In.)
 Calculated individual pipe flow = 69.831(CFS)
 Normal flow depth in pipe = 26.58(In.)
 Flow top width inside pipe = 40.49(In.)
 Critical Depth = 31.40(In.)
 Pipe flow velocity = 10.88(Ft/s)
 Travel time through pipe = 1.01 min.
 Time of concentration (TC) = 20.74 min.

 Process from Point/Station 45.000 to Point/Station 45.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 36.620(Ac.)
 Runoff from this stream = 69.831(CFS)
 Time of concentration = 20.74 min.
 Rainfall intensity = 2.075(In/Hr)
 Area averaged loss rate (Fm) = 0.1193(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1625

 Process from Point/Station 608.000 to Point/Station 609.000

**** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1060.800(Ft.)
 Bottom (of initial area) elevation = 1055.800(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.902 min.
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875
 Subarea runoff = 11.541(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073(In/Hr)

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 Process from Point/Station 609.000 to Point/Station 610.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1055.800(Ft.)
 End of street segment elevation = 1053.500(Ft.)
 Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 17.312(CFS)
 Depth of flow = 0.454(Ft.), Average velocity = 2.626(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 17.958(Ft.)
 Flow velocity = 2.63(Ft/s)
 Travel time = 2.09 min. TC = 16.00 min.

Adding area flow to street

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073(In/Hr)
 Rainfall intensity = 2.425(In/Hr) for a 25.0 year storm

Effective runoff coefficient used for area, (total area with modified rational method) ($Q=KCIA$) is $C = 0.873$
 Subarea runoff = 9.624 (CFS) for 5.000 (Ac.)
 Total runoff = 21.166 (CFS)
 Effective area this stream = 10.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 50.00 (Ac.)
 Area averaged F_m value = 0.073 (In/Hr)
 Street flow at end of street = 21.166 (CFS)
 Half street flow at end of street = 10.583 (CFS)
 Depth of flow = 0.483 (Ft.), Average velocity = 2.760 (Ft/s)
 Flow width (from curb towards crown) = 19.399 (Ft.)

 Process from Point/Station 610.000 to Point/Station 611.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1053.500 (Ft.)
 End of street segment elevation = 1049.000 (Ft.)
 Length of street segment = 660.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 20.000 (Ft.)
 Distance from crown to crossfall grade break = 18.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500 (Ft.)
 Gutter hike from flowline = 1.500 (In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 31.749 (CFS)
 Depth of flow = 0.541 (Ft.), Average velocity = 3.183 (Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000 (Ft.)
 Flow velocity = 3.18 (Ft/s)
 Travel time = 3.46 min. TC = 19.45 min.
 Adding area flow to street
 CONDOMINIUM subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 56.00
 Pervious ratio (A_p) = 0.3500 Max loss rate (F_m) = 0.257 (In/Hr)
 Rainfall intensity = 2.157 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified rational method) ($Q=KCIA$) is $C = 0.831$
 Subarea runoff = 14.680 (CFS) for 10.000 (Ac.)
 Total runoff = 35.846 (CFS)
 Effective area this stream = 20.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 60.00 (Ac.)
 Area averaged F_m value = 0.165 (In/Hr)
 Street flow at end of street = 35.846 (CFS)
 Half street flow at end of street = 17.923 (CFS)
 Depth of flow = 0.560 (Ft.), Average velocity = 3.340 (Ft/s)
 Note: depth of flow exceeds top of street crown.

Flow width (from curb towards crown) = 20.000 (Ft.)

 Process from Point/Station 611.000 to Point/Station 611.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 20.000 (Ac.)
 Runoff from this stream = 35.846 (CFS)
 Time of concentration = 19.45 min.
 Rainfall intensity = 2.157 (In/Hr)
 Area averaged loss rate (Fm) = 0.1651 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.2250
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	69.831	20.74	2.075
2	35.846	19.45	2.157
Qmax(1) =			
	1.000 *	1.000 *	69.831) +
	0.959 *	1.000 *	35.846) + = 104.218
Qmax(2) =			
	1.041 *	0.938 *	69.831) +
	1.000 *	1.000 *	35.846) + = 104.072

Total of 2 streams to confluence:

Flow rates before confluence point:

69.831 35.846

Maximum flow rates at confluence using above data:

104.218 104.072

Area of streams before confluence:

36.620 20.000

Effective area values after confluence:

56.620 54.354

Results of confluence:

Total flow rate = 104.218 (CFS)

Time of concentration = 20.736 min.

Effective stream area after confluence = 56.620 (Ac.)

Stream Area average Pervious fraction (Ap) = 0.185

Stream Area average soil loss rate (Fm) = 0.135 (In/Hr)

Study area (this main stream) = 56.62 (Ac.)

 Process from Point/Station 45.000 to Point/Station 90.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1040.000 (Ft.)
 Downstream point/station elevation = 1025.000 (Ft.)
 Pipe length = 750.00 (Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 104.218 (CFS)
 Given pipe size = 54.00 (In.)
 Calculated individual pipe flow = 104.218 (CFS)
 Normal flow depth in pipe = 22.90 (In.)
 Flow top width inside pipe = 53.37 (In.)
 Critical Depth = 35.99 (In.)

Pipe flow velocity = 16.23 (Ft/s)
 Travel time through pipe = 0.77 min.
 Time of concentration (TC) = 21.51 min.

 Process from Point/Station 90.000 to Point/Station 90.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 56.620 (Ac.)
 Runoff from this stream = 104.218 (CFS)
 Time of concentration = 21.51 min.
 Rainfall intensity = 2.031 (In/Hr)
 Area averaged loss rate (Fm) = 0.1355 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1846

 Process from Point/Station 612.000 to Point/Station 613.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 56.00
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.073 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000 (Ft.)
 Top (of initial area) elevation = 1058.700 (Ft.)
 Bottom (of initial area) elevation = 1053.700 (Ft.)
 Difference in elevation = 5.000 (Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.902 min.
 Rainfall intensity = 2.638 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875
 Subarea runoff = 11.541 (CFS)
 Total initial stream area = 5.000 (Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.073 (In/Hr)

 Process from Point/Station 613.000 to Point/Station 614.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1053.700 (Ft.)
 End of street segment elevation = 1051.100 (Ft.)
 Length of street segment = 330.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 20.000 (Ft.)
 Distance from crown to crossfall grade break = 18.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020

Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 17.312(CFS)
 Depth of flow = 0.446(Ft.), Average velocity = 2.750(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 17.539(Ft.)
 Flow velocity = 2.75(Ft/s)
 Travel time = 2.00 min. TC = 15.90 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073(In/Hr)
 Rainfall intensity = 2.434(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.873
 Subarea runoff = 9.702(CFS) for 5.000(Ac.)
 Total runoff = 21.244(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 70.00(Ac.)
 Area averaged Fm value = 0.073(In/Hr)
 Street flow at end of street = 21.244(CFS)
 Half street flow at end of street = 10.622(CFS)
 Depth of flow = 0.474(Ft.), Average velocity = 2.893(Ft/s)
 Flow width (from curb towards crown) = 18.975(Ft.)

++++++
 Process from Point/Station 614.000 to Point/Station 615.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1051.100(Ft.)
 End of street segment elevation = 1046.000(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 31.865(CFS)
 Depth of flow = 0.532(Ft.), Average velocity = 3.310(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 3.31(Ft/s)
 Travel time = 3.32 min. TC = 19.23 min.

Adding area flow to street

CONDOMINIUM subarea type

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000

SCS curve number for soil (AMC 2) = 56.00

Pervious ratio (Ap) = 0.3500 Max loss rate (Fm) = 0.257 (In/Hr)

Rainfall intensity = 2.172 (In/Hr) for a 25.0 year storm

Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.832

Subarea runoff = 14.877 (CFS) for 10.000 (Ac.)

Total runoff = 36.121 (CFS)

Effective area this stream = 20.00 (Ac.)

Total Study Area (Main Stream No. 1) = 80.00 (Ac.)

Area averaged Fm value = 0.165 (In/Hr)

Street flow at end of street = 36.121 (CFS)

Half street flow at end of street = 18.060 (CFS)

Depth of flow = 0.551 (Ft.), Average velocity = 3.479 (Ft/s)

Note: depth of flow exceeds top of street crown.

Flow width (from curb towards crown) = 20.000 (Ft.)

+++++
Process from Point/Station 615.000 to Point/Station 615.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 20.000 (Ac.)

Runoff from this stream = 36.121 (CFS)

Time of concentration = 19.23 min.

Rainfall intensity = 2.172 (In/Hr)

Area averaged loss rate (Fm) = 0.1651 (In/Hr)

Area averaged Pervious ratio (Ap) = 0.2250

Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	104.218	21.51	2.031
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2	36.121	19.23	2.172
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Qmax(1) =

1.000 * 1.000 * 104.218) +
0.930 * 1.000 * 36.121) + = 137.795

Qmax(2) =

1.075 * 0.894 * 104.218) +
1.000 * 1.000 * 36.121) + = 136.232

Total of 2 streams to confluence:

Flow rates before confluence point:

104.218 36.121

Maximum flow rates at confluence using above data:

137.795 136.232

Area of streams before confluence:

56.620 20.000

Effective area values after confluence:

76.620 70.615

Results of confluence:

Total flow rate = 137.795 (CFS)

Time of concentration = 21.506 min.
Effective stream area after confluence = 76.620 (Ac.)
Stream Area average Pervious fraction(A_p) = 0.195
Stream Area average soil loss rate(F_m) = 0.143 (In/Hr)
Study area (this main stream) = 76.62 (Ac.)
End of computations, Total Study Area = 80.00 (Ac.)

The following figures may
be used for a unit hydrograph study of the same area.
Note: These figures do not consider reduced effective area
effects caused by confluences in the rational equation.

Area averaged pervious area fraction(A_p) = 0.194
Area averaged SCS curve number = 56.0

LINE "DZ-4A"

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
 Rational Hydrology Study Date: 08/03/04

 FONTANA / LINE DZ-4A HYDROLOGY
 25 YEAR STORM
 JN 04339

 Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

 Rational hydrology study storm event year is 25.0
 10 Year storm 1 hour rainfall = 0.930(In.)
 100 Year storm 1 hour rainfall = 1.350(In.)
 Computed rainfall intensity:
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)
 Slope used for rainfall intensity curve b = 0.6000
 Soil antecedent moisture condition (AMC) = 2

 Process from Point/Station 625.000 to Point/Station 626.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1058.000(Ft.)
 Bottom (of initial area) elevation = 1051.300(Ft.)
 Difference in elevation = 6.700(Ft.)
 Slope = 0.00670 s(%) = 0.67
 $TC = k(0.389) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 16.778 min.
 Rainfall intensity = 2.357(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.760
 Subarea runoff = 8.954(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

 Process from Point/Station 626.000 to Point/Station 627.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

 Top of street segment elevation = 1051.300(Ft.)
 End of street segment elevation = 1049.000(Ft.)

Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 13.431(CFS)
 Depth of flow = 0.421(Ft.), Average velocity = 2.467(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 16.282(Ft.)
 Flow velocity = 2.47(Ft/s)
 Travel time = 2.23 min. TC = 19.01 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 2.187(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.749
 Subarea runoff = 7.424(CFS) for 5.000(Ac.)
 Total runoff = 16.378(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 10.00(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 16.378(CFS)
 Half street flow at end of street = 8.189(CFS)
 Depth of flow = 0.447(Ft.), Average velocity = 2.591(Ft/s)
 Flow width (from curb towards crown)= 17.578(Ft.)

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 Process from Point/Station 627.000 to Point/Station 628.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1049.000(Ft.)
 End of street segment elevation = 1044.600(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150

Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 24.567(CFS)
 Depth of flow = 0.507(Ft.), Average velocity = 2.855(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 2.86(Ft/s)
 Travel time = 3.85 min. TC = 22.86 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367(In/Hr)
 Rainfall intensity = 1.958(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.731
 Subarea runoff = 12.252(CFS) for 10.000(Ac.)
 Total runoff = 28.630(CFS)
 Effective area this stream = 20.00(Ac.)
 Total Study Area (Main Stream No. 1) = 20.00(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 28.630(CFS)
 Half street flow at end of street = 14.315(CFS)
 Depth of flow = 0.527(Ft.), Average velocity = 3.034(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000(Ft.)

++++++
 Process from Point/Station 628.000 to Point/Station 629.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1044.600(Ft.)
 End of street segment elevation = 1040.300(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 42.945(CFS)
 Depth of flow = 0.778(Ft.), Average velocity = 3.568(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 5.56(Ft.)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 34.140(Ft.)
 Flow velocity = 3.57(Ft/s)
 Travel time = 3.08 min. TC = 25.94 min.

Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(A_p) = 0.5000 Max loss rate(F_m) = 0.367(In/Hr)
 Rainfall intensity = 1.814(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) ($Q=KCIA$) is $C = 0.718$
 Subarea runoff = 23.479(CFS) for 20.000(Ac.)
 Total runoff = 52.109(CFS)
 Effective area this stream = 40.00(Ac.)
 Total Study Area (Main Stream No. 1) = 40.00(Ac.)
 Area averaged F_m value = 0.367(In/Hr)
 Street flow at end of street = 52.109(CFS)
 Half street flow at end of street = 52.109(CFS)
 Depth of flow = 0.828(Ft.), Average velocity = 3.678(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 8.08(Ft.)
 Flow width (from curb towards crown) = 36.667(Ft.)

 Process from Point/Station 629.000 to Point/Station 46.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1033.300(Ft.)
 Downstream point/station elevation = 1026.000(Ft.)
 Pipe length = 660.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 52.109(CFS)
 Given pipe size = 36.00(In.)
 Calculated individual pipe flow = 52.109(CFS)
 Normal flow depth in pipe = 23.11(In.)
 Flow top width inside pipe = 34.52(In.)
 Critical Depth = 28.15(In.)
 Pipe flow velocity = 10.87(Ft/s)
 Travel time through pipe = 1.01 min.
 Time of concentration (TC) = 26.95 min.

 Process from Point/Station 629.000 to Point/Station 46.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 40.000(Ac.)
 Runoff from this stream = 52.109(CFS)
 Time of concentration = 26.95 min.
 Rainfall intensity = 1.773(In/Hr)
 Area averaged loss rate (F_m) = 0.3670(In/Hr)
 Area averaged Pervious ratio (A_p) = 0.5000

 Process from Point/Station 630.000 to Point/Station 631.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1052.200(Ft.)
 Bottom (of initial area) elevation = 1044.000(Ft.)
 Difference in elevation = 8.200(Ft.)
 Slope = 0.00820 s(%) = 0.82
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 16.113 min.
 Rainfall intensity = 2.415(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.763
 Subarea runoff = 9.214(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

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 Process from Point/Station 631.000 to Point/Station 632.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1044.000(Ft.)
 End of street segment elevation = 1041.300(Ft.)
 Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 13.821(CFS)
 Depth of flow = 0.414(Ft.), Average velocity = 2.639(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 15.960(Ft.)
 Flow velocity = 2.64(Ft/s)
 Travel time = 2.08 min. TC = 18.20 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367(In/Hr)
 Rainfall intensity = 2.245(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.753
 Subarea runoff = 7.685(CFS) for 5.000(Ac.)

Total runoff = 16.899 (CFS)
 Effective area this stream = 10.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 50.00 (Ac.)
 Area averaged Fm value = 0.367 (In/Hr)
 Street flow at end of street = 16.899 (CFS)
 Half street flow at end of street = 8.449 (CFS)
 Depth of flow = 0.440 (Ft.), Average velocity = 2.773 (Ft/s)
 Flow width (from curb towards crown) = 17.250 (Ft.)

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 Process from Point/Station 632.000 to Point/Station 633.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1041.300 (Ft.)
 End of street segment elevation = 1035.900 (Ft.)
 Length of street segment = 660.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 20.000 (Ft.)
 Distance from crown to crossfall grade break = 18.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500 (Ft.)
 Gutter hike from flowline = 1.500 (In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 25.348 (CFS)
 Depth of flow = 0.498 (Ft.), Average velocity = 3.075 (Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000 (Ft.)
 Flow velocity = 3.07 (Ft/s)
 Travel time = 3.58 min. TC = 21.77 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367 (In/Hr)
 Rainfall intensity = 2.015 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.736
 Subarea runoff = 12.774 (CFS) for 10.000 (Ac.)
 Total runoff = 29.673 (CFS)
 Effective area this stream = 20.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 60.00 (Ac.)
 Area averaged Fm value = 0.367 (In/Hr)
 Street flow at end of street = 29.673 (CFS)
 Half street flow at end of street = 14.837 (CFS)
 Depth of flow = 0.518 (Ft.), Average velocity = 3.273 (Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000 (Ft.)

 Process from Point/Station 633.000 to Point/Station 633.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 20.000 (Ac.)
 Runoff from this stream = 29.673 (CFS)
 Time of concentration = 21.77 min.
 Rainfall intensity = 2.015 (In/Hr)
 Area averaged loss rate (Fm) = 0.3670 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	52.109	26.95	1.773
2	29.673	21.77	2.015

Qmax(1) =
 1.000 * 1.000 * 52.109) +
 0.853 * 1.000 * 29.673) + = 77.421

Qmax(2) =
 1.172 * 0.808 * 52.109) +
 1.000 * 1.000 * 29.673) + = 79.019

Total of 2 streams to confluence:
 Flow rates before confluence point:
 52.109 29.673
 Maximum flow rates at confluence using above data:
 77.421 79.019
 Area of streams before confluence:
 40.000 20.000
 Effective area values after confluence:
 60.000 52.313

Results of confluence:
 Total flow rate = 79.019 (CFS)
 Time of concentration = 21.775 min.
 Effective stream area after confluence = 52.313 (Ac.)
 Stream Area average Pervious fraction (Ap) = 0.500
 Stream Area average soil loss rate (Fm) = 0.367 (In/Hr)
 Study area (this main stream) = 60.00 (Ac.)

 Process from Point/Station 46.000 to Point/Station 91.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1026.000 (Ft.)
 Downstream point/station elevation = 1014.500 (Ft.)
 Pipe length = 750.00 (Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 79.019 (CFS)
 Given pipe size = 60.00 (In.)
 Calculated individual pipe flow = 79.019 (CFS)
 Normal flow depth in pipe = 20.23 (In.)
 Flow top width inside pipe = 56.73 (In.)
 Critical Depth = 30.19 (In.)
 Pipe flow velocity = 13.58 (Ft/s)
 Travel time through pipe = 0.92 min.
 Time of concentration (TC) = 22.70 min.


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Process from Point/Station      91.000 to Point/Station      91.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 52.313 (Ac.)
 Runoff from this stream = 79.019 (CFS)
 Time of concentration = 22.70 min.
 Rainfall intensity = 1.966 (In/Hr)
 Area averaged loss rate (Fm) = 0.3670 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000

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+++++
Process from Point/Station      634.000 to Point/Station      635.000
**** INITIAL AREA EVALUATION ****

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RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000 (Ft.)
 Top (of initial area) elevation = 1046.800 (Ft.)
 Bottom (of initial area) elevation = 1041.800 (Ft.)
 Difference in elevation = 5.000 (Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.389) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 10.306 (CFS)
 Total initial stream area = 6.000 (Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367 (In/Hr)

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+++++
Process from Point/Station      635.000 to Point/Station      636.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

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Top of street segment elevation = 1041.800 (Ft.)
 End of street segment elevation = 1037.800 (Ft.)
 Length of street segment = 330.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 20.000 (Ft.)
 Distance from crown to crossfall grade break = 18.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500 (Ft.)
 Gutter hike from flowline = 1.500 (In.)
 Manning's N in gutter = 0.0150

Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 15.458 (CFS)
 Depth of flow = 0.404 (Ft.), Average velocity = 3.146 (Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 15.445 (Ft.)
 Flow velocity = 3.15 (Ft/s)
 Travel time = 1.75 min. TC = 19.54 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwt/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367 (In/Hr)
 Rainfall intensity = 2.151 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.746
 Subarea runoff = 8.962 (CFS) for 6.000 (Ac.)
 Total runoff = 19.267 (CFS)
 Effective area this stream = 12.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 72.00 (Ac.)
 Area averaged Fm value = 0.367 (In/Hr)
 Street flow at end of street = 19.267 (CFS)
 Half street flow at end of street = 9.634 (CFS)
 Depth of flow = 0.431 (Ft.), Average velocity = 3.321 (Ft/s)
 Flow width (from curb towards crown) = 16.820 (Ft.)

++++++
 Process from Point/Station 636.000 to Point/Station 637.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1037.800 (Ft.)
 End of street segment elevation = 1031.000 (Ft.)
 Length of street segment = 660.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 20.000 (Ft.)
 Distance from crown to crossfall grade break = 18.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500 (Ft.)
 Gutter hike from flowline = 1.500 (In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 28.098 (CFS)
 Depth of flow = 0.496 (Ft.), Average velocity = 3.434 (Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000 (Ft.)
 Flow velocity = 3.43 (Ft/s)
 Travel time = 3.20 min. TC = 22.74 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwt/acre)
 Decimal fraction soil group A = 1.000

Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
 Rainfall intensity = 1.964(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.705
 Subarea runoff = 12.577(CFS) for 11.000(Ac.)
 Total runoff = 31.844(CFS)
 Effective area this stream = 23.00(Ac.)
 Total Study Area (Main Stream No. 1) = 83.00(Ac.)
 Area averaged Fm value = 0.425(In/Hr)
 Street flow at end of street = 31.844(CFS)
 Half street flow at end of street = 15.922(CFS)
 Depth of flow = 0.512(Ft.), Average velocity = 3.609(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++
 Process from Point/Station 637.000 to Point/Station 637.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 23.000(Ac.)
 Runoff from this stream = 31.844(CFS)
 Time of concentration = 22.74 min.
 Rainfall intensity = 1.964(In/Hr)
 Area averaged loss rate (Fm) = 0.4253(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	79.019	22.70	1.966
2	31.844	22.74	1.964

Qmax(1) =
 1.000 * 1.000 * 79.019) +
 1.002 * 0.998 * 31.844) + = 110.848
 Qmax(2) =
 0.999 * 1.000 * 79.019) +
 1.000 * 1.000 * 31.844) + = 110.747

Total of 2 streams to confluence:

Flow rates before confluence point:

79.019 31.844

Maximum flow rates at confluence using above data:

110.848 110.747

Area of streams before confluence:

52.313 23.000

Effective area values after confluence:

75.267 75.313

Results of confluence:

Total flow rate = 110.848(CFS)

Time of concentration = 22.696 min.

Effective stream area after confluence = 75.267(Ac.)

Stream Area average Pervious fraction(Ap) = 0.500

Stream Area average soil loss rate(Fm) = 0.385(In/Hr)
Study area (this main stream) = 75.31(Ac.)
End of computations, Total Study Area = 83.00 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.
Note: These figures do not consider reduced effective area
effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.500
Area averaged SCS curve number = 52.8

LINE "14'x9'RCB"

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
 Rational Hydrology Study Date: 01/13/05

FONTANA / LINE JURUPA AVE. 14'X 9' RCB HYDROLOGY
 25 YEAR STORM
 JN 04339

Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 25.0
 10 Year storm 1 hour rainfall = 0.930(In.)
 100 Year storm 1 hour rainfall = 1.350(In.)
 Computed rainfall intensity:
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)
 Slope used for rainfall intensity curve b = 0.6000
 Soil antecedent moisture condition (AMC) = 2

 Process from Point/Station 89.000 to Point/Station 89.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Soil classification AP and SCS values input by user
 USER INPUT of soil data for subarea
 SCS curve number for soil(AMC 2) = 68.38
 Pervious ratio(Ap) = 0.4790 Max loss rate(Fm)= 0.267(In/Hr)
 Rainfall intensity = 2.805(In/Hr) for a 25.0 year storm
 User specified values are as follows:
 TC = 12.55 min. Rain intensity = 2.81(In/Hr)
 Total area this stream = 577.91(Ac.)
 Total Study Area (Main Stream No. 1) = 577.91(Ac.)
 Total runoff = 1522.64(CFS)

 Process from Point/Station 89.000 to Point/Station 90.000
 **** IMPROVED CHANNEL TRAVEL TIME ****

Covered channel
 Upstream point elevation = 1028.200(Ft.)
 Downstream point elevation = 1022.300(Ft.)
 Channel length thru subarea = 1320.000(Ft.)
 Channel base width = 14.000(Ft.)
 Slope or 'Z' of left channel bank = 0.000
 Slope or 'Z' of right channel bank = 0.000
 Manning's 'N' = 0.015
 Maximum depth of channel = 9.000(Ft.)
 Flow(q) thru subarea = 1522.640(CFS)
 Depth of flow = 7.092(Ft.), Average velocity = 15.335(Ft/s)
 Channel flow top width = 14.000(Ft.)
 Flow Velocity = 15.33(Ft/s)
 Travel time = 1.43 min.

Time of concentration = 13.98 min.
Critical depth = 7.125(Ft.)

+++++
Process from Point/Station 90.000 to Point/Station 90.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 577.910(Ac.)
Runoff from this stream = 1522.640(CFS)
Time of concentration = 13.98 min.
Rainfall intensity = 2.629(In/Hr)
Area averaged loss rate (Fm) = 0.2670(In/Hr)
Area averaged Pervious ratio (Ap) = 0.4790

+++++
Process from Point/Station 90.000 to Point/Station 90.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Soil classification AP and SCS values input by user
USER INPUT of soil data for subarea
SCS curve number for soil(AMC 2) = 56.05
Pervious ratio(Ap) = 0.1950 Max loss rate(Fm)= 0.143(In/Hr)
Rainfall intensity = 2.030(In/Hr) for a 25.0 year storm
User specified values are as follows:
TC = 21.51 min. Rain intensity = 2.03(In/Hr)
Total area this stream = 76.62(Ac.)
Total Study Area (Main Stream No. 1) = 654.53(Ac.)
Total runoff = 137.80(CFS)

+++++
Process from Point/Station 90.000 to Point/Station 90.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 76.620(Ac.)
Runoff from this stream = 137.800(CFS)
Time of concentration = 21.51 min.
Rainfall intensity = 2.030(In/Hr)
Area averaged loss rate (Fm) = 0.1430(In/Hr)
Area averaged Pervious ratio (Ap) = 0.1950

+++++
Process from Point/Station 616.000 to Point/Station 617.000
**** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1540.000(Ft.)
Bottom (of initial area) elevation = 1160.000(Ft.)

Difference in elevation = 380.000(Ft.)
 Slope = 0.38000 s(%) = 38.00
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 10.097 min.
 Rainfall intensity = 3.196(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area ($Q=KCIA$) is $C = 0.786$
 Subarea runoff = 17.594(CFS)
 Total initial stream area = 7.000(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 617.000 to Point/Station 618.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 40.214(CFS)
 Depth of flow = 0.512(Ft.), Average velocity = 5.105(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 5.00
 2 150.00 0.00
 3 300.00 5.00
 Manning's 'N' friction factor = 0.035

Sub-Channel flow = 40.214(CFS)
 ' ' flow top width = 30.747(Ft.)
 ' ' velocity = 5.105(Ft/s)
 ' ' area = 7.878(Sq.Ft)
 ' ' Froude number = 1.777

Upstream point elevation = 1160.000(Ft.)
 Downstream point elevation = 1080.000(Ft.)
 Flow length = 900.000(Ft.)
 Travel time = 2.94 min.
 Time of concentration = 13.04 min.
 Depth of flow = 0.512(Ft.)
 Average velocity = 5.105(Ft/s)
 Total irregular channel flow = 40.214(CFS)
 Irregular channel normal depth above invert elev. = 0.512(Ft.)
 Average velocity of channel(s) = 5.105(Ft/s)

Sub-Channel No. 1 Critical depth = 0.645(Ft.)
 ' ' Critical flow top width = 38.672(Ft.)
 ' ' Critical flow velocity = 3.227(Ft/s)
 ' ' Critical flow area = 12.463(Sq.Ft)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(A_p) = 1.0000 Max loss rate(F_m) = 0.404(In/Hr)
 Rainfall intensity = 2.742(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) ($Q=KCIA$) is $C = 0.768$
 Subarea runoff = 35.022(CFS) for 18.000(Ac.)

Total runoff = 52.616(CFS)
 Effective area this stream = 25.00(Ac.)
 Total Study Area (Main Stream No. 1) = 679.53(Ac.)
 Area averaged Fm value = 0.404(In/Hr)

+++++
 Process from Point/Station 618.000 to Point/Station 90.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1033.000(Ft.)
 Downstream point/station elevation = 1025.000(Ft.)
 Pipe length = 420.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 52.616(CFS)
 Given pipe size = 48.00(In.)
 Calculated individual pipe flow = 52.616(CFS)
 Normal flow depth in pipe = 16.88(In.)
 Flow top width inside pipe = 45.84(In.)
 Critical Depth = 26.14(In.)
 Pipe flow velocity = 13.33(Ft/s)
 Travel time through pipe = 0.53 min.
 Time of concentration (TC) = 13.56 min.

+++++
 Process from Point/Station 90.000 to Point/Station 90.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 25.000(Ac.)
 Runoff from this stream = 52.616(CFS)
 Time of concentration = 13.56 min.
 Rainfall intensity = 2.678(In/Hr)
 Area averaged loss rate (Fm) = 0.4035(In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000

+++++
 Process from Point/Station 619.000 to Point/Station 620.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1056.400(Ft.)
 Bottom (of initial area) elevation = 1051.400(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%)= 0.50
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 10.306(CFS)
 Total initial stream area = 6.000(Ac.)
 Pervious area fraction = 0.500

Initial area Fm value = 0.367(In/Hr)

+++++
 Process from Point/Station 620.000 to Point/Station 621.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1051.400(Ft.)
 End of street segment elevation = 1046.000(Ft.)
 Length of street segment = 1070.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.083
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 15.458(CFS)
 Depth of flow = 0.461(Ft.), Average velocity = 2.261(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 18.293(Ft.)
 Flow velocity = 2.26(Ft/s)
 Travel time = 7.89 min. TC = 25.67 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 1.826(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.719
 Subarea runoff = 5.450(CFS) for 6.000(Ac.)
 Total runoff = 15.755(CFS)
 Effective area this stream = 12.00(Ac.)
 Total Study Area (Main Stream No. 1) = 691.53(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 15.755(CFS)
 Half street flow at end of street = 7.878(CFS)
 Depth of flow = 0.464(Ft.), Average velocity = 2.272(Ft/s)
 Flow width (from curb towards crown)= 18.428(Ft.)

+++++
 Process from Point/Station 621.000 to Point/Station 621.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 4
 Stream flow area = 12.000(Ac.)
 Runoff from this stream = 15.755(CFS)
 Time of concentration = 25.67 min.
 Rainfall intensity = 1.826(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)

Area averaged Pervious ratio (Ap) = 0.5000
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1522.640	13.98	2.629
2	137.800	21.51	2.030
3	52.616	13.56	2.678
4	15.755	25.67	1.826

Qmax(1) =
 1.000 * 1.000 * 1522.640) +
 1.317 * 0.650 * 137.800) +
 0.978 * 1.000 * 52.616) +
 1.550 * 0.545 * 15.755) + = 1705.428

Qmax(2) =
 0.747 * 1.000 * 1522.640) +
 1.000 * 1.000 * 137.800) +
 0.715 * 1.000 * 52.616) +
 1.140 * 0.838 * 15.755) + = 1327.290

Qmax(3) =
 1.021 * 0.970 * 1522.640) +
 1.343 * 0.630 * 137.800) +
 1.000 * 1.000 * 52.616) +
 1.584 * 0.528 * 15.755) + = 1689.602

Qmax(4) =
 0.660 * 1.000 * 1522.640) +
 0.892 * 1.000 * 137.800) +
 0.625 * 1.000 * 52.616) +
 1.000 * 1.000 * 15.755) + = 1176.449

Total of 4 streams to confluence:

Flow rates before confluence point:

1522.640 137.800 52.616 15.755

Maximum flow rates at confluence using above data:

1705.428 1327.290 1689.602 1176.449

Area of streams before confluence:

577.910 76.620 25.000 12.000

Effective area values after confluence:

659.260 689.583 640.042 691.530

Results of confluence:

Total flow rate = 1705.428(CFS)

Time of concentration = 13.985 min.

Effective stream area after confluence = 659.260(Ac.)

Stream Area average Pervious fraction(Ap) = 0.467

Stream Area average soil loss rate(Fm) = 0.260(In/Hr)

Study area (this main stream) = 691.53(Ac.)

+++++
 Process from Point/Station 90.000 to Point/Station 91.000
 **** IMPROVED CHANNEL TRAVEL TIME ****

Covered channel

Upstream point elevation = 1022.300(Ft.)

Downstream point elevation = 1013.100(Ft.)

Channel length thru subarea = 1320.000(Ft.)

Channel base width = 14.000(Ft.)

Slope or 'Z' of left channel bank = 0.000

Slope or 'Z' of right channel bank = 0.000

Manning's 'N' = 0.015
 Maximum depth of channel = 9.000(Ft.)
 Flow(q) thru subarea = 1705.428(CFS)
 Depth of flow = 6.539(Ft.), Average velocity = 18.630(Ft/s)
 Channel flow top width = 14.000(Ft.)
 Flow Velocity = 18.63(Ft/s)
 Travel time = 1.18 min.
 Time of concentration = 15.17 min.
 Critical depth = 7.750(Ft.)

++++++
 Process from Point/Station 91.000 to Point/Station 91.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 659.260(Ac.)
 Runoff from this stream = 1705.428(CFS)
 Time of concentration = 15.17 min.
 Rainfall intensity = 2.504(In/Hr)
 Area averaged loss rate (Fm) = 0.2599(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.4667

++++++
 Process from Point/Station 91.000 to Point/Station 91.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Soil classification AP and SCS values input by user
 USER INPUT of soil data for subarea
 SCS curve number for soil(AMC 2) = 53.21
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.385(In/Hr)
 Rainfall intensity = 1.966(In/Hr) for a 25.0 year storm
 User specified values are as follows:
 TC = 22.70 min. Rain intensity = 1.97(In/Hr)
 Total area this stream = 75.27(Ac.)
 Total Study Area (Main Stream No. 1) = 766.80(Ac.)
 Total runoff = 110.85(CFS)

++++++
 Process from Point/Station 91.000 to Point/Station 91.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 75.270(Ac.)
 Runoff from this stream = 110.850(CFS)
 Time of concentration = 22.70 min.
 Rainfall intensity = 1.966(In/Hr)
 Area averaged loss rate (Fm) = 0.3850(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000

++++++
 Process from Point/Station 638.000 to Point/Station 639.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1900.000(Ft.)
 Bottom (of initial area) elevation = 1540.000(Ft.)
 Difference in elevation = 360.000(Ft.)
 Slope = 0.36000 s(%)= 36.00
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 10.207 min.
 Rainfall intensity = 3.175(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.786
 Subarea runoff = 24.948(CFS)
 Total initial stream area = 10.000(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 639.000 to Point/Station 640.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 49.896(CFS)
 Depth of flow = 0.772(Ft.), Average velocity = 16.729(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	20.00
2	100.00	0.00
3	200.00	20.00

 Manning's 'N' friction factor = 0.035

Sub-Channel flow = 49.896(CFS)
 ' ' flow top width = 7.724(Ft.)
 ' ' velocity= 16.729(Ft/s)
 ' ' area = 2.983(Sq.Ft)
 ' ' Froude number = 4.744

Upstream point elevation = 1540.000(Ft.)
 Downstream point elevation = 1200.000(Ft.)
 Flow length = 600.000(Ft.)
 Travel time = 0.60 min.
 Time of concentration = 10.80 min.
 Depth of flow = 0.772(Ft.)
 Average velocity = 16.729(Ft/s)
 Total irregular channel flow = 49.896(CFS)
 Irregular channel normal depth above invert elev. = 0.772(Ft.)
 Average velocity of channel(s) = 16.729(Ft/s)

Sub-Channel No. 1 Critical depth = 1.438(Ft.)
 ' ' ' Critical flow top width = 14.375(Ft.)
 ' ' ' Critical flow velocity= 4.829(Ft/s)
 ' ' ' Critical flow area = 10.332(Sq.Ft)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 3.069(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.782
 Subarea runoff = 47.017(CFS) for 20.000(Ac.)
 Total runoff = 71.965(CFS)
 Effective area this stream = 30.00(Ac.)
 Total Study Area (Main Stream No. 1) = 796.80(Ac.)
 Area averaged Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 640.000 to Point/Station 641.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

 Estimated mean flow rate at midpoint of channel = 122.341(CFS)
 Depth of flow = 0.624(Ft.), Average velocity = 6.279(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	4.00
2	200.00	0.00
3	400.00	4.00

 Manning's 'N' friction factor = 0.035

Sub-Channel flow = 122.341(CFS)
 ' ' flow top width = 62.424(Ft.)
 ' ' velocity= 6.279(Ft/s)
 ' ' area = 19.484(Sq.Ft)
 ' ' Froude number = 1.981

Upstream point elevation = 1200.000(Ft.)
 Downstream point elevation = 1045.000(Ft.)
 Flow length = 1500.000(Ft.)
 Travel time = 3.98 min.
 Time of concentration = 14.79 min.
 Depth of flow = 0.624(Ft.)
 Average velocity = 6.279(Ft/s)
 Total irregular channel flow = 122.341(CFS)
 Irregular channel normal depth above invert elev. = 0.624(Ft.)
 Average velocity of channel(s) = 6.279(Ft/s)

Sub-Channel No. 1 Critical depth = 0.820(Ft.)

' ' ' Critical flow top width = 82.031(Ft.)
' ' ' Critical flow velocity= 3.636(Ft/s)
' ' ' Critical flow area = 33.646(Sq.Ft)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 2.542(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.757

Subarea runoff = 66.631(CFS) for 42.000(Ac.)
 Total runoff = 138.596(CFS)
 Effective area this stream = 72.00(Ac.)
 Total Study Area (Main Stream No. 1) = 838.80(Ac.)
 Area averaged Fm value = 0.404(In/Hr)

++++
 Process from Point/Station 641.000 to Point/Station 91.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1035.000(Ft.)
 Downstream point/station elevation = 1015.400(Ft.)
 Pipe length = 450.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 138.596(CFS)
 Given pipe size = 42.00(In.)
 Calculated individual pipe flow = 138.596(CFS)
 Normal flow depth in pipe = 24.91(In.)
 Flow top width inside pipe = 41.26(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 23.31(Ft/s)
 Travel time through pipe = 0.32 min.
 Time of concentration (TC) = 15.11 min.

++++
 Process from Point/Station 91.000 to Point/Station 91.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 72.000(Ac.)
 Runoff from this stream = 138.596(CFS)
 Time of concentration = 15.11 min.
 Rainfall intensity = 2.510(In/Hr)
 Area averaged loss rate (Fm) = 0.4035(In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000

++++
 Process from Point/Station 642.000 to Point/Station 643.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1042.000(Ft.)
 Bottom (of initial area) elevation = 1037.000(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.389) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 10.306(CFS)
 Total initial stream area = 6.000(Ac.)

Pervious area fraction = 0.500
Initial area Fm value = 0.367(In/Hr)

+++++
Process from Point/Station 643.000 to Point/Station 644.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1037.000(Ft.)
End of street segment elevation = 1031.000(Ft.)
Length of street segment = 1200.000(Ft.)
Height of curb above gutter flowline = 8.0(In.)
Width of half street (curb to crown) = 20.000(Ft.)
Distance from crown to crossfall grade break = 18.500(Ft.)
Slope from gutter to grade break (v/hz) = 0.083
Slope from grade break to crown (v/hz) = 0.020
Street flow is on [2] side(s) of the street
Distance from curb to property line = 10.000(Ft.)
Slope from curb to property line (v/hz) = 0.020
Gutter width = 1.500(Ft.)
Gutter hike from flowline = 1.500(In.)
Manning's N in gutter = 0.0150
Manning's N from gutter to grade break = 0.0150
Manning's N from grade break to crown = 0.0150
Estimated mean flow rate at midpoint of street = 17.176(CFS)
Depth of flow = 0.477(Ft.), Average velocity = 2.313(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width = 19.083(Ft.)
Flow velocity = 2.31(Ft/s)
Travel time = 8.65 min. TC = 26.44 min.
Adding area flow to street
RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 32.00
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
Rainfall intensity = 1.794(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.681
Subarea runoff = 6.798(CFS) for 8.000(Ac.)
Total runoff = 17.103(CFS)
Effective area this stream = 14.00(Ac.)
Total Study Area (Main Stream No. 1) = 852.80(Ac.)
Area averaged Fm value = 0.437(In/Hr)
Street flow at end of street = 17.103(CFS)
Half street flow at end of street = 8.552(CFS)
Depth of flow = 0.476(Ft.), Average velocity = 2.311(Ft/s)
Flow width (from curb towards crown)= 19.052(Ft.)

+++++
Process from Point/Station 644.000 to Point/Station 644.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 4
Stream flow area = 14.000(Ac.)
Runoff from this stream = 17.103(CFS)
Time of concentration = 26.44 min.
Rainfall intensity = 1.794(In/Hr)

Area averaged loss rate (Fm) = 0.4366(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000

+++++
 Process from Point/Station 645.000 to Point/Station 646.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1042.000(Ft.)
 Bottom (of initial area) elevation = 1037.000(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%)= 0.50
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.707
 Subarea runoff = 9.647(CFS)
 Total initial stream area = 6.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.489(In/Hr)

+++++
 Process from Point/Station 646.000 to Point/Station 647.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1037.000(Ft.)
 End of street segment elevation = 1031.000(Ft.)
 Length of street segment = 1200.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.083
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 15.275(CFS)
 Depth of flow = 0.460(Ft.), Average velocity = 2.247(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 18.242(Ft.)
 Flow velocity = 2.25(Ft/s)
 Travel time = 8.90 min. TC = 26.69 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000

Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
 Rainfall intensity = 1.784(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.653
 Subarea runoff = 5.503(CFS) for 7.000(Ac.)
 Total runoff = 15.150(CFS)
 Effective area this stream = 13.00(Ac.)
 Total Study Area (Main Stream No. 1) = 865.80(Ac.)
 Area averaged Fm value = 0.489(In/Hr)
 Street flow at end of street = 15.150(CFS)
 Half street flow at end of street = 7.575(CFS)
 Depth of flow = 0.459(Ft.), Average velocity = 2.242(Ft/s)
 Flow width (from curb towards crown)= 18.185(Ft.)

++++++
 Process from Point/Station 647.000 to Point/Station 647.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 5

Stream flow area = 13.000(Ac.)
 Runoff from this stream = 15.150(CFS)
 Time of concentration = 26.69 min.
 Rainfall intensity = 1.784(In/Hr)
 Area averaged loss rate (Fm) = 0.4889(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1705.428	15.17	2.504
2	110.850	22.70	1.966
3	138.596	15.11	2.510
4	17.103	26.44	1.794
5	15.150	26.69	1.784

Qmax(1) =
 1.000 * 1.000 * 1705.428) +
 1.340 * 0.668 * 110.850) +
 0.997 * 1.000 * 138.596) +
 1.523 * 0.574 * 17.103) +
 1.556 * 0.568 * 15.150) + = 1971.261

Qmax(2) =
 0.760 * 1.000 * 1705.428) +
 1.000 * 1.000 * 110.850) +
 0.742 * 1.000 * 138.596) +
 1.127 * 0.859 * 17.103) +
 1.141 * 0.850 * 15.150) + = 1541.286

Qmax(3) =
 1.003 * 0.996 * 1705.428) +
 1.344 * 0.666 * 110.850) +
 1.000 * 1.000 * 138.596) +
 1.527 * 0.571 * 17.103) +
 1.561 * 0.566 * 15.150) + = 1969.356

Qmax(4) =
 0.684 * 1.000 * 1705.428) +
 0.891 * 1.000 * 110.850) +

0.660 *	1.000 *	138.596) +	
1.000 *	1.000 *	17.103) +	
1.008 *	0.990 *	15.150) + =	1388.419

Qmax(5) =

0.679 *	1.000 *	1705.428) +	
0.885 *	1.000 *	110.850) +	
0.655 *	1.000 *	138.596) +	
0.992 *	1.000 *	17.103) +	
1.000 *	1.000 *	15.150) + =	1379.108

Total of 5 streams to confluence:

Flow rates before confluence point:

1705.428	110.850	138.596	17.103	15.150
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Maximum flow rates at confluence using above data:

1971.261	1541.286	1969.356	1388.419	1379.108
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Area of streams before confluence:

659.260	75.270	72.000	14.000	13.000
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Effective area values after confluence:

796.965	829.608	794.213	833.407	833.530
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Results of confluence:

Total flow rate = 1971.261(CFS)

Time of concentration = 15.166 min.

Effective stream area after confluence = 796.965(Ac.)

Stream Area average Pervious fraction(Ap) = 0.517

Stream Area average soil loss rate(Fm) = 0.290(In/Hr)

Study area (this main stream) = 833.53(Ac.)

 Process from Point/Station 91.000 to Point/Station 92.000
 **** IMPROVED CHANNEL TRAVEL TIME ****

Covered channel

Upstream point elevation = 1013.100(Ft.)

Downstream point elevation = 1006.400(Ft.)

Channel length thru subarea = 1340.000(Ft.)

Channel base width = 14.000(Ft.)

Slope or 'Z' of left channel bank = 0.000

Slope or 'Z' of right channel bank = 0.000

Manning's 'N' = 0.013

Maximum depth of channel = 9.000(Ft.)

Flow(q) thru subarea = 1971.261(CFS)

Depth of flow = 7.415(Ft.), Average velocity = 18.989(Ft/s)

Channel flow top width = 14.000(Ft.)

Flow Velocity = 18.99(Ft/s)

Travel time = 1.18 min.

Time of concentration = 16.34 min.

Critical depth = 8.500(Ft.)

 Process from Point/Station 92.000 to Point/Station 92.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 796.965(Ac.)

Runoff from this stream = 1971.261(CFS)

Time of concentration = 16.34 min.

Rainfall intensity = 2.394(In/Hr)

Area averaged loss rate (Fm) = 0.2902(In/Hr)

Area averaged Pervious ratio (Ap) = 0.5169

 Process from Point/Station 650.000 to Point/Station 651.000
 ***** INITIAL AREA EVALUATION *****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1040.300(Ft.)
 Bottom (of initial area) elevation = 1033.600(Ft.)
 Difference in elevation = 6.700(Ft.)
 Slope = 0.00670 s(%)= 0.67
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 16.778 min.
 Rainfall intensity = 2.357(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.713
 Subarea runoff = 8.405(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.489(In/Hr)

 Process from Point/Station 651.000 to Point/Station 652.000
 ***** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION *****

Top of street segment elevation = 1033.600(Ft.)
 End of street segment elevation = 1031.400(Ft.)
 Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.083
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 12.608(CFS)
 Depth of flow = 0.416(Ft.), Average velocity = 2.388(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 16.025(Ft.)
 Flow velocity = 2.39(Ft/s)
 Travel time = 2.30 min. TC = 19.08 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
 Rainfall intensity = 2.182(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.698
 Subarea runoff = 6.830(CFS) for 5.000(Ac.)
 Total runoff = 15.235(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 875.80(Ac.)
 Area averaged Fm value = 0.489(In/Hr)
 Street flow at end of street = 15.235(CFS)
 Half street flow at end of street = 7.618(CFS)
 Depth of flow = 0.440(Ft.), Average velocity = 2.502(Ft/s)
 Flow width (from curb towards crown)= 17.242(Ft.)

 Process from Point/Station 652.000 to Point/Station 653.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1031.400(Ft.)
 End of street segment elevation = 1026.000(Ft.)
 Length of street segment = 750.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.083
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 23.615(CFS)
 Depth of flow = 0.497(Ft.), Average velocity = 2.877(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 2.88(Ft/s)
 Travel time = 4.35 min. TC = 23.43 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
 Rainfall intensity = 1.929(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.672
 Subarea runoff = 11.982(CFS) for 11.000(Ac.)
 Total runoff = 27.218(CFS)
 Effective area this stream = 21.00(Ac.)
 Total Study Area (Main Stream No. 1) = 886.80(Ac.)
 Area averaged Fm value = 0.489(In/Hr)
 Street flow at end of street = 27.218(CFS)
 Half street flow at end of street = 13.609(CFS)

Warning: depth of flow exceeds top of curb
 Note: depth of flow exceeds top of street crown.
 Distance that curb overflow reaches into property = 10.00(Ft.)
 Flow width (from curb towards crown)= 20.000(Ft.)

++++
 Process from Point/Station 653.000 to Point/Station 654.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1026.000(Ft.)
 End of street segment elevation = 1023.000(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.083
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 34.346(CFS)
 Depth of flow = 0.767(Ft.), Average velocity = 2.963(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 4.99(Ft.)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 33.576(Ft.)
 Flow velocity = 2.96(Ft/s)
 Travel time = 3.71 min. TC = 27.14 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
 Rainfall intensity = 1.766(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.651
 Subarea runoff = 9.563(CFS) for 11.000(Ac.)
 Total runoff = 36.781(CFS)
 Effective area this stream = 32.00(Ac.)
 Total Study Area (Main Stream No. 1) = 897.80(Ac.)
 Area averaged Fm value = 0.489(In/Hr)
 Street flow at end of street = 36.781(CFS)
 Half street flow at end of street = 36.781(CFS)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 13.42(Ft.)
 Flow width (from curb towards crown)= 42.000(Ft.)

++++
 Process from Point/Station 654.000 to Point/Station 654.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 32.000(Ac.)
 Runoff from this stream = 36.781(CFS)
 Time of concentration = 27.14 min.
 Rainfall intensity = 1.766(In/Hr)
 Area averaged loss rate (Fm) = 0.4889(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1971.261	16.34	2.394
2	36.781	27.14	1.766
Qmax(1) =			
	1.000 *	1.000 *	1971.261) +
	1.492 *	0.602 *	36.781) + = 2004.303
Qmax(2) =			
	0.701 *	1.000 *	1971.261) +
	1.000 *	1.000 *	36.781) + = 1419.449

Total of 2 streams to confluence:

Flow rates before confluence point:

1971.261 36.781

Maximum flow rates at confluence using above data:

2004.303 1419.449

Area of streams before confluence:

796.965 32.000

Effective area values after confluence:

816.234 828.965

Results of confluence:

Total flow rate = 2004.303(CFS)

Time of concentration = 16.342 min.

Effective stream area after confluence = 816.234(Ac.)

Stream Area average Pervious fraction(Ap) = 0.516

Stream Area average soil loss rate(Fm) = 0.298(In/Hr)

Study area (this main stream) = 828.97(Ac.)

+++++
 Process from Point/Station 92.000 to Point/Station 93.000
 **** IMPROVED CHANNEL TRAVEL TIME ****

Covered channel

Upstream point elevation = 1006.400(Ft.)

Downstream point elevation = 1005.500(Ft.)

Channel length thru subarea = 450.000(Ft.)

Channel base width = 14.000(Ft.)

Slope or 'Z' of left channel bank = 0.000

Slope or 'Z' of right channel bank = 0.000

Manning's 'N' = 0.015

Maximum depth of channel = 9.000(Ft.)

Flow(q) thru subarea = 2004.303(CFS)

Pressure flow condition in covered channel:

Wetted perimeter = 46.00(Ft.) Flow area = 126.00(Sq.Ft)

Hydraulic grade line required at box inlet = 4.505(Ft.)

Friction loss = 5.405(Ft.)

Minor Friction loss = 0.000(Ft.) K-Factor = 0.000

Flow Velocity = 15.91(Ft/s)

Travel time = 0.47 min.

Time of concentration = 23.17 min.
End of computations, Total Study Area = 897.80 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.
Note: These figures do not consider reduced effective area
effects caused by confluences in the rational equation.

Area averaged pervious area fraction(A_p) = 0.514
Area averaged SCS curve number = 64.7

LINE "DZ-6"

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
 Rational Hydrology Study Date: 01/13/05

FONTANA / LINE DZ-6 HYDROLOGY
 25 YEAR STORM
 JN 04339

Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 25.0
 10 Year storm 1 hour rainfall = 0.930(In.)
 100 Year storm 1 hour rainfall = 1.350(In.)
 Computed rainfall intensity:
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)
 Slope used for rainfall intensity curve b = 0.6000
 Soil antecedent moisture condition (AMC) = 2

 Process from Point/Station 714.000 to Point/Station 715.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1104.000(Ft.)
 Bottom (of initial area) elevation = 1092.000(Ft.)
 Difference in elevation = 12.000(Ft.)
 Slope = 0.01200 s(%)= 1.20
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 11.669 min.
 Rainfall intensity = 2.930(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.870
 Subarea runoff = 17.846(CFS)
 Total initial stream area = 7.000(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.098(In/Hr)

 Process from Point/Station 715.000 to Point/Station 716.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1092.000(Ft.)
 End of street segment elevation = 1089.000(Ft.)
 Length of street segment = 800.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 31.867(CFS)
 Depth of flow = 0.591(Ft.), Average velocity = 2.662(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 2.66(Ft/s)
 Travel time = 5.01 min. TC = 16.68 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Rainfall intensity = 2.365(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.863
 Subarea runoff = 18.885(CFS) for 11.000(Ac.)
 Total runoff = 36.731(CFS)
 Effective area this stream = 18.00(Ac.)
 Total Study Area (Main Stream No. 1) = 18.00(Ac.)
 Area averaged Fm value = 0.098(In/Hr)
 Street flow at end of street = 36.731(CFS)
 Half street flow at end of street = 18.366(CFS)
 Depth of flow = 0.618(Ft.), Average velocity = 2.816(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++
 Process from Point/Station 716.000 to Point/Station 717.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1089.000(Ft.)
 End of street segment elevation = 1081.500(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150

Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 57.137(CFS)
 Depth of flow = 0.780(Ft.), Average velocity = 4.717(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 5.65(Ft.)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 34.236(Ft.)
 Flow velocity = 4.72(Ft/s)
 Travel time = 2.33 min. TC = 19.01 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Rainfall intensity = 2.187(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.860
 Subarea runoff = 34.704(CFS) for 20.000(Ac.)
 Total runoff = 71.435(CFS)
 Effective area this stream = 38.00(Ac.)
 Total Study Area (Main Stream No. 1) = 38.00(Ac.)
 Area averaged Fm value = 0.098(In/Hr)
 Street flow at end of street = 71.435(CFS)
 Half street flow at end of street = 71.435(CFS)
 Depth of flow = 0.838(Ft.), Average velocity = 4.888(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 8.58(Ft.)
 Flow width (from curb towards crown)= 37.160(Ft.)

++++++
 Process from Point/Station 717.000 to Point/Station 33.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1075.000(Ft.)
 Downstream point/station elevation = 1061.000(Ft.)
 Pipe length = 990.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 71.435(CFS)
 Given pipe size = 36.00(In.)
 Calculated individual pipe flow = 71.435(CFS)
 Normal flow depth in pipe = 26.72(In.)
 Flow top width inside pipe = 31.49(In.)
 Critical Depth = 32.12(In.)
 Pipe flow velocity = 12.70(Ft/s)
 Travel time through pipe = 1.30 min.
 Time of concentration (TC) = 20.31 min.

++++++
 Process from Point/Station 33.000 to Point/Station 33.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 38.000(Ac.)
 Runoff from this stream = 71.435(CFS)
 Time of concentration = 20.31 min.
 Rainfall intensity = 2.102(In/Hr)

Area averaged loss rate (Fm) = 0.0978(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

+++++
 Process from Point/Station 718.000 to Point/Station 719.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1082.000(Ft.)
 Bottom (of initial area) elevation = 1075.000(Ft.)
 Difference in elevation = 7.000(Ft.)
 Slope = 0.00700 s(%)= 0.70
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 12.997 min.
 Rainfall intensity = 2.747(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.868
 Subarea runoff = 11.921(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.098(In/Hr)

+++++
 Process from Point/Station 719.000 to Point/Station 720.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1075.000(Ft.)
 End of street segment elevation = 1073.300(Ft.)
 Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 17.881(CFS)
 Depth of flow = 0.480(Ft.), Average velocity = 2.363(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 19.269(Ft.)
 Flow velocity = 2.36(Ft/s)
 Travel time = 2.33 min. TC = 15.33 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000

Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Rainfall intensity = 2.488(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.865
 Subarea runoff = 9.594(CFS) for 5.000(Ac.)
 Total runoff = 21.515(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 48.00(Ac.)
 Area averaged Fm value = 0.098(In/Hr)
 Street flow at end of street = 21.515(CFS)
 Half street flow at end of street = 10.757(CFS)
 Depth of flow = 0.506(Ft.), Average velocity = 2.506(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++
 Process from Point/Station 720.000 to Point/Station 721.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1073.300(Ft.)
 End of street segment elevation = 1070.000(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 32.272(CFS)
 Depth of flow = 0.568(Ft.), Average velocity = 2.918(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 2.92(Ft/s)
 Travel time = 3.77 min. TC = 19.10 min.
 Adding area flow to street

COMMERCIAL subarea type

Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Rainfall intensity = 2.181(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.860
 Subarea runoff = 15.977(CFS) for 10.000(Ac.)
 Total runoff = 37.492(CFS)
 Effective area this stream = 20.00(Ac.)
 Total Study Area (Main Stream No. 1) = 58.00(Ac.)

Area averaged Fm value = 0.098(In/Hr)
 Street flow at end of street = 37.492(CFS)
 Half street flow at end of street = 18.746(CFS)
 Depth of flow = 0.594(Ft.), Average velocity = 3.096(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++
 Process from Point/Station 721.000 to Point/Station 722.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1070.000(Ft.)
 End of street segment elevation = 1068.000(Ft.)
 Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 46.865(CFS)
 Depth of flow = 0.810(Ft.), Average velocity = 3.506(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 7.17(Ft.)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 35.750(Ft.)
 Flow velocity = 3.51(Ft/s)
 Travel time = 1.57 min. TC = 20.66 min.
 Adding area flow to street
 CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Rainfall intensity = 2.080(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.822
 Subarea runoff = 13.822(CFS) for 10.000(Ac.)
 Total runoff = 51.314(CFS)
 Effective area this stream = 30.00(Ac.)
 Total Study Area (Main Stream No. 1) = 68.00(Ac.)
 Area averaged Fm value = 0.179(In/Hr)
 Street flow at end of street = 51.314(CFS)
 Half street flow at end of street = 51.314(CFS)
 Depth of flow = 0.834(Ft.), Average velocity = 3.559(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 8.36(Ft.)
 Flow width (from curb towards crown)= 36.941(Ft.)

+++++

Process from Point/Station 722.000 to Point/Station 722.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 30.000(Ac.)
 Runoff from this stream = 51.314(CFS)
 Time of concentration = 20.66 min.
 Rainfall intensity = 2.080(In/Hr)
 Area averaged loss rate (Fm) = 0.1793(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1833
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	71.435	20.31	2.102
2	51.314	20.66	2.080

Qmax(1) =
 1.000 * 1.000 * 71.435) +
 1.011 * 0.983 * 51.314) + = 122.445

Qmax(2) =
 0.989 * 1.000 * 71.435) +
 1.000 * 1.000 * 51.314) + = 121.976

Total of 2 streams to confluence:

Flow rates before confluence point:

71.435 51.314

Maximum flow rates at confluence using above data:

122.445 121.976

Area of streams before confluence:

38.000 30.000

Effective area values after confluence:

67.485 68.000

Results of confluence:

Total flow rate = 122.445(CFS)

Time of concentration = 20.310 min.

Effective stream area after confluence = 67.485(Ac.)

Stream Area average Pervious fraction(Ap) = 0.137

Stream Area average soil loss rate(Fm) = 0.134(In/Hr)

Study area (this main stream) = 68.00(Ac.)

+++++
 Process from Point/Station 33.000 to Point/Station 34.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1061.000(Ft.)

Downstream point/station elevation = 1048.200(Ft.)

Pipe length = 990.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 122.445(CFS)

Given pipe size = 39.00(In.)

NOTE: Normal flow is pressure flow in user selected pipe size.

The approximate hydraulic grade line above the pipe invert is
 14.039(Ft.) at the headworks or inlet of the pipe(s)

Pipe friction loss = 21.764(Ft.)

Minor friction loss = 5.074(Ft.) K-factor = 1.50

Pipe flow velocity = 14.76(Ft/s)

Travel time through pipe = 1.12 min.

Time of concentration (TC) = 21.43 min.


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Process from Point/Station      34.000 to Point/Station      34.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 67.485(Ac.)
 Runoff from this stream = 122.445(CFS)
 Time of concentration = 21.43 min.
 Rainfall intensity = 2.035(In/Hr)
 Area averaged loss rate (Fm) = 0.1337(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1368

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Process from Point/Station      723.000 to Point/Station      724.000
**** INITIAL AREA EVALUATION ****

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CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1072.000(Ft.)
 Bottom (of initial area) elevation = 1066.600(Ft.)
 Difference in elevation = 5.400(Ft.)
 Slope = 0.00540 s(%)= 0.54
 $TC = k(0.360)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 16.212 min.
 Rainfall intensity = 2.406(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.772
 Subarea runoff = 9.286(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.350
 Initial area Fm value = 0.342(In/Hr)

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Process from Point/Station      724.000 to Point/Station      725.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

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Top of street segment elevation = 1066.600(Ft.)
 End of street segment elevation = 1063.000(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150

Estimated mean flow rate at midpoint of street = 13.929(CFS)
 Depth of flow = 0.441(Ft.), Average velocity = 2.270(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 17.313(Ft.)
 Flow velocity = 2.27(Ft/s)
 Travel time = 4.85 min. TC = 21.06 min.
 Adding area flow to street
 CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Rainfall intensity = 2.056(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.750
 Subarea runoff = 6.141(CFS) for 5.000(Ac.)
 Total runoff = 15.427(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 78.00(Ac.)
 Area averaged Fm value = 0.342(In/Hr)
 Street flow at end of street = 15.427(CFS)
 Half street flow at end of street = 7.713(CFS)
 Depth of flow = 0.455(Ft.), Average velocity = 2.327(Ft/s)
 Flow width (from curb towards crown)= 18.008(Ft.)

++++++
 Process from Point/Station 725.000 to Point/Station 729.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1063.000(Ft.)
 End of street segment elevation = 1056.600(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 15.427(CFS)
 Depth of flow = 0.516(Ft.), Average velocity = 3.431(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 21.037(Ft.)
 Flow velocity = 3.43(Ft/s)
 Travel time = 3.21 min. TC = 24.26 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00

Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Rainfall intensity = 1.889(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.737
 Subarea runoff = 0.000(CFS) for 0.000(Ac.)
 Total runoff = 15.427(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 78.00(Ac.)
 Area averaged Fm value = 0.342(In/Hr)
 Street flow at end of street = 15.427(CFS)
 Half street flow at end of street = 15.427(CFS)
 Depth of flow = 0.516(Ft.), Average velocity = 3.431(Ft/s)
 Flow width (from curb towards crown)= 21.037(Ft.)

++++++
 Process from Point/Station 729.000 to Point/Station 729.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 10.000(Ac.)
 Runoff from this stream = 15.427(CFS)
 Time of concentration = 24.26 min.
 Rainfall intensity = 1.889(In/Hr)
 Area averaged loss rate (Fm) = 0.3422(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.3500

++++++
 Process from Point/Station 726.000 to Point/Station 727.000
 **** INITIAL AREA EVALUATION ****

CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1069.200(Ft.)
 Bottom (of initial area) elevation = 1062.000(Ft.)
 Difference in elevation = 7.200(Ft.)
 Slope = 0.00720 s(%)= 0.72
 $TC = k(0.360)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 15.305 min.
 Rainfall intensity = 2.490(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.776
 Subarea runoff = 9.666(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.350
 Initial area Fm value = 0.342(In/Hr)

++++++
 Process from Point/Station 727.000 to Point/Station 728.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1062.000(Ft.)
 End of street segment elevation = 1060.000(Ft.)

Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 14.499(CFS)
 Depth of flow = 0.440(Ft.), Average velocity = 2.385(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 17.230(Ft.)
 Flow velocity = 2.38(Ft/s)
 Travel time = 2.31 min. TC = 17.61 min.
 Adding area flow to street
 CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Rainfall intensity = 2.289(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.765
 Subarea runoff = 7.856(CFS) for 5.000(Ac.)
 Total runoff = 17.522(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 88.00(Ac.)
 Area averaged Fm value = 0.342(In/Hr)
 Street flow at end of street = 17.522(CFS)
 Half street flow at end of street = 8.761(CFS)
 Depth of flow = 0.466(Ft.), Average velocity = 2.499(Ft/s)
 Flow width (from curb towards crown)= 18.533(Ft.)

++++++
 Process from Point/Station 728.000 to Point/Station 729.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1060.000(Ft.)
 End of street segment elevation = 1056.600(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150

Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 26.284 (CFS)
 Depth of flow = 0.534 (Ft.), Average velocity = 2.714 (Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000 (Ft.)
 Flow velocity = 2.71 (Ft/s)
 Travel time = 4.05 min. TC = 21.67 min.
 Adding area flow to street
 CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 32.00
 Pervious ratio (Ap) = 0.3500 Max loss rate (Fm) = 0.342 (In/Hr)
 Rainfall intensity = 2.022 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.748
 Subarea runoff = 12.706 (CFS) for 10.000 (Ac.)
 Total runoff = 30.229 (CFS)
 Effective area this stream = 20.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 98.00 (Ac.)
 Area averaged Fm value = 0.342 (In/Hr)
 Street flow at end of street = 30.229 (CFS)
 Half street flow at end of street = 15.114 (CFS)
 Depth of flow = 0.555 (Ft.), Average velocity = 2.868 (Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000 (Ft.)

++++++
 Process from Point/Station 729.000 to Point/Station 729.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3

Stream flow area = 20.000 (Ac.)
 Runoff from this stream = 30.229 (CFS)
 Time of concentration = 21.67 min.
 Rainfall intensity = 2.022 (In/Hr)
 Area averaged loss rate (Fm) = 0.3422 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.3500
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	122.445	21.43	2.035
2	15.427	24.26	1.889
3	30.229	21.67	2.022
Qmax (1) =			
	1.000 *	1.000 *	122.445) +
	1.095 *	0.883 *	15.427) +
	1.008 *	0.989 *	30.229) + = 167.493
Qmax (2) =			
	0.923 *	1.000 *	122.445) +
	1.000 *	1.000 *	15.427) +
	0.921 *	1.000 *	30.229) + = 156.287
Qmax (3) =			
	0.993 *	1.000 *	122.445) +

1.086 * 0.893 * 15.427) +
 1.000 * 1.000 * 30.229) + = 166.768

Total of 3 streams to confluence:

Flow rates before confluence point:

122.445 15.427 30.229

Maximum flow rates at confluence using above data:

167.493 156.287 166.768

Area of streams before confluence:

67.485 10.000 20.000

Effective area values after confluence:

96.097 97.485 96.414

Results of confluence:

Total flow rate = 167.493(CFS)

Time of concentration = 21.428 min.

Effective stream area after confluence = 96.097(Ac.)

Stream Area average Pervious fraction(Ap) = 0.202

Stream Area average soil loss rate(Fm) = 0.198(In/Hr)

Study area (this main stream) = 97.49(Ac.)

+++++
 Process from Point/Station 34.000 to Point/Station 35.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1048.200(Ft.)

Downstream point/station elevation = 1042.000(Ft.)

Pipe length = 660.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 167.493(CFS)

Given pipe size = 39.00(In.)

NOTE: Normal flow is pressure flow in user selected pipe size.

The approximate hydraulic grade line above the pipe invert is

30.445(Ft.) at the headworks or inlet of the pipe(s)

Pipe friction loss = 27.150(Ft.)

Minor friction loss = 9.495(Ft.) K-factor = 1.50

Pipe flow velocity = 20.19(Ft/s)

Travel time through pipe = 0.54 min.

Time of concentration (TC) = 21.97 min.

+++++
 Process from Point/Station 35.000 to Point/Station 35.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 96.097(Ac.)

Runoff from this stream = 167.493(CFS)

Time of concentration = 21.97 min.

Rainfall intensity = 2.005(In/Hr)

Area averaged loss rate (Fm) = 0.1979(In/Hr)

Area averaged Pervious ratio (Ap) = 0.2024

+++++
 Process from Point/Station 730.000 to Point/Station 731.000
 **** INITIAL AREA EVALUATION ****

CONDOMINIUM subarea type

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.257(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1063.700(Ft.)
 Bottom (of initial area) elevation = 1055.800(Ft.)
 Difference in elevation = 7.900(Ft.)
 Slope = 0.00790 s(%)= 0.79
 $TC = k(0.360)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 15.024 min.
 Rainfall intensity = 2.518(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.808
 Subarea runoff = 10.176(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.350
 Initial area Fm value = 0.257(In/Hr)

++++++
 Process from Point/Station 731.000 to Point/Station 732.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1055.800(Ft.)
 End of street segment elevation = 1053.600(Ft.)
 Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 15.264(CFS)
 Depth of flow = 0.440(Ft.), Average velocity = 2.504(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 17.254(Ft.)
 Flow velocity = 2.50(Ft/s)
 Travel time = 2.20 min. TC = 17.22 min.
 Adding area flow to street
 CONDOMINIUM subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.257(In/Hr)
 Rainfall intensity = 2.320(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.800
 Subarea runoff = 8.394(CFS) for 5.000(Ac.)
 Total runoff = 18.570(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 108.00(Ac.)
 Area averaged Fm value = 0.257(In/Hr)

Street flow at end of street = 18.570(CFS)
 Half street flow at end of street = 9.285(CFS)
 Depth of flow = 0.467(Ft.), Average velocity = 2.628(Ft/s)
 Flow width (from curb towards crown)= 18.607(Ft.)

+++++
 Process from Point/Station 732.000 to Point/Station 733.000
 ***** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION *****

Top of street segment elevation = 1053.600(Ft.)
 End of street segment elevation = 1049.000(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 27.855(CFS)
 Depth of flow = 0.656(Ft.), Average velocity = 3.510(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 28.045(Ft.)
 Flow velocity = 3.51(Ft/s)
 Travel time = 3.13 min. TC = 20.35 min.
 Adding area flow to street
 CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Rainfall intensity = 2.099(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.772
 Subarea runoff = 13.815(CFS) for 10.000(Ac.)
 Total runoff = 32.385(CFS)
 Effective area this stream = 20.00(Ac.)
 Total Study Area (Main Stream No. 1) = 118.00(Ac.)
 Area averaged Fm value = 0.300(In/Hr)
 Street flow at end of street = 32.385(CFS)
 Half street flow at end of street = 32.385(CFS)
 Depth of flow = 0.695(Ft.), Average velocity = 3.567(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 1.40(Ft.)
 Flow width (from curb towards crown)= 29.981(Ft.)

+++++
 Process from Point/Station 733.000 to Point/Station 733.000
 ***** CONFLUENCE OF MINOR STREAMS *****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 20.000 (Ac.)
 Runoff from this stream = 32.385 (CFS)
 Time of concentration = 20.35 min.
 Rainfall intensity = 2.099 (In/Hr)
 Area averaged loss rate (Fm) = 0.2996 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.3500
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	167.493	21.97	2.005
2	32.385	20.35	2.099

$Q_{max}(1) =$
 $1.000 * 1.000 * 167.493) +$
 $0.948 * 1.000 * 32.385) + = 198.184$

$Q_{max}(2) =$
 $1.052 * 0.926 * 167.493) +$
 $1.000 * 1.000 * 32.385) + = 195.630$

Total of 2 streams to confluence:

Flow rates before confluence point:

167.493 32.385

Maximum flow rates at confluence using above data:

198.184 195.630

Area of streams before confluence:

96.097 20.000

Effective area values after confluence:

116.097 109.023

Results of confluence:

Total flow rate = 198.184 (CFS)

Time of concentration = 21.972 min.

Effective stream area after confluence = 116.097 (Ac.)

Stream Area average Pervious fraction (Ap) = 0.228

Stream Area average soil loss rate (Fm) = 0.215 (In/Hr)

Study area (this main stream) = 116.10 (Ac.)

End of computations, Total Study Area = 118.00 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction (Ap) = 0.227

Area averaged SCS curve number = 34.0

LINE "DZ-7"

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
Rational Hydrology Study Date: 01/13/05FONTANA / LINE DZ-7 HYDROLOGY
25 YEAR STORM
JN 04339

Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 25.0
 10 Year storm 1 hour rainfall = 0.930(In.)
 100 Year storm 1 hour rainfall = 1.350(In.)
 Computed rainfall intensity:
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)
 Slope used for rainfall intensity curve b = 0.6000
 Soil antecedent moisture condition (AMC) = 2

+++++
 Process from Point/Station 800.000 to Point/Station 801.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type

Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1098.000(Ft.)
 Bottom (of initial area) elevation = 1088.000(Ft.)
 Difference in elevation = 10.000(Ft.)
 Slope = 0.01000 s(%)= 1.00
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 12.102 min.
 Rainfall intensity = 2.867(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.869
 Subarea runoff = 14.954(CFS)
 Total initial stream area = 6.000(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.098(In/Hr)

+++++
 Process from Point/Station 801.000 to Point/Station 802.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1088.000(Ft.)
 End of street segment elevation = 1081.000(Ft.)
 Length of street segment = 820.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 27.415(CFS)
 Depth of flow = 0.505(Ft.), Average velocity = 3.213(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 3.21(Ft/s)
 Travel time = 4.25 min. TC = 16.36 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Rainfall intensity = 2.393(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.863
 Subarea runoff = 18.097(CFS) for 10.000(Ac.)
 Total runoff = 33.051(CFS)
 Effective area this stream = 16.00(Ac.)
 Total Study Area (Main Stream No. 1) = 16.00(Ac.)
 Area averaged Fm value = 0.098(In/Hr)
 Street flow at end of street = 33.051(CFS)
 Half street flow at end of street = 16.526(CFS)
 Depth of flow = 0.530(Ft.), Average velocity = 3.461(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++
 Process from Point/Station 802.000 to Point/Station 803.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1081.000(Ft.)
 End of street segment elevation = 1075.000(Ft.)
 Length of street segment = 620.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150

Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 53.708 (CFS)
 Depth of flow = 0.785 (Ft.), Average velocity = 4.365 (Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 5.89 (Ft.)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 34.476 (Ft.)
 Flow velocity = 4.37 (Ft/s)
 Travel time = 2.37 min. TC = 18.72 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 32.00
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.098 (In/Hr)
 Rainfall intensity = 2.207 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.860
 Subarea runoff = 35.274 (CFS) for 20.000 (Ac.)
 Total runoff = 68.325 (CFS)
 Effective area this stream = 36.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 36.00 (Ac.)
 Area averaged Fm value = 0.098 (In/Hr)
 Street flow at end of street = 68.325 (CFS)
 Half street flow at end of street = 68.325 (CFS)
 Depth of flow = 0.848 (Ft.), Average velocity = 4.539 (Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 9.05 (Ft.)
 Flow width (from curb towards crown) = 37.634 (Ft.)

++++++
 Process from Point/Station 803.000 to Point/Station 36.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1069.000 (Ft.)
 Downstream point/station elevation = 1054.000 (Ft.)
 Pipe length = 990.00 (Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 68.325 (CFS)
 Given pipe size = 36.00 (In.)
 Calculated individual pipe flow = 68.325 (CFS)
 Normal flow depth in pipe = 25.08 (In.)
 Flow top width inside pipe = 33.10 (In.)
 Critical Depth = 31.61 (In.)
 Pipe flow velocity = 12.99 (Ft/s)
 Travel time through pipe = 1.27 min.
 Time of concentration (TC) = 19.99 min.

++++++
 Process from Point/Station 36.000 to Point/Station 36.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 36.000 (Ac.)
 Runoff from this stream = 68.325 (CFS)
 Time of concentration = 19.99 min.
 Rainfall intensity = 2.121 (In/Hr)

Area averaged loss rate (Fm) = 0.0978 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000

+++++
 Process from Point/Station 804.000 to Point/Station 805.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 32.00
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.098 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000 (Ft.)
 Top (of initial area) elevation = 1081.500 (Ft.)
 Bottom (of initial area) elevation = 1071.000 (Ft.)
 Difference in elevation = 10.500 (Ft.)
 Slope = 0.01050 s(%) = 1.05
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 11.985 min.
 Rainfall intensity = 2.884 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.869
 Subarea runoff = 12.537 (CFS)
 Total initial stream area = 5.000 (Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.098 (In/Hr)

+++++
 Process from Point/Station 805.000 to Point/Station 806.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1071.000 (Ft.)
 End of street segment elevation = 1069.000 (Ft.)
 Length of street segment = 660.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 20.000 (Ft.)
 Distance from crown to crossfall grade break = 18.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500 (Ft.)
 Gutter hike from flowline = 1.500 (In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 25.074 (CFS)
 Depth of flow = 0.568 (Ft.), Average velocity = 2.270 (Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000 (Ft.)
 Flow velocity = 2.27 (Ft/s)
 Travel time = 4.85 min. TC = 16.83 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 1.000

Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)
 Rainfall intensity = 2.352(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.863
 Subarea runoff = 17.897(CFS) for 10.000(Ac.)
 Total runoff = 30.435(CFS)
 Effective area this stream = 15.00(Ac.)
 Total Study Area (Main Stream No. 1) = 51.00(Ac.)
 Area averaged Fm value = 0.098(In/Hr)
 Street flow at end of street = 30.435(CFS)
 Half street flow at end of street = 15.217(CFS)
 Depth of flow = 0.602(Ft.), Average velocity = 2.451(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++
 Process from Point/Station 806.000 to Point/Station 807.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1069.000(Ft.)
 End of street segment elevation = 1065.000(Ft.)
 Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 35.507(CFS)
 Depth of flow = 0.516(Ft.), Average velocity = 3.958(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 3.96(Ft/s)
 Travel time = 1.39 min. TC = 18.22 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
 Rainfall intensity = 2.243(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.822
 Subarea runoff = 6.417(CFS) for 5.000(Ac.)
 Total runoff = 36.851(CFS)
 Effective area this stream = 20.00(Ac.)

Total Study Area (Main Stream No. 1) = 56.00(Ac.)
 Area averaged Fm value = 0.196(In/Hr)
 Street flow at end of street = 36.851(CFS)
 Half street flow at end of street = 18.426(CFS)
 Depth of flow = 0.521(Ft.), Average velocity = 4.016(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++
 Process from Point/Station 807.000 to Point/Station 808.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1065.000(Ft.)
 End of street segment elevation = 1060.000(Ft.)
 Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 46.064(CFS)
 Depth of flow = 0.685(Ft.), Average velocity = 5.249(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 0.91(Ft.)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 29.489(Ft.)
 Flow velocity = 5.25(Ft/s)
 Travel time = 1.05 min. TC = 19.27 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
 Rainfall intensity = 2.169(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.778
 Subarea runoff = 13.788(CFS) for 10.000(Ac.)
 Total runoff = 50.639(CFS)
 Effective area this stream = 30.00(Ac.)
 Total Study Area (Main Stream No. 1) = 66.00(Ac.)
 Area averaged Fm value = 0.293(In/Hr)
 Street flow at end of street = 50.639(CFS)
 Half street flow at end of street = 50.639(CFS)
 Depth of flow = 0.710(Ft.), Average velocity = 5.281(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 2.19(Ft.)
 Flow width (from curb towards crown)= 30.772(Ft.)

+++++
 Process from Point/Station 808.000 to Point/Station 808.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 30.000(Ac.)
 Runoff from this stream = 50.639(CFS)
 Time of concentration = 19.27 min.
 Rainfall intensity = 2.169(In/Hr)
 Area averaged loss rate (Fm) = 0.2933(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.3000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	68.325	19.99	2.121
2	50.639	19.27	2.169
Qmax(1) =			
	1.000 *	1.000 *	68.325) +
	0.975 *	1.000 *	50.639) + = 117.682
Qmax(2) =			
	1.023 *	0.964 *	68.325) +
	1.000 *	1.000 *	50.639) + = 118.035

Total of 2 streams to confluence:
 Flow rates before confluence point:
 68.325 50.639
 Maximum flow rates at confluence using above data:
 117.682 118.035
 Area of streams before confluence:
 36.000 30.000
 Effective area values after confluence:
 66.000 64.696
 Results of confluence:
 Total flow rate = 118.035(CFS)
 Time of concentration = 19.269 min.
 Effective stream area after confluence = 64.696(Ac.)
 Stream Area average Pervious fraction(Ap) = 0.191
 Stream Area average soil loss rate(Fm) = 0.187(In/Hr)
 Study area (this main stream) = 66.00(Ac.)

+++++
 Process from Point/Station 36.000 to Point/Station 37.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1054.000(Ft.)
 Downstream point/station elevation = 1043.500(Ft.)
 Pipe length = 990.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 118.035(CFS)
 Given pipe size = 42.00(In.)
 NOTE: Normal flow is pressure flow in user selected pipe size.
 The approximate hydraulic grade line above the pipe invert is
 6.627(Ft.) at the headworks or inlet of the pipe(s)
 Pipe friction loss = 13.622(Ft.)
 Minor friction loss = 3.506(Ft.) K-factor = 1.50
 Pipe flow velocity = 12.27(Ft/s)
 Travel time through pipe = 1.34 min.
 Time of concentration (TC) = 20.61 min.

+++++
 Process from Point/Station 37.000 to Point/Station 37.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 64.696(Ac.)
 Runoff from this stream = 118.035(CFS)
 Time of concentration = 20.61 min.
 Rainfall intensity = 2.083(In/Hr)
 Area averaged loss rate (Fm) = 0.1867(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1909

+++++
 Process from Point/Station 809.000 to Point/Station 810.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1068.000(Ft.)
 Bottom (of initial area) elevation = 1061.000(Ft.)
 Difference in elevation = 7.000(Ft.)
 Slope = 0.00700 s(%)= 0.70
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 16.631 min.
 Rainfall intensity = 2.369(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.714
 Subarea runoff = 8.461(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.489(In/Hr)

+++++
 Process from Point/Station 810.000 to Point/Station 811.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1061.000(Ft.)
 End of street segment elevation = 1057.000(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150

Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 12.692 (CFS)
 Depth of flow = 0.422 (Ft.), Average velocity = 2.308 (Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 16.366 (Ft.)
 Flow velocity = 2.31 (Ft/s)
 Travel time = 4.77 min. TC = 21.40 min.
 Adding area flow to street
 RESIDENTIAL (5 - 7 dwt/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 32.00
 Pervious ratio (Ap) = 0.5000 Max loss rate (Fm) = 0.489 (In/Hr)
 Rainfall intensity = 2.037 (In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.684
 Subarea runoff = 5.469 (CFS) for 5.000 (Ac.)
 Total runoff = 13.930 (CFS)
 Effective area this stream = 10.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 76.00 (Ac.)
 Area averaged Fm value = 0.489 (In/Hr)
 Street flow at end of street = 13.930 (CFS)
 Half street flow at end of street = 6.965 (CFS)
 Depth of flow = 0.434 (Ft.), Average velocity = 2.361 (Ft/s)
 Flow width (from curb towards crown) = 16.965 (Ft.)

++++++
 Process from Point/Station 811.000 to Point/Station 812.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1057.000 (Ft.)
 End of street segment elevation = 1051.000 (Ft.)
 Length of street segment = 660.000 (Ft.)
 Height of curb above gutter flowline = 8.0 (In.)
 Width of half street (curb to crown) = 42.000 (Ft.)
 Distance from crown to crossfall grade break = 40.500 (Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000 (Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500 (Ft.)
 Gutter hike from flowline = 1.500 (In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 27.861 (CFS)
 Depth of flow = 0.628 (Ft.), Average velocity = 3.878 (Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 26.670 (Ft.)
 Flow velocity = 3.88 (Ft/s)
 Travel time = 2.84 min. TC = 24.23 min.
 Adding area flow to street
 SCHOOL subarea
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.6000 Max loss rate(Fm)= 0.587(In/Hr)
 Rainfall intensity = 1.890(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.636
 Subarea runoff = 22.143(CFS) for 20.000(Ac.)
 Total runoff = 36.073(CFS)
 Effective area this stream = 30.00(Ac.)
 Total Study Area (Main Stream No. 1) = 96.00(Ac.)
 Area averaged Fm value = 0.554(In/Hr)
 Street flow at end of street = 36.073(CFS)
 Half street flow at end of street = 36.073(CFS)
 Depth of flow = 0.688(Ft.), Average velocity = 4.068(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 1.06(Ft.)
 Flow width (from curb towards crown)= 29.640(Ft.)

+++++
 Process from Point/Station 812.000 to Point/Station 812.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 30.000(Ac.)
 Runoff from this stream = 36.073(CFS)
 Time of concentration = 24.23 min.
 Rainfall intensity = 1.890(In/Hr)
 Area averaged loss rate (Fm) = 0.5541(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5667
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	118.035	20.61	2.083
2	36.073	24.23	1.890
Qmax(1) =			
	1.000 *	1.000 *	118.035) +
	1.144 *	0.851 *	36.073) + = 153.145
Qmax(2) =			
	0.898 *	1.000 *	118.035) +
	1.000 *	1.000 *	36.073) + = 142.114

Total of 2 streams to confluence:

Flow rates before confluence point:

118.035 36.073

Maximum flow rates at confluence using above data:

153.145 142.114

Area of streams before confluence:

64.696 30.000

Effective area values after confluence:

90.215 94.696

Results of confluence:

Total flow rate = 153.145(CFS)

Time of concentration = 20.614 min.

Effective stream area after confluence = 90.215(Ac.)

Stream Area average Pervious fraction(Ap) = 0.310

Stream Area average soil loss rate(Fm) = 0.303(In/Hr)

Study area (this main stream) = 94.70(Ac.)

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Process from Point/Station      37.000 to Point/Station      38.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****

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Upstream point/station elevation = 1043.500(Ft.)
Downstream point/station elevation = 1038.000(Ft.)
Pipe length = 660.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 153.145(CFS)
Given pipe size = 42.00(In.)
NOTE: Normal flow is pressure flow in user selected pipe size.
The approximate hydraulic grade line above the pipe invert is
      15.689(Ft.) at the headworks or inlet of the pipe(s)
Pipe friction loss = 15.287(Ft.)
Minor friction loss = 5.901(Ft.) K-factor = 1.50
Pipe flow velocity = 15.92(Ft/s)
Travel time through pipe = 0.69 min.
Time of concentration (TC) = 21.31 min.

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Process from Point/Station      38.000 to Point/Station      38.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 1
Stream flow area = 90.215(Ac.)
Runoff from this stream = 153.145(CFS)
Time of concentration = 21.31 min.
Rainfall intensity = 2.042(In/Hr)
Area averaged loss rate (Fm) = 0.3031(In/Hr)
Area averaged Pervious ratio (Ap) = 0.3099

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Process from Point/Station      813.000 to Point/Station      814.000
**** INITIAL AREA EVALUATION ****

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CONDOMINIUM subarea type
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 32.00
Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1056.600(Ft.)
Bottom (of initial area) elevation = 1048.500(Ft.)
Difference in elevation = 8.100(Ft.)
Slope = 0.00810 s(%)= 0.81
TC = k(0.360)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 14.949 min.
Rainfall intensity = 2.526(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.778
Subarea runoff = 9.826(CFS)
Total initial stream area = 5.000(Ac.)
Pervious area fraction = 0.350
Initial area Fm value = 0.342(In/Hr)

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Process from Point/Station 814.000 to Point/Station 815.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1048.500(Ft.)
 End of street segment elevation = 1047.300(Ft.)
 Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 14.739(CFS)
 Depth of flow = 0.478(Ft.), Average velocity = 1.976(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 19.128(Ft.)
 Flow velocity = 1.98(Ft/s)
 Travel time = 2.78 min. TC = 17.73 min.
 Adding area flow to street
 CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Rainfall intensity = 2.280(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.765
 Subarea runoff = 7.612(CFS) for 5.000(Ac.)
 Total runoff = 17.438(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 106.00(Ac.)
 Area averaged Fm value = 0.342(In/Hr)
 Street flow at end of street = 17.438(CFS)
 Half street flow at end of street = 8.719(CFS)
 Depth of flow = 0.501(Ft.), Average velocity = 2.076(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++
 Process from Point/Station 815.000 to Point/Station 816.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1047.300(Ft.)
 End of street segment elevation = 1045.000(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street

Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 26.156(CFS)
 Depth of flow = 0.563(Ft.), Average velocity = 2.407(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 2.41(Ft/s)
 Travel time = 4.57 min. TC = 22.30 min.
 Adding area flow to street
 CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Rainfall intensity = 1.987(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.745
 Subarea runoff = 12.164(CFS) for 10.000(Ac.)
 Total runoff = 29.601(CFS)
 Effective area this stream = 20.00(Ac.)
 Total Study Area (Main Stream No. 1) = 116.00(Ac.)
 Area averaged Fm value = 0.342(In/Hr)
 Street flow at end of street = 29.601(CFS)
 Half street flow at end of street = 14.801(CFS)
 Depth of flow = 0.584(Ft.), Average velocity = 2.528(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++
 Process from Point/Station 816.000 to Point/Station 816.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 20.000(Ac.)
 Runoff from this stream = 29.601(CFS)
 Time of concentration = 22.30 min.
 Rainfall intensity = 1.987(In/Hr)
 Area averaged loss rate (Fm) = 0.3422(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.3500
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	153.145	21.31	2.042
2	29.601	22.30	1.987
Qmax(1) =			
	1.000 *	1.000 *	153.145) +
	1.034 *	0.955 *	29.601) + = 182.373
Qmax(2) =			
	0.968 *	1.000 *	153.145) +

$$1.000 * 1.000 * 29.601) + = 177.878$$

Total of 2 streams to confluence:

Flow rates before confluence point:

153.145 29.601

Maximum flow rates at confluence using above data:

182.373 177.878

Area of streams before confluence:

90.215 20.000

Effective area values after confluence:

109.321 110.215

Results of confluence:

Total flow rate = 182.373(CFS)

Time of concentration = 21.305 min.

Effective stream area after confluence = 109.321(Ac.)

Stream Area average Pervious fraction(Ap) = 0.317

Stream Area average soil loss rate(Fm) = 0.310(In/Hr)

Study area (this main stream) = 110.22(Ac.)

End of computations, Total Study Area = 116.00 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.316

Area averaged SCS curve number = 32.0

LINE "DZ-5"

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
 Rational Hydrology Study Date: 01/13/05

 FONTANA / LINE DZ-5 HYDROLOGY
 25 YEAR STORM
 JN 04339

 Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

 Rational hydrology study storm event year is 25.0
 10 Year storm 1 hour rainfall = 0.930(In.)
 100 Year storm 1 hour rainfall = 1.350(In.)
 Computed rainfall intensity:
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)
 Slope used for rainfall intensity curve b = 0.6000
 Soil antecedent moisture condition (AMC) = 2

+++++
 Process from Point/Station 700.000 to Point/Station 701.000
 **** INITIAL AREA EVALUATION ****

 CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1104.000(Ft.)
 Bottom (of initial area) elevation = 1096.700(Ft.)
 Difference in elevation = 7.300(Ft.)
 Slope = 0.00730 s(%)= 0.73
 $TC = k(0.360)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 15.263 min.
 Rainfall intensity = 2.494(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.777
 Subarea runoff = 9.685(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.350
 Initial area Fm value = 0.342(In/Hr)

+++++
 Process from Point/Station 701.000 to Point/Station 702.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

 Top of street segment elevation = 1096.700(Ft.)
 End of street segment elevation = 1095.000(Ft.)
 Length of street segment = 330.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 14.527(CFS)
 Depth of flow = 0.451(Ft.), Average velocity = 2.244(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 17.791(Ft.)
 Flow velocity = 2.24(Ft/s)
 Travel time = 2.45 min. TC = 17.71 min.
 Adding area flow to street
 CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Rainfall intensity = 2.281(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.765
 Subarea runoff = 7.766(CFS) for 5.000(Ac.)
 Total runoff = 17.451(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 10.00(Ac.)
 Area averaged Fm value = 0.342(In/Hr)
 Street flow at end of street = 17.451(CFS)
 Half street flow at end of street = 8.725(CFS)
 Depth of flow = 0.477(Ft.), Average velocity = 2.348(Ft/s)
 Flow width (from curb towards crown)= 19.090(Ft.)

++++++
 Process from Point/Station 702.000 to Point/Station 703.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1095.000(Ft.)
 End of street segment elevation = 1092.000(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150

Estimated mean flow rate at midpoint of street = 26.176(CFS)
 Depth of flow = 0.542(Ft.), Average velocity = 2.609(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 2.61(Ft/s)
 Travel time = 4.22 min. TC = 21.93 min.

Adding area flow to street

CONDOMINIUM subarea type

Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Rainfall intensity = 2.007(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.747
 Subarea runoff = 12.513(CFS) for 10.000(Ac.)
 Total runoff = 29.964(CFS)
 Effective area this stream = 20.00(Ac.)
 Total Study Area (Main Stream No. 1) = 20.00(Ac.)
 Area averaged Fm value = 0.342(In/Hr)
 Street flow at end of street = 29.964(CFS)
 Half street flow at end of street = 14.982(CFS)
 Depth of flow = 0.564(Ft.), Average velocity = 2.753(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 20.000(Ft.)

 Process from Point/Station 703.000 to Point/Station 704.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1092.000(Ft.)
 End of street segment elevation = 1082.000(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 44.946(CFS)
 Depth of flow = 0.678(Ft.), Average velocity = 5.244(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 0.56(Ft.)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 29.148(Ft.)
 Flow velocity = 5.24(Ft/s)
 Travel time = 2.10 min. TC = 24.03 min.
 Adding area flow to street
 CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000

Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Rainfall intensity = 1.900(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.738
 Subarea runoff = 26.111(CFS) for 20.000(Ac.)
 Total runoff = 56.075(CFS)
 Effective area this stream = 40.00(Ac.)
 Total Study Area (Main Stream No. 1) = 40.00(Ac.)
 Area averaged Fm value = 0.342(In/Hr)
 Street flow at end of street = 56.075(CFS)
 Half street flow at end of street = 56.075(CFS)
 Depth of flow = 0.737(Ft.), Average velocity = 5.334(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 3.53(Ft.)
 Flow width (from curb towards crown)= 32.118(Ft.)

++++++
 Process from Point/Station 704.000 to Point/Station 30.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1076.000(Ft.)
 Downstream point/station elevation = 1066.000(Ft.)
 Pipe length = 1000.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 56.075(CFS)
 Given pipe size = 36.00(In.)
 Calculated individual pipe flow = 56.075(CFS)
 Normal flow depth in pipe = 25.27(In.)
 Flow top width inside pipe = 32.94(In.)
 Critical Depth = 29.14(In.)
 Pipe flow velocity = 10.57(Ft/s)
 Travel time through pipe = 1.58 min.
 Time of concentration (TC) = 25.60 min.

++++++
 Process from Point/Station 30.000 to Point/Station 30.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 40.000(Ac.)
 Runoff from this stream = 56.075(CFS)
 Time of concentration = 25.60 min.
 Rainfall intensity = 1.829(In/Hr)
 Area averaged loss rate (Fm) = 0.3422(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.3500

++++++
 Process from Point/Station 705.000 to Point/Station 706.000
 **** INITIAL AREA EVALUATION ****

CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1085.700(Ft.)
 Bottom (of initial area) elevation = 1075.300(Ft.)
 Difference in elevation = 10.400(Ft.)
 Slope = 0.01040 s(%)= 1.04
 $TC = k(0.360)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 14.220 min.
 Rainfall intensity = 2.603(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.782
 Subarea runoff = 20.344(CFS)
 Total initial stream area = 10.000(Ac.)
 Pervious area fraction = 0.350
 Initial area Fm value = 0.342(In/Hr)

+++++
 Process from Point/Station 706.000 to Point/Station 707.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1075.300(Ft.)
 End of street segment elevation = 1072.000(Ft.)
 Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 27.972(CFS)
 Depth of flow = 0.497(Ft.), Average velocity = 3.397(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 3.40(Ft/s)
 Travel time = 1.62 min. TC = 15.84 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 2.440(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.770
 Subarea runoff = 12.523(CFS) for 7.500(Ac.)
 Total runoff = 32.866(CFS)
 Effective area this stream = 17.50(Ac.)
 Total Study Area (Main Stream No. 1) = 57.50(Ac.)
 Area averaged Fm value = 0.353(In/Hr)

Street flow at end of street = 32.866(CFS)
 Half street flow at end of street = 16.433(CFS)
 Depth of flow = 0.518(Ft.), Average velocity = 3.622(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000(Ft.)

+++++
 Process from Point/Station 707.000 to Point/Station 707.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 17.500(Ac.)
 Runoff from this stream = 32.866(CFS)
 Time of concentration = 15.84 min.
 Rainfall intensity = 2.440(In/Hr)
 Area averaged loss rate (Fm) = 0.3528(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.4143
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	56.075	25.60	1.829
2	32.866	15.84	2.440
Qmax(1) =			
	1.000 *	1.000 *	56.075) +
	0.707 *	1.000 *	32.866) + = 79.321
Qmax(2) =			
	1.411 *	0.619 *	56.075) +
	1.000 *	1.000 *	32.866) + = 81.807

Total of 2 streams to confluence:
 Flow rates before confluence point:
 56.075 32.866
 Maximum flow rates at confluence using above data:
 79.321 81.807
 Area of streams before confluence:
 40.000 17.500
 Effective area values after confluence:
 57.500 42.244
 Results of confluence:
 Total flow rate = 81.807(CFS)
 Time of concentration = 15.839 min.
 Effective stream area after confluence = 42.244(Ac.)
 Stream Area average Pervious fraction(Ap) = 0.370
 Stream Area average soil loss rate(Fm) = 0.345(In/Hr)
 Study area (this main stream) = 57.50(Ac.)

+++++
 Process from Point/Station 30.000 to Point/Station 31.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1066.000(Ft.)
 Downstream point/station elevation = 1062.200(Ft.)
 Pipe length = 990.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 81.807(CFS)
 Given pipe size = 39.00(In.)
 NOTE: Normal flow is pressure flow in user selected pipe size.

The approximate hydraulic grade line above the pipe invert is
 8.180(Ft.) at the headworks or inlet of the pipe(s)
 Pipe friction loss = 9.715(Ft.)
 Minor friction loss = 2.265(Ft.) K-factor = 1.50
 Pipe flow velocity = 9.86(Ft/s)
 Travel time through pipe = 1.67 min.
 Time of concentration (TC) = 17.51 min.

+++++
 Process from Point/Station 31.000 to Point/Station 31.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 42.244(Ac.)
 Runoff from this stream = 81.807(CFS)
 Time of concentration = 17.51 min.
 Rainfall intensity = 2.297(In/Hr)
 Area averaged loss rate (Fm) = 0.3455(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.3696

+++++
 Process from Point/Station 708.000 to Point/Station 709.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1072.000(Ft.)
 Bottom (of initial area) elevation = 1069.200(Ft.)
 Difference in elevation = 2.800(Ft.)
 Slope = 0.00280 s(%) = 0.28
 $TC = k(0.389) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 19.976 min.
 Rainfall intensity = 2.122(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.744
 Subarea runoff = 11.850(CFS)
 Total initial stream area = 7.500(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

+++++
 Process from Point/Station 709.000 to Point/Station 710.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1069.200(Ft.)
 End of street segment elevation = 1062.600(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020

Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 27.649(CFS)
 Depth of flow = 0.617(Ft.), Average velocity = 4.012(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 26.116(Ft.)
 Flow velocity = 4.01(Ft/s)
 Travel time = 2.74 min. TC = 22.72 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367(In/Hr)
 Rainfall intensity = 1.965(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.732
 Subarea runoff = 27.697(CFS) for 20.000(Ac.)
 Total runoff = 39.547(CFS)
 Effective area this stream = 27.50(Ac.)
 Total Study Area (Main Stream No. 1) = 85.00(Ac.)
 Area averaged Fm value = 0.367(In/Hr)
 Street flow at end of street = 39.547(CFS)
 Half street flow at end of street = 39.547(CFS)
 Depth of flow = 0.700(Ft.), Average velocity = 4.278(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 1.66(Ft.)
 Flow width (from curb towards crown) = 30.242(Ft.)

++++++
 Process from Point/Station 710.000 to Point/Station 710.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 27.500(Ac.)
 Runoff from this stream = 39.547(CFS)
 Time of concentration = 22.72 min.
 Rainfall intensity = 1.965(In/Hr)
 Area averaged loss rate (Fm) = 0.3670(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	81.807	17.51	2.297
2	39.547	22.72	1.965
Qmax(1) =	1.000 *	1.000 *	81.807) +
	1.208 *	0.771 *	39.547) + = 118.627
Qmax(2) =			

0.830 * 1.000 * 81.807) +
 1.000 * 1.000 * 39.547) + = 107.433

Total of 2 streams to confluence:

Flow rates before confluence point:

81.807 39.547

Maximum flow rates at confluence using above data:

118.627 107.433

Area of streams before confluence:

42.244 27.500

Effective area values after confluence:

63.443 69.744

Results of confluence:

Total flow rate = 118.627(CFS)

Time of concentration = 17.512 min.

Effective stream area after confluence = 63.443(Ac.)

Stream Area average Pervious fraction(Ap) = 0.421

Stream Area average soil loss rate(Fm) = 0.354(In/Hr)

Study area (this main stream) = 69.74(Ac.)

 Process from Point/Station 31.000 to Point/Station 32.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1056.600(Ft.)
 Downstream point/station elevation = 1052.000(Ft.)
 Pipe length = 660.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 118.627(CFS)
 Given pipe size = 39.00(In.)
 NOTE: Normal flow is pressure flow in user selected pipe size.
 The approximate hydraulic grade line above the pipe invert is
 13.782(Ft.) at the headworks or inlet of the pipe(s)
 Pipe friction loss = 13.619(Ft.)
 Minor friction loss = 4.763(Ft.) K-factor = 1.50
 Pipe flow velocity = 14.30(Ft/s)
 Travel time through pipe = 0.77 min.
 Time of concentration (TC) = 18.28 min.

 Process from Point/Station 32.000 to Point/Station 32.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 63.443(Ac.)
 Runoff from this stream = 118.627(CFS)
 Time of concentration = 18.28 min.
 Rainfall intensity = 2.238(In/Hr)
 Area averaged loss rate (Fm) = 0.3539(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.4210

 Process from Point/Station 711.000 to Point/Station 712.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1069.600(Ft.)
 Bottom (of initial area) elevation = 1062.100(Ft.)
 Difference in elevation = 7.500(Ft.)
 Slope = 0.00750 s(%)= 0.75
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 16.404 min.
 Rainfall intensity = 2.389(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.762
 Subarea runoff = 9.098(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.367(In/Hr)

++++++
 Process from Point/Station 712.000 to Point/Station 713.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1062.100(Ft.)
 End of street segment elevation = 1058.000(Ft.)
 Length of street segment = 990.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 22.746(CFS)
 Depth of flow = 0.669(Ft.), Average velocity = 2.740(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 0.11(Ft.)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 28.690(Ft.)
 Flow velocity = 2.74(Ft/s)
 Travel time = 6.02 min. TC = 22.43 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 56.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
 Rainfall intensity = 1.980(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.733
 Subarea runoff = 19.939(CFS) for 15.000(Ac.)
 Total runoff = 29.037(CFS)
 Effective area this stream = 20.00(Ac.)

Total Study Area (Main Stream No. 1) = 105.00 (Ac.)
 Area averaged Fm value = 0.367 (In/Hr)
 Street flow at end of street = 29.037 (CFS)
 Half street flow at end of street = 29.037 (CFS)
 Depth of flow = 0.735 (Ft.), Average velocity = 2.786 (Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 3.41 (Ft.)
 Flow width (from curb towards crown) = 31.992 (Ft.)

++++++
 Process from Point/Station 713.000 to Point/Station 713.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 20.000 (Ac.)
 Runoff from this stream = 29.037 (CFS)
 Time of concentration = 22.43 min.
 Rainfall intensity = 1.980 (In/Hr)
 Area averaged loss rate (Fm) = 0.3670 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	118.627	18.28	2.238
2	29.037	22.43	1.980
Qmax(1) =			
	1.000 *	1.000 *	118.627) +
	1.160 *	0.815 *	29.037) + = 146.088
Qmax(2) =			
	0.863 *	1.000 *	118.627) +
	1.000 *	1.000 *	29.037) + = 131.405

Total of 2 streams to confluence:

Flow rates before confluence point:

118.627 29.037

Maximum flow rates at confluence using above data:

146.088 131.405

Area of streams before confluence:

63.443 20.000

Effective area values after confluence:

79.746 83.443

Results of confluence:

Total flow rate = 146.088 (CFS)

Time of concentration = 18.281 min.

Effective stream area after confluence = 79.746 (Ac.)

Stream Area average Pervious fraction (Ap) = 0.440

Stream Area average soil loss rate (Fm) = 0.357 (In/Hr)

Study area (this main stream) = 83.44 (Ac.)

++++++
 Process from Point/Station 32.000 to Point/Station 35.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1052.000 (Ft.)

Downstream point/station elevation = 1041.000 (Ft.)

Pipe length = 1320.00 (Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 146.088(CFS)
 Given pipe size = 51.00(In.)
 Calculated individual pipe flow = 146.088(CFS)
 Normal flow depth in pipe = 39.56(In.)
 Flow top width inside pipe = 42.54(In.)
 Critical Depth = 42.87(In.)
 Pipe flow velocity = 12.36(Ft/s)
 Travel time through pipe = 1.78 min.
 Time of concentration (TC) = 20.06 min.

++++++
 Process from Point/Station 35.000 to Point/Station 35.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 79.746(Ac.)
 Runoff from this stream = 146.088(CFS)
 Time of concentration = 20.06 min.
 Rainfall intensity = 2.117(In/Hr)
 Area averaged loss rate (Fm) = 0.3571(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.4399

++++++
 Process from Point/Station 35.000 to Point/Station 35.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Soil classification AP and SCS values input by user
 USER INPUT of soil data for subarea
 SCS curve number for soil(AMC 2) = 36.98
 Pervious ratio(Ap) = 0.2280 Max loss rate(Fm)= 0.215(In/Hr)
 Rainfall intensity = 2.005(In/Hr) for a 25.0 year storm
 User specified values are as follows:
 TC = 21.97 min. Rain intensity = 2.00(In/Hr)
 Total area this stream = 116.10(Ac.)
 Total Study Area (Main Stream No. 1) = 221.10(Ac.)
 Total runoff = 198.18(CFS)

++++++
 Process from Point/Station 35.000 to Point/Station 35.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 116.100(Ac.)
 Runoff from this stream = 198.180(CFS)
 Time of concentration = 21.97 min.
 Rainfall intensity = 2.005(In/Hr)
 Area averaged loss rate (Fm) = 0.2150(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.2280
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	146.088	20.06	2.117
2	198.180	21.97	2.005

Qmax(1) =
 1.000 * 1.000 * 146.088) +

$1.063 * 0.913 * 198.180) + = 338.411$
 $Q_{max}(2) =$
 $0.936 * 1.000 * 146.088) +$
 $1.000 * 1.000 * 198.180) + = 334.941$

Total of 2 streams to confluence:
Flow rates before confluence point:

146.088 198.180

Maximum flow rates at confluence using above data:
338.411 334.941

Area of streams before confluence:
79.746 116.100

Effective area values after confluence:
185.759 195.846

Results of confluence:

Total flow rate = 338.411(CFS)

Time of concentration = 20.061 min.

Effective stream area after confluence = 185.759(Ac.)

Stream Area average Pervious fraction(Ap) = 0.314

Stream Area average soil loss rate(Fm) = 0.273(In/Hr)

Study area (this main stream) = 195.85(Ac.)

++++++
 Process from Point/Station 35.000 to Point/Station 38.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1041.000(Ft.)
 Downstream point/station elevation = 1035.000(Ft.)
 Pipe length = 1320.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 338.411(CFS)
 Given pipe size = 84.00(In.)
 Calculated individual pipe flow = 338.411(CFS)
 Normal flow depth in pipe = 56.06(In.)
 Flow top width inside pipe = 79.15(In.)
 Critical Depth = 58.21(In.)
 Pipe flow velocity = 12.39(Ft/s)
 Travel time through pipe = 1.78 min.
 Time of concentration (TC) = 21.84 min.

++++++
 Process from Point/Station 38.000 to Point/Station 38.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 185.759(Ac.)
 Runoff from this stream = 338.411(CFS)
 Time of concentration = 21.84 min.
 Rainfall intensity = 2.012(In/Hr)
 Area averaged loss rate (Fm) = 0.2728(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.3143

++++++
 Process from Point/Station 38.000 to Point/Station 38.000
 **** USER DEFINED FLOW INFORMATION AT A POINT ****

Soil classification AP and SCS values input by user
 USER INPUT of soil data for subarea
 SCS curve number for soil(AMC 2) = 31.98

Pervious ratio(Ap) = 0.3170 Max loss rate(Fm) = 0.310(In/Hr)
 Rainfall intensity = 2.042(In/Hr) for a 25.0 year storm
 User specified values are as follows:
 TC = 21.31 min. Rain intensity = 2.04(In/Hr)
 Total area this stream = 109.32(Ac.)
 Total Study Area (Main Stream No. 1) = 330.42(Ac.)
 Total runoff = 182.37(CFS)

++++++
 Process from Point/Station 38.000 to Point/Station 38.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 109.320(Ac.)
 Runoff from this stream = 182.370(CFS)
 Time of concentration = 21.31 min.
 Rainfall intensity = 2.042(In/Hr)
 Area averaged loss rate (Fm) = 0.3100(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.3170
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	338.411	21.84	2.012
2	182.370	21.31	2.042

Qmax(1) =
 1.000 * 1.000 * 338.411) +
 0.983 * 1.000 * 182.370) + = 517.654

Qmax(2) =
 1.017 * 0.976 * 338.411) +
 1.000 * 1.000 * 182.370) + = 518.256

Total of 2 streams to confluence:

Flow rates before confluence point:

338.411 182.370

Maximum flow rates at confluence using above data:

517.654 518.256

Area of streams before confluence:

185.759 109.320

Effective area values after confluence:

295.079 290.599

Results of confluence:

Total flow rate = 518.256(CFS)

Time of concentration = 21.310 min.

Effective stream area after confluence = 290.599(Ac.)

Stream Area average Pervious fraction(Ap) = 0.315

Stream Area average soil loss rate(Fm) = 0.287(In/Hr)

Study area (this main stream) = 295.08(Ac.)

++++++
 Process from Point/Station 38.000 to Point/Station 39.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1035.000(Ft.)

Downstream point/station elevation = 1026.600(Ft.)

Pipe length = 990.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 518.256(CFS)

Given pipe size = 84.00(In.)
 Calculated individual pipe flow = 518.256(CFS)
 Normal flow depth in pipe = 61.22(In.)
 Flow top width inside pipe = 74.69(In.)
 Critical Depth = 71.20(In.)
 Pipe flow velocity = 17.26(Ft/s)
 Travel time through pipe = 0.96 min.
 Time of concentration (TC) = 22.27 min.

++++++
 Process from Point/Station 39.000 to Point/Station 39.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 290.599(Ac.)
 Runoff from this stream = 518.256(CFS)
 Time of concentration = 22.27 min.
 Rainfall intensity = 1.989(In/Hr)
 Area averaged loss rate (Fm) = 0.2866(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.3153

++++++
 Process from Point/Station 817.000 to Point/Station 818.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwt/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1049.000(Ft.)
 Bottom (of initial area) elevation = 1044.000(Ft.)
 Difference in elevation = 5.000(Ft.)
 Slope = 0.00500 s(%) = 0.50
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 17.789 min.
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.707
 Subarea runoff = 8.039(CFS)
 Total initial stream area = 5.000(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.489(In/Hr)

++++++
 Process from Point/Station 818.000 to Point/Station 819.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1044.000(Ft.)
 End of street segment elevation = 1042.300(Ft.)
 Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020

Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 12.059(CFS)
 Depth of flow = 0.426(Ft.), Average velocity = 2.144(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 16.557(Ft.)
 Flow velocity = 2.14(Ft/s)
 Travel time = 2.57 min. TC = 20.35 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwt/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.489(In/Hr)
 Rainfall intensity = 2.099(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method)(Q=KCIA) is C = 0.690
 Subarea runoff = 6.449(CFS) for 5.000(Ac.)
 Total runoff = 14.488(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 340.42(Ac.)
 Area averaged Fm value = 0.489(In/Hr)
 Street flow at end of street = 14.488(CFS)
 Half street flow at end of street = 7.244(CFS)
 Depth of flow = 0.450(Ft.), Average velocity = 2.243(Ft/s)
 Flow width (from curb towards crown) = 17.772(Ft.)

++++++
 Process from Point/Station 819.000 to Point/Station 820.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1042.300(Ft.)
 End of street segment elevation = 1039.000(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 21.732(CFS)
 Depth of flow = 0.509(Ft.), Average velocity = 2.494(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:

Halfstreet flow width = 20.000(Ft.)
 Flow velocity = 2.49(Ft/s)
 Travel time = 4.41 min. TC = 24.77 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.489(In/Hr)
 Rainfall intensity = 1.866(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.664
 Subarea runoff = 10.294(CFS) for 10.000(Ac.)
 Total runoff = 24.782(CFS)
 Effective area this stream = 20.00(Ac.)
 Total Study Area (Main Stream No. 1) = 350.42(Ac.)
 Area averaged Fm value = 0.489(In/Hr)
 Street flow at end of street = 24.782(CFS)
 Half street flow at end of street = 12.391(CFS)
 Depth of flow = 0.527(Ft.), Average velocity = 2.627(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown) = 20.000(Ft.)

++++++
 Process from Point/Station 820.000 to Point/Station 821.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1039.000(Ft.)
 End of street segment elevation = 1037.000(Ft.)
 Length of street segment = 330.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 30.977(CFS)
 Depth of flow = 0.701(Ft.), Average velocity = 3.332(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 1.74(Ft.)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 30.325(Ft.)
 Flow velocity = 3.33(Ft/s)
 Travel time = 1.65 min. TC = 26.42 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00

Pervious ratio(A_p) = 0.5000 Max loss rate(F_m) = 0.489(In/Hr)
 Rainfall intensity = 1.795(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) ($Q=KCIA$) is $C = 0.655$
 Subarea runoff = 10.478(CFS) for 10.000(Ac.)
 Total runoff = 35.260(CFS)
 Effective area this stream = 30.00(Ac.)
 Total Study Area (Main Stream No. 1) = 360.42(Ac.)
 Area averaged F_m value = 0.489(In/Hr)
 Street flow at end of street = 35.260(CFS)
 Half street flow at end of street = 35.260(CFS)
 Depth of flow = 0.736(Ft.), Average velocity = 3.372(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 3.46(Ft.)
 Flow width (from curb towards crown) = 32.042(Ft.)

++++++
 Process from Point/Station 821.000 to Point/Station 821.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 30.000(Ac.)
 Runoff from this stream = 35.260(CFS)
 Time of concentration = 26.42 min.
 Rainfall intensity = 1.795(In/Hr)
 Area averaged loss rate (F_m) = 0.4889(In/Hr)
 Area averaged Pervious ratio (A_p) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	518.256	22.27	1.989
2	35.260	26.42	1.795
$Q_{max}(1) =$ $1.000 * 1.000 * 518.256) +$ $1.148 * 0.843 * 35.260) + = 552.387$			
$Q_{max}(2) =$ $0.886 * 1.000 * 518.256) +$ $1.000 * 1.000 * 35.260) + = 494.489$			

Total of 2 streams to confluence:

Flow rates before confluence point:

518.256 35.260

Maximum flow rates at confluence using above data:

552.387 494.489

Area of streams before confluence:

290.599 30.000

Effective area values after confluence:

315.885 320.599

Results of confluence:

Total flow rate = 552.387(CFS)

Time of concentration = 22.266 min.

Effective stream area after confluence = 315.885(Ac.)

Stream Area average Pervious fraction(A_p) = 0.333

Stream Area average soil loss rate(F_m) = 0.306(In/Hr)

Study area (this main stream) = 320.60(Ac.)

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Process from Point/Station      39.000 to Point/Station      40.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****

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Upstream point/station elevation = 1026.600(Ft.)
Downstream point/station elevation = 1012.800(Ft.)
Pipe length = 1720.00(Ft.)   Manning's N = 0.013
No. of pipes = 1   Required pipe flow = 552.387(CFS)
Given pipe size = 84.00(In.)
Calculated individual pipe flow = 552.387(CFS)
Normal flow depth in pipe = 66.38(In.)
Flow top width inside pipe = 68.41(In.)
Critical Depth = 73.04(In.)
Pipe flow velocity = 16.94(Ft/s)
Travel time through pipe = 1.69 min.
Time of concentration (TC) = 23.96 min.

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Process from Point/Station      40.000 to Point/Station      40.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 1
Stream flow area = 315.885(Ac.)
Runoff from this stream = 552.387(CFS)
Time of concentration = 23.96 min.
Rainfall intensity = 1.903(In/Hr)
Area averaged loss rate (Fm) = 0.3055(In/Hr)
Area averaged Pervious ratio (Ap) = 0.3326

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Process from Point/Station      822.000 to Point/Station      823.000
**** INITIAL AREA EVALUATION ****

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RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 32.00
Pervious ratio(Ap) = 0.5000   Max loss rate(Fm)= 0.489(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1037.700(Ft.)
Bottom (of initial area) elevation = 1034.300(Ft.)
Difference in elevation = 3.400(Ft.)
Slope = 0.00340   s(%)= 0.34
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 19.216 min.
Rainfall intensity = 2.172(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.697
Subarea runoff = 7.576(CFS)
Total initial stream area = 5.000(Ac.)
Pervious area fraction = 0.500
Initial area Fm value = 0.489(In/Hr)

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Process from Point/Station      823.000 to Point/Station      824.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

```

Top of street segment elevation = 1034.300(Ft.)
 End of street segment elevation = 1032.000(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 20.000(Ft.)
 Distance from crown to crossfall grade break = 18.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [2] side(s) of the street
 Distance from curb to property line = 10.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 11.364(CFS)
 Depth of flow = 0.444(Ft.), Average velocity = 1.823(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 17.451(Ft.)
 Flow velocity = 1.82(Ft/s)
 Travel time = 6.03 min. TC = 25.25 min.
 Adding area flow to street
 RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.489(In/Hr)
 Rainfall intensity = 1.844(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.661
 Subarea runoff = 4.621(CFS) for 5.000(Ac.)
 Total runoff = 12.198(CFS)
 Effective area this stream = 10.00(Ac.)
 Total Study Area (Main Stream No. 1) = 370.42(Ac.)
 Area averaged Fm value = 0.489(In/Hr)
 Street flow at end of street = 12.198(CFS)
 Half street flow at end of street = 6.099(CFS)
 Depth of flow = 0.454(Ft.), Average velocity = 1.855(Ft/s)
 Flow width (from curb towards crown) = 17.933(Ft.)

++++++
 Process from Point/Station 824.000 to Point/Station 825.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1032.000(Ft.)
 End of street segment elevation = 1027.000(Ft.)
 Length of street segment = 660.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)

Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 18.296(CFS)
 Depth of flow = 0.566(Ft.), Average velocity = 3.262(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 23.533(Ft.)
 Flow velocity = 3.26(Ft/s)
 Travel time = 3.37 min. TC = 28.62 min.
 Adding area flow to street
 CONDOMINIUM subarea type
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Rainfall intensity = 1.711(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.681
 Subarea runoff = 11.112(CFS) for 10.000(Ac.)
 Total runoff = 23.310(CFS)
 Effective area this stream = 20.00(Ac.)
 Total Study Area (Main Stream No. 1) = 380.42(Ac.)
 Area averaged Fm value = 0.416(In/Hr)
 Street flow at end of street = 23.310(CFS)
 Half street flow at end of street = 23.310(CFS)
 Depth of flow = 0.611(Ft.), Average velocity = 3.464(Ft/s)
 Flow width (from curb towards crown)= 25.802(Ft.)

++++++
 Process from Point/Station 825.000 to Point/Station 826.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1027.000(Ft.)
 End of street segment elevation = 1023.000(Ft.)
 Length of street segment = 750.000(Ft.)
 Height of curb above gutter flowline = 8.0(In.)
 Width of half street (curb to crown) = 42.000(Ft.)
 Distance from crown to crossfall grade break = 40.500(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.000(Ft.)
 Slope from curb to property line (v/hz) = 0.020
 Gutter width = 1.500(Ft.)
 Gutter hike from flowline = 1.500(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 26.806(CFS)
 Depth of flow = 0.679(Ft.), Average velocity = 3.112(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 0.64(Ft.)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 29.221(Ft.)
 Flow velocity = 3.11(Ft/s)
 Travel time = 4.02 min. TC = 32.64 min.
 Adding area flow to street

CONDOMINIUM subarea type

Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
 Rainfall intensity = 1.581(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.673
 Subarea runoff = 4.356(CFS) for 6.000(Ac.)
 Total runoff = 27.666(CFS)
 Effective area this stream = 26.00(Ac.)
 Total Study Area (Main Stream No. 1) = 386.42(Ac.)
 Area averaged Fm value = 0.399(In/Hr)
 Street flow at end of street = 27.666(CFS)
 Half street flow at end of street = 27.666(CFS)
 Depth of flow = 0.688(Ft.), Average velocity = 3.116(Ft/s)
 Warning: depth of flow exceeds top of curb
 Distance that curb overflow reaches into property = 1.07(Ft.)
 Flow width (from curb towards crown)= 29.657(Ft.)

++++++
 Process from Point/Station 826.000 to Point/Station 826.000
 **** CONFLUENCE OF MINOR STREAMS ****

 Along Main Stream number: 1 in normal stream number 2

Stream flow area = 26.000(Ac.)
 Runoff from this stream = 27.666(CFS)
 Time of concentration = 32.64 min.
 Rainfall intensity = 1.581(In/Hr)
 Area averaged loss rate (Fm) = 0.3986(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.4077
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	552.387	23.96	1.903
2	27.666	32.64	1.581
Qmax(1) =			
	1.000 *	1.000 *	552.387) +
	1.273 *	0.734 *	27.666) + = 578.231
Qmax(2) =			
	0.798 *	1.000 *	552.387) +
	1.000 *	1.000 *	27.666) + = 468.647

Total of 2 streams to confluence:

Flow rates before confluence point:

552.387 27.666

Maximum flow rates at confluence using above data:

578.231 468.647

Area of streams before confluence:

315.885 26.000

Effective area values after confluence:

334.971 341.885

Results of confluence:

Total flow rate = 578.231(CFS)

Time of concentration = 23.959 min.

Effective stream area after confluence = 334.971(Ac.)
 Stream Area average Pervious fraction(Ap) = 0.338
 Stream Area average soil loss rate(Fm) = 0.313(In/Hr)
 Study area (this main stream) = 341.88(Ac.)

+++++
 Process from Point/Station 40.000 to Point/Station 94.000
 **** PIPEFLOW TRAVEL TIME (User specified size) ****

Upstream point/station elevation = 1011.300(Ft.)
 Downstream point/station elevation = 1004.000(Ft.)
 Pipe length = 900.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 578.231(CFS)
 Given pipe size = 102.00(In.)
 Calculated individual pipe flow = 578.231(CFS)
 Normal flow depth in pipe = 56.91(In.)
 Flow top width inside pipe = 101.31(In.)
 Critical Depth = 72.44(In.)
 Pipe flow velocity = 17.78(Ft/s)
 Travel time through pipe = 0.84 min.
 Time of concentration (TC) = 24.80 min.

+++++
 Process from Point/Station 94.000 to Point/Station 94.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 334.971(Ac.)
 Runoff from this stream = 578.231(CFS)
 Time of concentration = 24.80 min.
 Rainfall intensity = 1.864(In/Hr)
 Area averaged loss rate (Fm) = 0.3126(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.3383

+++++
 Process from Point/Station 827.000 to Point/Station 828.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 1.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 32.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
 Initial subarea data:
 Initial area flow distance = 900.000(Ft.)
 Top (of initial area) elevation = 1023.000(Ft.)
 Bottom (of initial area) elevation = 1014.000(Ft.)
 Difference in elevation = 9.000(Ft.)
 Slope = 0.01000 s(%)= 1.00
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 14.847 min.
 Rainfall intensity = 2.536(In/Hr) for a 25.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.726
 Subarea runoff = 11.055(CFS)
 Total initial stream area = 6.000(Ac.)
 Pervious area fraction = 0.500

Initial area Fm value = 0.489(In/Hr)

+++++
 Process from Point/Station 828.000 to Point/Station 828.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 6.000(Ac.)
 Runoff from this stream = 11.055(CFS)
 Time of concentration = 14.85 min.
 Rainfall intensity = 2.536(In/Hr)
 Area averaged loss rate (Fm) = 0.4889(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5000
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	578.231	24.80	1.864
2	11.055	14.85	2.536

Qmax(1) =
 1.000 * 1.000 * 578.231) +
 0.672 * 1.000 * 11.055) + = 585.656
 Qmax(2) =
 1.433 * 0.599 * 578.231) +
 1.000 * 1.000 * 11.055) + = 507.139

Total of 2 streams to confluence:

Flow rates before confluence point:
 578.231 11.055

Maximum flow rates at confluence using above data:
 585.656 507.139

Area of streams before confluence:
 334.971 6.000

Effective area values after confluence:
 340.971 206.522

Results of confluence:

Total flow rate = 585.656(CFS)
 Time of concentration = 24.802 min.
 Effective stream area after confluence = 340.971(Ac.)
 Stream Area average Pervious fraction(Ap) = 0.341
 Stream Area average soil loss rate(Fm) = 0.316(In/Hr)
 Study area (this main stream) = 340.97(Ac.)
 End of computations, Total Study Area = 392.42 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.343

Area averaged SCS curve number = 36.8

DECLERZ CHL.

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4
Rational Hydrology Study Date: 01/13/05

FONTANA / DECLEZ CHANNEL HYDROLOGY
25 YEAR STORM
JN 04339

Hall & Forman, Inc. - S/N 950

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 25.0
10 Year storm 1 hour rainfall = 0.930(In.)
100 Year storm 1 hour rainfall = 1.350(In.)
Computed rainfall intensity:
Storm year = 25.00 1 hour rainfall = 1.097 (In.)
Slope used for rainfall intensity curve b = 0.6000
Soil antecedent moisture condition (AMC) = 2

+++++
Process from Point/Station 93.000 to Point/Station 93.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Soil classification AP and SCS values input by user
USER INPUT of soil data for subarea
SCS curve number for soil(AMC 2) = 67.05
Pervious ratio(Ap) = 0.5160 Max loss rate(Fm)= 0.298(In/Hr)
Rainfall intensity = 2.394(In/Hr) for a 25.0 year storm
User specified values are as follows:
TC = 16.34 min. Rain intensity = 2.39(In/Hr)
Total area this stream = 816.23(Ac.)
Total Study Area (Main Stream No. 1) = 816.23(Ac.)
Total runoff = 2004.30(CFS)

+++++
Process from Point/Station 93.000 to Point/Station 94.000
**** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 1005.500(Ft.)
Downstream point elevation = 1004.000(Ft.)
Channel length thru subarea = 500.000(Ft.)
Channel base width = 24.000(Ft.)
Slope or 'Z' of left channel bank = 0.000
Slope or 'Z' of right channel bank = 0.000
Manning's 'N' = 0.015
Maximum depth of channel = 9.000(Ft.)
Flow(q) thru subarea = 2004.300(CFS)
Depth of flow = 6.075(Ft.), Average velocity = 13.748(Ft/s)
Channel flow top width = 24.000(Ft.)
Flow Velocity = 13.75(Ft/s)
Travel time = 0.61 min.
Time of concentration = 16.95 min.

Critical depth = 6.000(Ft.)

+++++
Process from Point/Station 94.000 to Point/Station 94.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 816.230(Ac.)
Runoff from this stream = 2004.300(CFS)
Time of concentration = 16.95 min.
Rainfall intensity = 2.343(In/Hr)
Area averaged loss rate (Fm) = 0.2980(In/Hr)
Area averaged Pervious ratio (Ap) = 0.5160

+++++
Process from Point/Station 94.000 to Point/Station 94.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****

Soil classification AP and SCS values input by user
USER INPUT of soil data for subarea
SCS curve number for soil(AMC 2) = 38.89
Pervious ratio(Ap) = 0.3410 Max loss rate(Fm)= 0.316(In/Hr)
Rainfall intensity = 1.864(In/Hr) for a 25.0 year storm
User specified values are as follows:
TC = 24.80 min. Rain intensity = 1.86(In/Hr)
Total area this stream = 340.97(Ac.)
Total Study Area (Main Stream No. 1) = 1157.20(Ac.)
Total runoff = 585.66(CFS)

+++++
Process from Point/Station 94.000 to Point/Station 94.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 340.970(Ac.)
Runoff from this stream = 585.660(CFS)
Time of concentration = 24.80 min.
Rainfall intensity = 1.864(In/Hr)
Area averaged loss rate (Fm) = 0.3160(In/Hr)
Area averaged Pervious ratio (Ap) = 0.3410
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	2004.300	16.95	2.343
2	585.660	24.80	1.864

Qmax(1) =
1.000 * 1.000 * 2004.300) +
1.309 * 0.683 * 585.660) + = 2528.181

Qmax(2) =
0.766 * 1.000 * 2004.300) +
1.000 * 1.000 * 585.660) + = 2120.895

Total of 2 streams to confluence:
Flow rates before confluence point:
2004.300 585.660

Maximum flow rates at confluence using above data:

2528.181 2120.895

Area of streams before confluence:

816.230 340.970

Effective area values after confluence:

1049.219 1157.200

Results of confluence:

Total flow rate = 2528.181(CFS)

Time of concentration = 16.946 min.

Effective stream area after confluence = 1049.219(Ac.)

Stream Area average Pervious fraction(A_p) = 0.464

Stream Area average soil loss rate(F_m) = 0.303(In/Hr)

Study area (this main stream) = 1157.20(Ac.)

End of computations, Total Study Area = 1157.20 (Ac.)

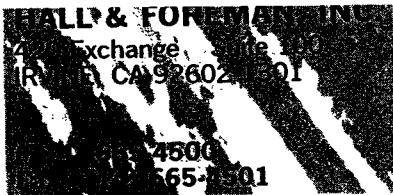
The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction(A_p) = 0.464

Area averaged SCS curve number = 58.8



4500 Exchange, Suite 100
Riverside, CA 92502-1501

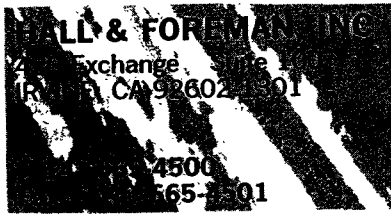
4500
565-1501

FONTANA

JOB No. 04339
BY HERMAN
DATE
SHT. 1649
OF

◆ LAND PLANNING ◆ CIVIL ENGINEERING ◆ SURVEYING

HYDRAULICS



JOB No. _____
BY _____
DATE _____
SHT. 1650
OF _____

◆ LAND PLANNING ◆ CIVIL ENGINEERING ◆ SURVEYING

25 YEAR

T1 FONTANA / DECLEZ CHANNEL W/O DETENTION (AMC2) 0
 0
 T2 25 YEAR STORM
 T3 JN 04339
 SO 23300.0001002.670 1 1002.670
 R 24100.0001005.070 1 .014 .000
 .000 0
 JX 24100.0101005.070 1 2 .014 524.000 1005.070 .0
 .000
 R 24242.1201005.500 1 .014 .000
 WX 24242.1201005.500 3
 R 24242.1301005.500 3 .013 .000
 .000 0
 SH 24242.1301005.500 3 1005.500
 CD 1 2 0 .000 11.000 24.000 .000 .000 .00
 CD 2 4 1 .000 9.000 .000 .000 .000 .00
 CD 3 3 0 .000 9.000 14.000 .000 .000 .00
 Q 2004.000 .0

FILE: DECLEZOCH.WSW

W S P G W - EDIT LISTING - Version 14.05

Date: 1-16-2005 Time: 3:33:50

WATER SURFACE PROFILE - CHANNEL DEFINITION LISTING

PAGE 1

CARD CODE	SECT NO	CHN TYPE	NO OF PIER/PIP	AVE PIER WIDTH	HEIGHT 1 DIAMETER	BASE WIDTH	ZL	ZR	INV DROP	Y(1)	Y(2)	Y(3)	Y(4)	Y(5)	Y(6)	Y(7)	Y(8)	Y(9)	Y(10)
CD	1	2	0	.000	11.000	24.000			.00										
CD	2	4	1		9.000														
CD	3	3	0	.000	9.000	14.000	.000	.000	.00										

W S P G W

PAGE NO 1

WATER SURFACE PROFILE - TITLE CARD LISTING

HEADING LINE NO 1 IS -

FONTANA / DECLEZ CHANNEL W/O DETENTION (AMC2)

0

HEADING LINE NO 2 IS -

25 YEAR STORM

HEADING LINE NO 3 IS -

JN 04339

W S P G W

PAGE NO 2

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	1 IS A	SYSTEM OUTLET	U/S DATA	STATION	INVERT	SECT	W S ELEV												
				23300.000	1002.670	1	1002.670												
ELEMENT NO	2	IS A REACH	U/S DATA	STATION	INVERT	SECT		N		RADIUS	ANGLE	ANG PT	MAN H						
				24100.000	1005.070	1		.014		.000	.000	.000	0						
ELEMENT NO	3	IS A JUNCTION	U/S DATA	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4				
				24100.010	1005.070	1	2	0	.014	524.000	.000	1005.070	.000	.000	.000	.000			
												RADIUS	ANGLE						
												.000	.000						
THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING																			
THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING																			
ELEMENT NO	4	IS A REACH	U/S DATA	STATION	INVERT	SECT		N		RADIUS	ANGLE	ANG PT	MAN H						
				24242.120	1005.500	1		.014		.000	.000	.000	0						
ELEMENT NO	5	IS A WALL EXIT	U/S DATA	STATION	INVERT	SECT													
				24242.120	1005.500	3													
ELEMENT NO	6	IS A REACH	U/S DATA	STATION	INVERT	SECT		N		RADIUS	ANGLE	ANG PT	MAN H						
				24242.130	1005.500	3		.013		.000	.000	.000	0						
ELEMENT NO	7	IS A SYSTEM HEADWORKS	U/S DATA	STATION	INVERT	SECT													
				24242.130	1005.500	3						W S ELEV	1005.500						

Date: 1-16-2005 Time: 3:33:34

0

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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height/ | Base Wt | | No Wth
      | Elev  | (FT)  | Elev  | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip
L/Elem | Ch Slope | | | | | | | | | | | | | |
***** | | | | | | | | | | | | | | | |
23300.000 | 1002.670 | 6.806 | 1009.476 | 2528.00 | 15.48 | 3.72 | 1013.20 | .00 | 7.01 | 24.00 | 11.000 | 24.000 | .00 | 0 .0
      | | | | | | | | | | | | | | | |
722.635 | .0030 | | | | | | | | | | | | | | | |
24022.630 | 1004.838 | 6.806 | 1011.644 | 2528.00 | 15.48 | 3.72 | 1015.36 | .00 | 7.01 | 24.00 | 11.000 | 24.000 | .00 | 0 .0
      | | | | | | | | | | | | | | | |
77.365 | .0030 | | | | | | | | | | | | | | | |
24100.000 | 1005.070 | 7.010 | 1012.080 | 2528.00 | 15.03 | 3.51 | 1015.59 | .00 | 7.01 | 24.00 | 11.000 | 24.000 | .00 | 0 .0
      | | | | | | | | | | | | | | | |
JUNCT STR | .0000 | | | | | | | | | | | | | | | |
24100.010 | 1005.070 | 9.499 | 1014.569 | 2004.00 | 8.79 | 1.20 | 1015.77 | .00 | 6.01 | 24.00 | 11.000 | 24.000 | .00 | 0 .0
      | | | | | | | | | | | | | | | |
142.109 | .0030 | | | | | | | | | | | | | | | |
24242.120 | 1005.500 | 9.064 | 1014.564 | 2004.00 | 9.21 | 1.32 | 1015.88 | .00 | 6.01 | 24.00 | 11.000 | 24.000 | .00 | 0 .0
      | | | | | | | | | | | | | | | |
WALL EXIT | | | | | | | | | | | | | | | |
24242.120 | 1005.500 | 9.064 | 1014.564 | 2004.00 | 15.90 | 3.93 | 1018.49 | .00 | 8.60 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | | | |
.012 | .0000 | | | | | | | | | | | | | | | |
24242.130 | 1005.500 | 9.064 | 1014.564 | 2004.00 | 15.90 | 3.93 | 1018.49 | .00 | 8.60 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | | | |

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T1 FONTANA / JURUPA AVE. 14'x 9' RCB W/O DETENTION (AMC2)
 O
 T2 25 YEAR STORM
 T3 JN 04339
 SO 7990.5001005.500 1 1016.140
 R 8003.0701005.530 1 .013 .000
 .000 0
 R 8143.7401005.810 1 .013 -89.554
 .000 0
 R 8600.0001006.720 1 .013 .000
 .000 0
 R 9200.0001009.720 1 .013 .000
 .000 0
 JX 9200.0101009.720 1 2 .013 33.000 1013.220 -45.0
 .000
 R 9680.0001012.120 1 .013 .000
 .000 0
 R 9770.0001012.930 1 .013 .000
 .000 0
 JX 9770.0101012.930 1 2 .013 28.000 1015.400 45.0
 .000
 R 9770.0201012.930 1 .013 .000
 .000 0
 JX 9770.0301012.930 1 3 .013 138.000 1015.400 45.0
 .000
 R 9790.0001013.090 1 .013 .000
 .000 0
 JX 9790.0101013.090 1 4 .013 100.000 1014.500 -45.0
 .000
 R 10700.0001019.670 1 .013 .000
 .000 0
 R 11000.0001021.870 1 .013 .000
 .000 0
 R 11108.0001022.300 1 .013 .000
 .000 0
 JX 11108.0101022.300 1 5 6.013 64.000 118.0001025.0001025.000 45.0-45.0
 .000
 R 12357.7301027.300 1 .013 .000
 .000 0
 R 12503.4001027.860 1 .013 -39.369
 .000 0
 JX 12503.4101028.860 8 7 1.013 48.000 728.0001029.9201027.860 45.0 .0
 .000
 R 12528.3001028.900 8 .013 30.000
 .000 0
 SH 12528.3001028.900 8 1028.900
 CD 1 3 0 .000 9.000 14.000 .000 .000 .00
 CD 2 4 1 .000 3.000 .000 .000 .000 .00
 CD 3 4 1 .000 3.500 .000 .000 .000 .00
 CD 4 4 1 .000 5.000 .000 .000 .000 .00
 CD 5 4 1 .000 4.000 .000 .000 .000 .00
 CD 6 4 1 .000 4.500 .000 .000 .000 .00
 CD 7 4 1 .000 4.000 .000 .000 .000 .00
 CD 8 4 1 .000 8.000 .000 .000 .000 .00
 Q 747.000 .0

WATER SURFACE PROFILE - CHANNEL DEFINITION LISTING

PAGE 1

CARD CODE	SECT NO	CHN TYPE	NO OF PIER/PIP	AVE PIER WIDTH	HEIGHT 1 DIAMETER	BASE WIDTH	ZL	ZR	INV DROP	Y(1)	Y(2)	Y(3)	Y(4)	Y(5)	Y(6)	Y(7)	Y(8)	Y(9)	Y(10)
CD	1	3	0	.000	9.000	14.000	.000	.000	.00										
CD	2	4	1		3.000														
CD	3	4	1		3.500														
CD	4	4	1		5.000														
CD	5	4	1		4.000														
CD	6	4	1		4.500														
CD	7	4	1		4.000														
CD	8	4	1		8.000														

W S P G W

PAGE NO 1

WATER SURFACE PROFILE - TITLE CARD LISTING

HEADING LINE NO 1 IS -

FONTANA / JURUPA AVE. 14'x 9' RCB W/O DETENTION (AMC2)

HEADING LINE NO 2 IS -

100 YEAR STORM

HEADING LINE NO 3 IS -

JN 04339

W S P G W

PAGE NO 2

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	1 IS A	SYSTEM OUTLET	U/S DATA	STATION	INVERT	SECT	W S ELEV												
ELEMENT NO	2 IS A	REACH	U/S DATA	STATION	INVERT	SECT													
				7990.500	1005.500	1	1016.140												
ELEMENT NO	3 IS A	REACH	U/S DATA	STATION	INVERT	SECT													
				8003.070	1005.530	1		N	.013			RADIUS	ANGLE	ANG PT	MAN H				
												.000	.000	.000	0				
ELEMENT NO	4 IS A	REACH	U/S DATA	STATION	INVERT	SECT													
				8143.740	1005.810	1		N	.013			RADIUS	ANGLE	ANG PT	MAN H				
												90.000	-89.554	.000	0				
ELEMENT NO	5 IS A	REACH	U/S DATA	STATION	INVERT	SECT													
				8600.000	1006.720	1		N	.013			RADIUS	ANGLE	ANG PT	MAN H				
												.000	.000	.000	0				
ELEMENT NO	6 IS A	JUNCTION	U/S DATA	STATION	INVERT	SECT													
				9200.000	1009.720	1		N	.013			RADIUS	ANGLE	ANG PT	MAN H				
												.000	.000	.000	0				
				STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4				
				9200.010	1009.720	1	2	0	.013	33.000	.000	1013.220	.000	-45.000	.000				
												RADIUS	ANGLE						
												.000	.000						
THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING																			
THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING																			
ELEMENT NO	7 IS A	REACH	U/S DATA	STATION	INVERT	SECT													
				9680.000	1012.120	1		N	.013			RADIUS	ANGLE	ANG PT	MAN H				
												.000	.000	.000	0				
ELEMENT NO	8 IS A	REACH	U/S DATA	STATION	INVERT	SECT													
				9770.000	1012.930	1		N	.013			RADIUS	ANGLE	ANG PT	MAN H				
												.000	.000	.000	0				
ELEMENT NO	9 IS A	JUNCTION	U/S DATA	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4				
				9770.010	1012.930	1	2	0	.013	28.000	.000	1015.400	.000	45.000	.000				

THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING
 THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING

RADIUS
.000
ANGLE
.000

W S P G W

PAGE NO 3

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO 10 IS A REACH
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H
 9770.020 1012.930 1 .013 .000 .000 .000 0
 ELEMENT NO 11 IS A JUNCTION
 U/S DATA STATION INVERT SECT LAT-1 LAT-2 N Q3 Q4 INVERT-3 INVERT-4 PHI 3 PHI 4
 9770.030 1012.930 1 3 0 .013 138.000 .000 1015.400 .000 45.000 .000
 RADIUS ANGLE
 .000 .000

THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING
 THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING

ELEMENT NO 12 IS A REACH
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H
 9790.000 1013.090 1 .013 .000 .000 .000 0
 ELEMENT NO 13 IS A JUNCTION
 U/S DATA STATION INVERT SECT LAT-1 LAT-2 N Q3 Q4 INVERT-3 INVERT-4 PHI 3 PHI 4
 9790.010 1013.090 1 4 0 .013 100.000 .000 1014.500 .000 -45.000 .000
 RADIUS ANGLE
 .000 .000

THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING
 THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING

ELEMENT NO 14 IS A REACH
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H
 10700.000 1019.670 1 .013 .000 .000 .000 0
 ELEMENT NO 15 IS A REACH
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H
 11000.000 1021.870 1 .013 .000 .000 .000 0
 ELEMENT NO 16 IS A REACH
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H
 11108.000 1022.300 1 .013 .000 .000 .000 0
 ELEMENT NO 17 IS A JUNCTION
 U/S DATA STATION INVERT SECT LAT-1 LAT-2 N Q3 Q4 INVERT-3 INVERT-4 PHI 3 PHI 4
 11108.010 1022.300 1 5 6 .013 64.000 118.000 1025.000 1025.000 45.000 -45.000
 RADIUS ANGLE
 .000 .000

THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING
 THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING

W S P G W

PAGE NO 4

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO 18 IS A REACH
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H
 12357.730 1027.300 1 .013 .000 .000 .000 0
 ELEMENT NO 19 IS A REACH
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H
 12503.400 1027.860 1 .013 212.001 -39.369 .000 0
 ELEMENT NO 20 IS A JUNCTION
 U/S DATA STATION INVERT SECT LAT-1 LAT-2 N Q3 Q4 INVERT-3 INVERT-4 PHI 3 PHI 4
 12503.410 1028.860 8 7 1 .013 48.000 728.000 1029.920 1027.860 45.000 .000
 RADIUS ANGLE

ELEMENT NO	21	IS A REACH	*	*	*
		U/S DATA	STATION	INVERT	SECT
			12528.300	1028.900	8
ELEMENT NO	22	IS A SYSTEM HEADWORKS			*
		U/S DATA	STATION	INVERT	SECT
			12528.300	1028.900	8

N
.013

*

	.000	.000		
	RADIUS	ANGLE	ANG PT	MAN H
	47.536	30.000	.000	0
	W S ELEV			
	1028.900			

Program Package Serial Number: 1432

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 4: 2:35

FONTANA / JURUPA AVE. 14'x 9' RCB W/O DETENTION (AMC2)

100 YEAR STORM

JN 04339

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt/or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
7990.500	1005.500	10.640	1016.140	2004.00	15.90	3.93	1020.07	.00	8.60	14.00	9.000	14.000	.00	0 .0
12.570	.0024					.0051	.06	10.64	.93	9.00	.013	.00	.00	BOX
8003.070	1005.530	10.673	1016.203	2004.00	15.90	3.93	1020.13	.00	8.60	14.00	9.000	14.000	.00	0 .0
140.670	.0020					.0051	.71	.00	.93	9.00	.013	.00	.00	BOX
8143.740	1005.810	11.888	1017.698	2004.00	15.90	3.93	1021.63	.00	8.60	14.00	9.000	14.000	.00	0 .0
456.260	.0020					.0051	2.30	11.89	.93	9.00	.013	.00	.00	BOX
8600.000	1006.720	13.283	1020.003	2004.00	15.90	3.93	1023.93	.00	8.60	14.00	9.000	14.000	.00	0 .0
600.000	.0050					.0051	3.03	13.28	.93	7.51	.013	.00	.00	BOX
9200.000	1009.720	13.313	1023.033	2004.00	15.90	3.93	1026.96	.00	8.60	14.00	9.000	14.000	.00	0 .0
JUNCT STR	.0000					.0049	.00	13.31	.93		.013	.00	.00	BOX
9200.010	1009.720	13.543	1023.263	1971.00	15.64	3.80	1027.06	.00	8.51	14.00	9.000	14.000	.00	0 .0
479.990	.0050					.0049	2.35	13.54	.92	7.41	.013	.00	.00	BOX
9680.000	1012.120	13.489	1025.609	1971.00	15.64	3.80	1029.41	.00	8.51	14.00	9.000	14.000	.00	0 .0
90.000	.0090					.0049	.44	13.49	.92	5.96	.013	.00	.00	BOX
9770.000	1012.930	13.119	1026.049	1971.00	15.64	3.80	1029.85	.00	8.51	14.00	9.000	14.000	.00	0 .0
JUNCT STR	.0000					.0047	.00	13.12	.92		.013	.00	.00	BOX
9770.020	1012.930	13.314	1026.244	1943.00	15.42	3.69	1029.94	.00	8.43	14.00	9.000	14.000	.00	0 .0
JUNCT STR	.0000					.0041	.00	13.31	.91		.013	.00	.00	BOX

Program Package Serial Number: 1432

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 4: 2:35

FONTANA / JURUPA AVE. 14'x 9' RCB W/O DETENTION (AMC2)

100 YEAR STORM

JN 04339

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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height | Base Wt | | No Wth
      | Elev  | (FT)  | Elev  | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip
L/Elem | Ch Slope | | | | | | | | | | | | | |
***** | | | | | | | | | | | | | |
9770.030 | 1012.930 | 13.981 | 1026.911 | 1805.00 | 14.33 | 3.19 | 1030.10 | .00 | 8.02 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | |
19.970 | .0080 | | | | | | | | | | | | | |
      | | | | | | | | | | | | | |
9790.000 | 1013.090 | 13.902 | 1026.992 | 1805.00 | 14.33 | 3.19 | 1030.18 | .00 | 8.02 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | |
JUNCT STR | .0000 | | | | | | | | | | | | | |
      | | | | | | | | | | | | | |
9790.010 | 1013.090 | 14.500 | 1027.590 | 1705.00 | 13.53 | 2.84 | 1030.43 | .00 | 7.72 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | |
909.990 | .0072 | | | | | | | | | | | | | |
      | | | | | | | | | | | | | |
10700.000 | 1019.670 | 11.248 | 1030.918 | 1705.00 | 13.53 | 2.84 | 1033.76 | .00 | 7.72 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | |
300.000 | .0073 | | | | | | | | | | | | | |
      | | | | | | | | | | | | | |
11000.000 | 1021.870 | 10.145 | 1032.015 | 1705.00 | 13.53 | 2.84 | 1034.86 | .00 | 7.72 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | |
108.000 | .0040 | | | | | | | | | | | | | |
      | | | | | | | | | | | | | |
11108.000 | 1022.300 | 10.109 | 1032.409 | 1705.00 | 13.53 | 2.84 | 1035.25 | .00 | 7.72 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | |
JUNCT STR | .0000 | | | | | | | | | | | | | |
      | | | | | | | | | | | | | |
11108.010 | 1022.300 | 11.049 | 1033.349 | 1523.00 | 12.09 | 2.27 | 1035.62 | .00 | 7.16 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | |
1249.721 | .0040 | | | | | | | | | | | | | |
      | | | | | | | | | | | | | |
12357.730 | 1027.300 | 9.695 | 1036.995 | 1523.00 | 12.09 | 2.27 | 1039.26 | .00 | 7.16 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | |
145.670 | .0038 | | | | | | | | | | | | | |
      | | | | | | | | | | | | | |
12503.400 | 1027.860 | 9.861 | 1037.721 | 1523.00 | 12.09 | 2.27 | 1039.99 | .00 | 7.16 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | |
JUNCT STR | ***** | | | | | | | | | | | | | |
      | | | | | | | | | | | | | |

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----- WARNING - Junction Analysis - Change in Channel Type -----

Program Package Serial Number: 1432

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 4: 2:35

FONTANA / JURUPA AVE. 14'x 9' RCB W/O DETENTION (AMC2)

100 YEAR STORM

JN 04339

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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height/ | Base Wt | | No Wth
      | Elev  | (FT)  | Elev  | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip
L/Elem | Ch Slope | | | | | | | | | | | | | | |
*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****
12503.410 | 1028.860 | 9.908 | 1038.768 | 747.00 | 14.86 | 3.43 | 1042.20 | .00 | 6.87 | .00 | 8.000 | .000 | .00 | 1 .0
      | 24.890 | .0016 | | | | | | | | | | | | | | |
      | | | | | | | | | | | | | | |
12528.300 | 1028.900 | 10.431 | 1039.331 | 747.00 | 14.86 | 3.43 | 1042.76 | .00 | 6.87 | .00 | 8.000 | .000 | .00 | 1 .0
      | | | | | | | | | | | | | | |

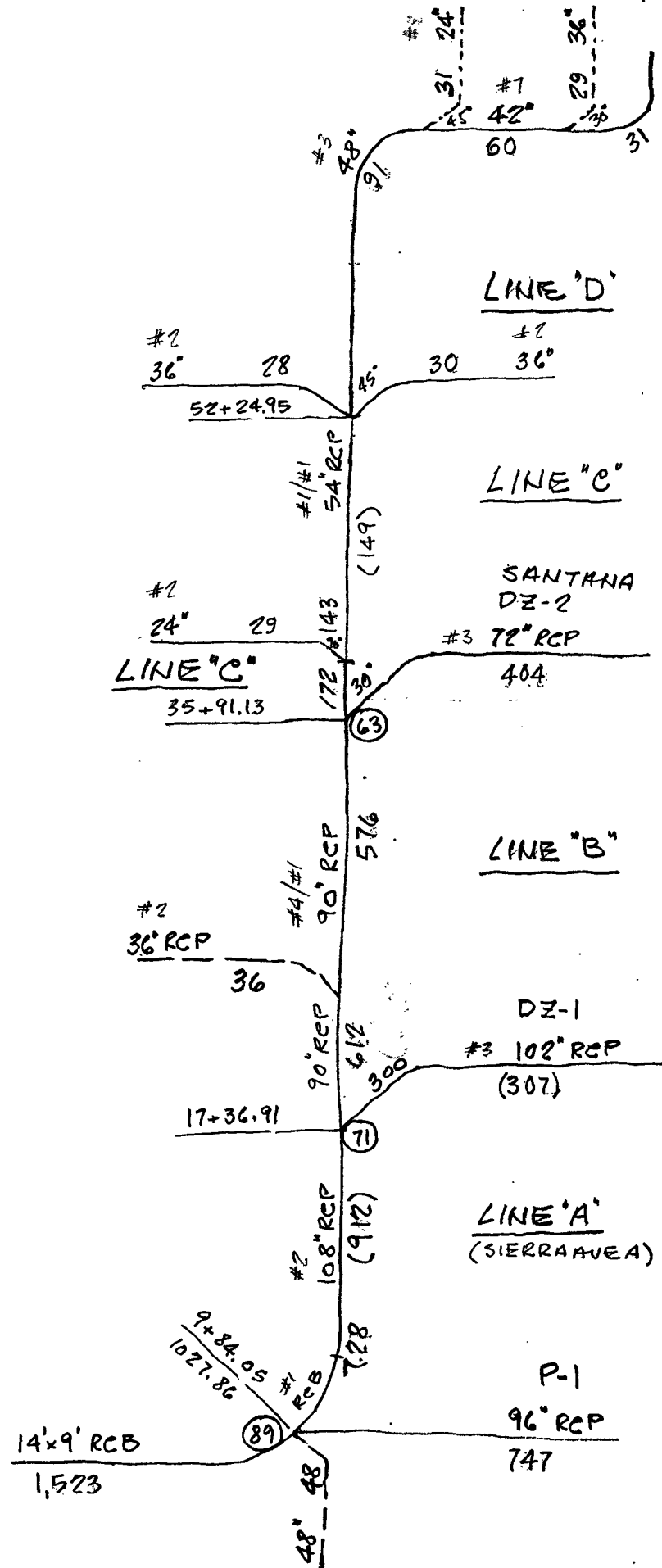
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SIERRA AVE. W/O DETENTION
FONTANA 7 (in computer)

JN04339

1662

25 YR.



↑
N
(307) Peak Q
300 Confluent Q

T1 FONTANA / SIERRA AVE. LINE"A"

0

T2 25 YEAR STORM

T3 JN 04339

SO 984.0501027.860 1

1038.770

R 1055.5801028.170 1 .013

-19.332

.000 0

TS 1085.5801028.290 2 .014

-8.108

R 1735.6001030.240 2 .013

.000

.000 0

JX 1757.8401031.790 4 3 .014 300.000

1030.640

30.0

.000

R 1757.8501031.790 4 .013

.000

.000 0

SH 1757.8501031.790 4

1031.790

CD 1 3 0 .000 9.000 14.000 .000 .000 .00

CD 2 4 1 .000 9.000 .000 .000 .000 .00

CD 3 4 1 .000 8.500 .000 .000 .000 .00

CD 4 4 1 .000 7.500 .000 .000 .000 .00

Q 612.000 .0

FILE: SIERRAAVEA.WSW

W S P G W - EDIT LISTING - Version 14.05

Date: 1-16-2005 Time: 4:58: 1

WATER SURFACE PROFILE - CHANNEL DEFINITION LISTING

PAGE 1

CARD CODE	SECT NO	CHN TYPE	NO OF PIER/PIP	AVE PIER WIDTH	HEIGHT 1 DIAMETER	BASE WIDTH	ZL	ZR	INV DROP	Y(1)	Y(2)	Y(3)	Y(4)	Y(5)	Y(6)	Y(7)	Y(8)	Y(9)	Y(10)
CD	1	3	0	.000	9.000	14.000	.000	.000	.00										
CD	2	4	1		9.000														
CD	3	4	1		8.500														
CD	4	4	1		7.500														

W S P G W

PAGE NO 1

WATER SURFACE PROFILE - TITLE CARD LISTING

HEADING LINE NO 1 IS -

FONTANA / SIERRA AVE. LINE"A"

HEADING LINE NO 2 IS -

25 YEAR STORM

HEADING LINE NO 3 IS -

JN 04339

W S P G W

PAGE NO 2

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	1 IS A	SYSTEM OUTLET	U/S DATA	STATION	INVERT	SECT	W S ELEV												
				984.050	1027.860	1	1038.770												
ELEMENT NO	2 IS A	REACH	U/S DATA	STATION	INVERT	SECT													
				1055.580	1028.170	1													
ELEMENT NO	3 IS A	TRANSITION	U/S DATA	STATION	INVERT	SECT													
				1085.580	1028.290	2													
ELEMENT NO	4 IS A	REACH	U/S DATA	STATION	INVERT	SECT													
				1735.600	1030.240	2													
ELEMENT NO	5 IS A	JUNCTION	U/S DATA	STATION	INVERT	SECT													
				1757.840	1031.790	4													
ELEMENT NO	6 IS A	REACH	U/S DATA	STATION	INVERT	SECT													
				1757.850	1031.790	4													
ELEMENT NO	7 IS A	SYSTEM HEADWORKS	U/S DATA	STATION	INVERT	SECT													
				1757.850	1031.790	4													

W S ELEV
1031.790

Program Package Serial Number: 1432

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 4:57:20

FONTANA / SIERRA AVE. LINE"A"

25 YEAR STORM

JN 04339

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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height/ | Base Wt | | No Wth
         | Elev   | (FT)  | Elev   | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip
L/Elem  | Ch Slope |          |          |          |          | SF Ave | HF | SE Dpth | Froude N | Norm Dp | "N" | X-Fall | ZR | Type Ch
*****
984.050 | 1027.860 | 10.910 | 1038.770 | 912.00 | 7.24 | .81 | 1039.58 | .00 | 5.09 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |
71.530 | .0043 |         |         |         |         | .0010 | .07 | .00 | .43 | 4.44 | .013 | .00 | .00 | BOX
1055.580 | 1028.170 | 10.750 | 1038.920 | 912.00 | 7.24 | .81 | 1039.73 | .00 | 5.09 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |
TRANS STR | .0040 |         |         |         |         | .0034 | .10 | .00 | .43 |         | .014 | .00 | .00 | BOX
1085.580 | 1028.290 | 8.801 | 1037.091 | 912.00 | 14.42 | 3.23 | 1040.32 | .00 | 7.42 | 2.65 | 9.000 | .000 | .00 | 1 .0
         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |
83.053 | .0030 |         |         |         |         | .0050 | .41 | 8.80 | .52 | 9.00 | .013 | .00 | .00 | PIPE
1168.633 | 1028.539 | 9.000 | 1037.539 | 912.00 | 14.34 | 3.19 | 1040.73 | .00 | 7.42 | .00 | 9.000 | .000 | .00 | 1 .0
         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |
566.967 | .0030 |         |         |         |         | .0053 | 2.98 | 9.00 | .00 | 9.00 | .013 | .00 | .00 | PIPE
1735.600 | 1030.240 | 10.324 | 1040.564 | 912.00 | 14.34 | 3.19 | 1043.76 | .00 | 7.42 | .00 | 9.000 | .000 | .00 | 1 .0
         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |
JUNCT STR | .0697 |         |         |         |         | .0068 | .15 | 10.32 | .00 |         | .014 | .00 | .00 | PIPE
1757.840 | 1031.790 | 10.781 | 1042.571 | 612.00 | 13.85 | 2.98 | 1045.55 | .00 | 6.34 | .00 | 7.500 | .000 | .00 | 1 .0
         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |
.010 | .0000 |         |         |         |         | .0064 | .00 | 10.78 | .00 | .00 | .013 | .00 | .00 | PIPE
1757.850 | 1031.790 | 10.781 | 1042.572 | 612.00 | 13.85 | 2.98 | 1045.55 | .00 | 6.34 | .00 | 7.500 | .000 | .00 | 1 .0
         |         |         |         |         |         |         |         |         |         |         |         |         |         |         |

```

T1 FONTANA / SIERRA AVE. LINE"B"

0

T2 25 YEAR STORM

T3 JN 04339

SO 1757.8501031.790 1

1042.570

R 2441.5001034.530 1

.013

.000

.000 0

JX 2441.5101034.530 1 2

.013

36.000

1039.150

-90.0

.000

R 3590.5801039.120 1

.013

.000

.000 0

JX 3607.6501039.990 4 3

.014

172.000

1042.180

.0

30.000

R 3607.6601039.990 4

.013

.000

.000 0

SH 3607.6601039.990 4

1039.990

CD 1 4 1 .000 7.500

.000

.000

.000

.00

CD 2 4 1 .000 3.000

.000

.000

.000

.00

CD 3 4 1 .000 4.500

.000

.000

.000

.00

CD 4 4 1 .000 6.000

.000

.000

.000

.00

Q 404.000 .0

Program Package Serial Number: 1432

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 5: 4: 0

FONTANA / SIERRA AVE. LINE"B"

25 YEAR STORM

JN 04339

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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height/ | Base Wt | ZL | No Wth
      | Elev   | (FT)  | Elev   | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. |    | Prs/Pip
L/Elem | Ch Slope |      |      |      |      | SF Ave | HF | SE Dpth | Froude N | Norm Dp | "N" | X-Fall | ZR | Type Ch
*****
1757.850 | 1031.790 | 10.780 | 1042.570 | 612.00 | 13.85 | 2.98 | 1045.55 | .00 | 6.34 | .00 | 7.500 | .000 | .00 | 1 .0
      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |
683.650 | .0040 |      |      |      |      | .0064 | 4.34 | 10.78 | .00 | 7.50 | .013 | .00 | .00 | PIPE
2441.500 | 1034.530 | 12.383 | 1046.913 | 612.00 | 13.85 | 2.98 | 1049.89 | .00 | 6.34 | .00 | 7.500 | .000 | .00 | 1 .0
      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |
JUNCT STR | .0000 |      |      |      |      | .0060 | .00 | 12.38 | .00 | .00 | .013 | .00 | .00 | PIPE
2441.510 | 1034.530 | 13.063 | 1047.593 | 576.00 | 13.04 | 2.64 | 1050.23 | .00 | 6.18 | .00 | 7.500 | .000 | .00 | 1 .0
      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |
1149.070 | .0040 |      |      |      |      | .0056 | 6.47 | 13.06 | .00 | 7.50 | .013 | .00 | .00 | PIPE
3590.580 | 1039.120 | 14.939 | 1054.059 | 576.00 | 13.04 | 2.64 | 1056.70 | .00 | 6.18 | .00 | 7.500 | .000 | .00 | 1 .0
      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |
JUNCT STR | .0510 |      |      |      |      | .0085 | .15 | .00 | .00 | .00 | .014 | .00 | .00 | PIPE
3607.650 | 1039.990 | 14.109 | 1054.099 | 404.00 | 14.29 | 3.17 | 1057.27 | .00 | 5.35 | .00 | 6.000 | .000 | .00 | 1 .0
      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |
      | .010 | .0000 |      |      |      |      | .0091 | .00 | 14.11 | .00 | .00 | .013 | .00 | .00 | PIPE
3607.660 | 1039.990 | 14.109 | 1054.099 | 404.00 | 14.29 | 3.17 | 1057.27 | .00 | 5.35 | .00 | 6.000 | .000 | .00 | 1 .0
      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |

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T1 FONTANA / SIERRA AVE. LINE"C"

0

T2 25 YEAR STORM

T3 JN 04339

SO	3607.3301042.180	1				1054.100	
R	3787.6901051.310	1		.013			.000
	.000 0						
JX	3794.3501051.480	1	2	.014	29.000	1052.860	-85.0
	.000						
R	3794.3601051.480	1		.013			.000
	.000 0						
SH	3794.3601051.480	1				1051.480	
CD	1 4 1	.000	4.500	.000	.000	.000	.00
CD	2 4 1	.000	2.000	.000	.000	.000	.00
Q		149.000	.0				

FILE: SIERRAAVEC.WSW

W S P G W - EDIT LISTING - Version 14.05

Date: 1-16-2005 Time: 5:23: 1

WATER SURFACE PROFILE - CHANNEL DEFINITION LISTING

PAGE 1

CARD CODE	SECT NO	CHN TYPE	NO OF PIER/PIP	AVE WIDTH	PIER DIAMETER	HEIGHT 1 BASE	WIDTH	ZL	ZR	INV DROP	Y(1)	Y(2)	Y(3)	Y(4)	Y(5)	Y(6)	Y(7)	Y(8)	Y(9)	Y(10)
CD	1	4	1		4.500															
CD	2	4	1		2.000															

W S P G W

PAGE NO 1

WATER SURFACE PROFILE - TITLE CARD LISTING

HEADING LINE NO 1 IS -
FONTANA / SIERRA AVE. LINE"C"
HEADING LINE NO 2 IS -
25 YEAR STORM
HEADING LINE NO 3 IS -
JN 04339

W S P G W

PAGE NO 2

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	IS	A	SYSTEM OUTLET	U/S DATA	STATION	INVERT	SECT	W S ELEV	RADIUS	ANGLE	ANG PT	MAN H
ELEMENT NO 1	IS	A	SYSTEM OUTLET	U/S DATA	3607.330	1042.180	1	1054.100				
ELEMENT NO 2	IS	A	REACH	U/S DATA	3787.690	1051.310	1					
ELEMENT NO 3	IS	A	JUNCTION	U/S DATA	3794.350	1051.480	1					
ELEMENT NO 4	IS	A	REACH	U/S DATA	3794.360	1051.480	1					
ELEMENT NO 5	IS	A	SYSTEM HEADWORKS	U/S DATA	3794.360	1051.480	1					

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 5:21:58

FONTANA / SIERRA AVE. LINE"C"

25 YEAR STORM

JN 04339

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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height/ | Base Wt | | No Wth
      | Elev  | (FT)  | Elev  | (CFS) | (FPS) | Head | Grd.El. | Elev  | Depth  | Width  | Dia.-FT | or I.D. | ZL | Prs/Pip
L/Elem | Ch Slope | | | | | | | | | | | | | | |
*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****
3607.330 | 1042.180 | 11.920 | 1054.100 | 178.00 | 11.19 | 1.95 | 1056.05 | .00 | 3.87 | .00 | 4.500 | .000 | .00 | 1 .0
      | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
174.884 | .0506 | | | | | | | | | | | | | | |
      | | | | | | | | | | | | | | |
3782.214 | 1051.033 | 4.500 | 1055.533 | 178.00 | 11.19 | 1.95 | 1057.48 | .00 | 3.87 | .00 | 4.500 | .000 | .00 | 1 .0
      | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
5.173 | .0506 | | | | | | | | | | | | | | |
      | | | | | | | | | | | | | | |
3787.386 | 1051.295 | 4.082 | 1055.377 | 178.00 | 11.74 | 2.14 | 1057.52 | .00 | 3.87 | 2.61 | 4.500 | .000 | .00 | 1 .0
      | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
.303 | .0506 | | | | | | | | | | | | | | |
      | | | | | | | | | | | | | | |
3787.690 | 1051.310 | 4.025 | 1055.335 | 178.00 | 11.86 | 2.18 | 1057.52 | .00 | 3.87 | 2.77 | 4.500 | .000 | .00 | 1 .0
      | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
JUNCT STR | .0255 | | | | | | | | | | | | | | |
      | | | | | | | | | | | | | | |
3794.350 | 1051.480 | 5.295 | 1056.775 | 149.00 | 9.37 | 1.36 | 1058.14 | .00 | 3.58 | .00 | 4.500 | .000 | .00 | 1 .0
      | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
.010 | .0000 | | | | | | | | | | | | | | |
      | | | | | | | | | | | | | | |
3794.360 | 1051.480 | 5.295 | 1056.775 | 149.00 | 9.37 | 1.36 | 1058.14 | .00 | 3.58 | .00 | 4.500 | .000 | .00 | 1 .0
      | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

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T1 FONTANA / SIERRA AVE. LINE"D"

0

T2 25 YEAR STORM

T3 JN 04339

SO	3794.3601051.480	1				1056.780		
R	5219.3701065.020	1		.013				.000
	.000 0							
JX	5227.2801055.560	3	2	2.014	30.000	28.0001066.2001066.200	45.0-45.0	
	.000							
R	5602.4801069.340	5		.013				.000
	.000 0							
JX	5607.1401069.880	7		.014				
R	6270.8101076.000	7		.013				.000
	.000 0							
R	6343.0401076.740	7		.013				91.966
	.000 0							
R	6358.1601076.720	7		.013				.000
	.000 0							
JX	6362.8301076.740	7	8	.014	31.000	1077.500		-45.0
	.000							
R	6763.1801078.340	7		.013				.000
	.000 0							
JX	6773.1801078.370	7	2	.014	29.000	1078.650		-30.0
	.000							
R	7239.9301080.330	7		.013				.000
	.000 0							
R	7373.4301081.000	7		.013				.000
	.000 0							
R	7387.9301081.070	7		.013				.000
	.000 0							
SH	7387.9301081.070	7				1081.070		
CD	1 4 1	.000	4.500	.000	.000	.000	.00	
CD	2 4 1	.000	3.000	.000	.000	.000	.00	
CD	3 4 1	.000	4.000	.000	.000	.000	.00	
CD	5 4 1	.000	4.000	.000	.000	.000	.00	
CD	7 4 1	.000	3.500	.000	.000	.000	.00	
CD	8 4 1	.000	2.000	.000	.000	.000	.00	
Q		31.000	.0					

WATER SURFACE PROFILE - CHANNEL DEFINITION LISTING

PAGE 1

CARD CODE	SECT NO	CHN TYPE	NO OF PIER/PIP	AVE PIER WIDTH	HEIGHT 1 DIAMETER	BASE WIDTH	ZL	ZR	INV DROP	Y(1)	Y(2)	Y(3)	Y(4)	Y(5)	Y(6)	Y(7)	Y(8)	Y(9)	Y(10)
CD	1	4	1		4.500														
CD	2	4	1		3.000														
CD	3	4	1		4.000														
CD	5	4	1		4.000														
CD	7	4	1		3.500														
CD	8	4	1		2.000														

W S P G W

PAGE NO 1

WATER SURFACE PROFILE - TITLE CARD LISTING

HEADING LINE NO 1 IS -

FONTANA / SIERRA AVE. LINE"D"

HEADING LINE NO 2 IS -

25 YEAR STORM

HEADING LINE NO 3 IS -

JN 04339

W S P G W

PAGE NO 2

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	1 IS A SYSTEM OUTLET	U/S DATA	STATION	INVERT	SECT	W S ELEV	RADIUS	ANGLE	ANG PT	MAN H				
			3794.360	1051.480	1	1056.780								
ELEMENT NO 2	IS A REACH	U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H				
			5219.370	1065.020	1	.013	.000	.000	.000	0				
ELEMENT NO 3	IS A JUNCTION	U/S DATA	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4
			5227.280	1055.560	3	2	2	.014	30.000	28.000	1066.200	1066.200	45.000	-45.000
							RADIUS	ANGLE						
							.000	.000						

THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING

THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING

WARNING - ADJACENT SECTIONS ARE NOT IDENTICAL - SEE SECTION NUMBERS AND CHANNEL DEFINITIONS

ELEMENT NO	4 IS A REACH	U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H				
			5602.480	1069.340	5	.013	.000	.000	.000	0				
ELEMENT NO 5	IS A JUNCTION	U/S DATA	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4
			5607.140	1069.880	7	0	0	.014	.000	.000	.000	.000	.000	.000
							RADIUS	ANGLE						
							.000	.000						
ELEMENT NO 6	IS A REACH	U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H				
			6270.810	1076.000	7	.013	.000	.000	.000	0				
ELEMENT NO 7	IS A REACH	U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H				
			6343.040	1076.740	7	.013	45.000	91.966	.000	0				
ELEMENT NO 8	IS A REACH	U/S DATA	STATION	INVERT	SECT	N	RADIUS	ANGLE	ANG PT	MAN H				
			6358.160	1076.720	7	.013	.000	.000	.000	0				

THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING

ELEMENT NO 9 IS A JUNCTION

U/S DATA	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4
	6362.830	1076.740	7	8	0	.014	31.000	.000	1077.500	.000	-45.000	.000
									RADIUS	ANGLE		
									.000	.000		

PAGE NO 3

W S P G W
WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	IS A	REACH	U/S DATA	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4	RADIUS	ANGLE	ANG PT	MAN H
10	IS A	REACH	U/S DATA	6763.180	1078.340	7			.013							.000	.000	.000	0
11	IS A	JUNCTION	U/S DATA	6773.180	1078.370	7	2	0	.014	29.000	.000	1078.650	.000	-30.000	.000	.000	.000		
12	IS A	REACH	U/S DATA	7239.930	1080.330	7			.013							.000	.000	.000	0
13	IS A	REACH	U/S DATA	7373.430	1081.000	7			.013							.000	.000	.000	0
14	IS A	REACH	U/S DATA	7387.930	1081.070	7			.013							.000	.000	.000	0
15	IS A	SYSTEM HEADWORKS	U/S DATA	7387.930	1081.070	7													

W S ELEV
1081.070

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 5:33:13

FONTANA / SIERRA AVE. LINE"D"
25 YEAR STORM
JN 04339

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt/or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
3794.360	1051.480	5.300	1056.780	149.00	9.37	1.36	1058.14	.00	3.58	.00	4.500	.000	.00	1 .0
212.739	.0095					.0057	1.21	5.30	.00	2.98	.013	.00	.00	PIPE
4007.099	1053.501	4.500	1058.001	149.00	9.37	1.36	1059.36	.00	3.58	.00	4.500	.000	.00	1 .0
44.426	.0095					.0053	.24	4.50	.00	2.98	.013	.00	.00	PIPE
4051.525	1053.923	4.258	1058.182	149.00	9.57	1.42	1059.60	.00	3.58	2.03	4.500	.000	.00	1 .0
HYDRAULIC JUMP														
4051.525	1053.923	2.982	1056.905	149.00	13.32	2.75	1059.66	.00	3.58	4.26	4.500	.000	.00	1 .0
620.664	.0095					.0095	5.90	2.98	1.45	2.98	.013	.00	.00	PIPE
4672.188	1059.821	2.982	1062.803	149.00	13.32	2.75	1065.56	.00	3.58	4.26	4.500	.000	.00	1 .0
259.206	.0095					.0095	2.45	2.98	1.45	2.98	.013	.00	.00	PIPE
4931.395	1062.284	2.988	1065.272	149.00	13.28	2.74	1068.01	.00	3.58	4.25	4.500	.000	.00	1 .0
203.938	.0095					.0089	1.82	2.99	1.44	2.98	.013	.00	.00	PIPE
5135.333	1064.221	3.119	1067.341	149.00	12.67	2.49	1069.83	.00	3.58	4.15	4.500	.000	.00	1 .0
55.949	.0095					.0080	.45	3.12	1.33	2.98	.013	.00	.00	PIPE
5191.282	1064.753	3.259	1068.012	149.00	12.08	2.26	1070.28	.00	3.58	4.02	4.500	.000	.00	1 .0
22.196	.0095					.0071	.16	3.26	1.22	2.98	.013	.00	.00	PIPE
5213.478	1064.964	3.412	1068.376	149.00	11.51	2.06	1070.44	.00	3.58	3.85	4.500	.000	.00	1 .0
5.892	.0095					.0064	.04	3.41	1.11	2.98	.013	.00	.00	PIPE

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 5:33:13

FONTANA / SIERRA AVE. LINE"D"

25 YEAR STORM

JN 04339

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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height | Base Wt | | No Wth
| Elev | (FT) | Elev | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip
L/Elem | Ch Slope | | | | | SF Ave | HF | SE Dpth | Froude N | Norm Dp | "N" | X-Fall | ZR | Type Ch
*****
5219.370 | 1065.020 | 3.582 | 1068.602 | 149.00 | 10.98 | 1.87 | 1070.47 | .00 | 3.58 | 3.63 | 4.500 | .000 | .00 | 1 | .0
JUNCT STR -1.1960 | | | | | .0058 | .05 | 3.58 | 1.00 | | .014 | .00 | .00 | PIPE
5227.280 | 1055.560 | 15.222 | 1070.782 | 91.00 | 7.24 | .81 | 1071.60 | .00 | 2.89 | .00 | 4.000 | .000 | .00 | 1 | .0
331.015 | .0367 | | | | .0040 | 1.33 | 15.22 | .00 | 1.58 | .013 | .00 | .00 | PIPE
5558.295 | 1067.717 | 4.393 | 1072.110 | 91.00 | 7.24 | .81 | 1072.92 | .00 | 2.89 | .00 | 4.000 | .000 | .00 | 1 | .0
HYDRAULIC JUMP
5558.295 | 1067.717 | 1.816 | 1069.533 | 91.00 | 16.40 | 4.18 | 1073.71 | .00 | 2.89 | 3.98 | 4.000 | .000 | .00 | 1 | .0
15.944 | .0367 | | | | .0213 | .34 | 1.82 | 2.45 | 1.58 | .013 | .00 | .00 | PIPE
5574.239 | 1068.303 | 1.869 | 1070.172 | 91.00 | 15.79 | 3.87 | 1074.05 | .00 | 2.89 | 3.99 | 4.000 | .000 | .00 | 1 | .0
15.945 | .0367 | | | | .0190 | .30 | 1.87 | 2.32 | 1.58 | .013 | .00 | .00 | PIPE
5590.184 | 1068.888 | 1.939 | 1070.827 | 91.00 | 15.06 | 3.52 | 1074.35 | .00 | 2.89 | 4.00 | 4.000 | .000 | .00 | 1 | .0
12.296 | .0367 | | | | .0168 | .21 | 1.94 | 2.16 | 1.58 | .013 | .00 | .00 | PIPE
5602.480 | 1069.340 | 2.014 | 1071.354 | 91.00 | 14.36 | 3.20 | 1074.56 | .00 | 2.89 | 4.00 | 4.000 | .000 | .00 | 1 | .0
JUNCT STR .1159 | | | | | .0144 | .07 | 2.01 | 2.01 | | .014 | .00 | .00 | PIPE
5607.140 | 1069.880 | 2.702 | 1072.582 | 91.00 | 11.42 | 2.02 | 1074.61 | .00 | 2.96 | 2.94 | 3.500 | .000 | .00 | 1 | .0
522.263 | .0092 | | | | .0092 | 4.82 | 2.70 | 1.22 | 2.70 | .013 | .00 | .00 | PIPE
6129.403 | 1074.696 | 2.702 | 1077.398 | 91.00 | 11.42 | 2.02 | 1079.42 | .00 | 2.96 | 2.94 | 3.500 | .000 | .00 | 1 | .0
141.407 | .0092 | | | | .0094 | 1.33 | 2.70 | 1.22 | 2.70 | .013 | .00 | .00 | PIPE

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WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 5:33:13

FONTANA / SIERRA AVE. LINE"D"

25 YEAR STORM

JN 04339

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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height/ | Base Wt | | No Wth
         | Elev   | (FT)  | Elev   | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip
L/Elem | Ch Slope |
***** |
6270.810 | 1076.000 | 2.649 | 1078.649 | 91.00 | 11.65 | 2.11 | 1080.76 | .28 | 2.96 | 3.00 | 3.500 | .000 | .00 | 1 .0
         | 19.022 | .0102 |         |         |         |         | .0095 | .18 | 2.93 | 1.27 | 2.58 | .013 | .00 | .00 | PIPE
6289.833 | 1076.195 | 2.671 | 1078.866 | 91.00 | 11.55 | 2.07 | 1080.94 | .27 | 2.96 | 2.98 | 3.500 | .000 | .00 | 1 .0
         | 44.009 | .0102 |         |         |         |         | .0090 | .40 | 2.94 | 1.25 | 2.58 | .013 | .00 | .00 | PIPE
6333.842 | 1076.646 | 2.804 | 1079.450 | 91.00 | 11.01 | 1.88 | 1081.33 | .23 | 2.96 | 2.79 | 3.500 | .000 | .00 | 1 .0
         | 9.198 | .0102 |         |         |         |         | .0082 | .07 | 3.04 | 1.13 | 2.58 | .013 | .00 | .00 | PIPE
6343.040 | 1076.740 | 2.957 | 1079.697 | 91.00 | 10.49 | 1.71 | 1081.41 | .00 | 2.96 | 2.53 | 3.500 | .000 | .00 | 1 .0
         | 1.916 | -.0013 |         |         |         |         | .0075 | .01 | 2.96 | 1.00 | .00 | .013 | .00 | .00 | PIPE
6344.956 | 1076.737 | 3.105 | 1079.842 | 91.00 | 10.09 | 1.58 | 1081.42 | .00 | 2.96 | 2.22 | 3.500 | .000 | .00 | 1 .0
         | 6.074 | -.0013 |         |         |         |         | .0072 | .04 | 3.10 | .88 | .00 | .013 | .00 | .00 | PIPE
6351.030 | 1076.729 | 3.260 | 1079.990 | 91.00 | 9.75 | 1.48 | 1081.47 | .00 | 2.96 | 1.77 | 3.500 | .000 | .00 | 1 .0
         | 7.130 | -.0013 |         |         |         |         | .0071 | .05 | 3.26 | .75 | .00 | .013 | .00 | .00 | PIPE
6358.160 | 1076.720 | 3.375 | 1080.095 | 91.00 | 9.57 | 1.42 | 1081.52 | .00 | 2.96 | 1.30 | 3.500 | .000 | .00 | 1 .0
JUNCT STR | .0043 |         |         |         |         |         | .0062 | .03 | 3.38 | .62 |         | .014 | .00 | .00 | PIPE
6362.830 | 1076.740 | 4.293 | 1081.033 | 60.00 | 6.24 | .60 | 1081.64 | .00 | 2.43 | .00 | 3.500 | .000 | .00 | 1 .0
         | 400.350 | .0040 |         |         |         |         | .0036 | 1.42 | 4.29 | .00 | 2.71 | .013 | .00 | .00 | PIPE
6763.180 | 1078.340 | 4.117 | 1082.457 | 60.00 | 6.24 | .60 | 1083.06 | .00 | 2.43 | .00 | 3.500 | .000 | .00 | 1 .0
JUNCT STR | .0030 |         |         |         |         |         | .0026 | .03 | 4.12 | .00 |         | .014 | .00 | .00 | PIPE

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Program Package Serial Number: 1432

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 5:33:13

FONTANA / SIERRA AVE. LINE"D"

25 YEAR STORM

JN 04339

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*****
Station  | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height/ | Base Wt | | No Wth |
          | Elev   | (FT)  | Elev   | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip |
L/Elem   | Ch Slope |          |          |          |          | SF Ave | HF | SE Dpth | Froude N | Norm Dp | "N" | X-Fall | ZR | Type Ch |
*****
6773.180 | 1078.370 | 4.666 | 1083.036 | 31.00 | 3.22 | .16 | 1083.20 | .00 | 1.72 | .00 | 3.500 | .000 | .00 | 1 .0 |
          | .0042 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
358.822 | .0042 | - | - | - | - | - | - | - | - | - | - | - | - | - |
          | .0009 | .34 | 4.67 | .00 | 1.70 | .013 | .00 | .00 | PIPE |
7132.002 | 1079.877 | 3.500 | 1083.377 | 31.00 | 3.22 | .16 | 1083.54 | .00 | 1.72 | .00 | 3.500 | .000 | .00 | 1 .0 |
          | .0042 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
92.816 | .0042 | - | - | - | - | - | - | - | - | - | - | - | - | - |
          | .0009 | .08 | 3.50 | .00 | 1.70 | .013 | .00 | .00 | PIPE |
7224.818 | 1080.266 | 3.175 | 1083.442 | 31.00 | 3.38 | .18 | 1083.62 | .00 | 1.72 | 2.03 | 3.500 | .000 | .00 | 1 .0 |
          | .0042 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
15.112 | .0042 | - | - | - | - | - | - | - | - | - | - | - | - | - |
          | .0008 | .01 | 3.18 | .28 | 1.70 | .013 | .00 | .00 | PIPE |
7239.930 | 1080.330 | 3.120 | 1083.450 | 31.00 | 3.42 | .18 | 1083.63 | .00 | 1.72 | 2.18 | 3.500 | .000 | .00 | 1 .0 |
          | .0050 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
38.474 | .0050 | - | - | - | - | - | - | - | - | - | - | - | - | - |
          | .0009 | .03 | 3.12 | .30 | 1.61 | .013 | .00 | .00 | PIPE |
7278.404 | 1080.523 | 2.942 | 1083.465 | 31.00 | 3.59 | .20 | 1083.67 | .00 | 1.72 | 2.56 | 3.500 | .000 | .00 | 1 .0 |
          | .0050 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
31.728 | .0050 | - | - | - | - | - | - | - | - | - | - | - | - | - |
          | .0010 | .03 | 2.94 | .34 | 1.61 | .013 | .00 | .00 | PIPE |
7310.132 | 1080.682 | 2.793 | 1083.475 | 31.00 | 3.77 | .22 | 1083.70 | .00 | 1.72 | 2.81 | 3.500 | .000 | .00 | 1 .0 |
          | .0050 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
27.727 | .0050 | - | - | - | - | - | - | - | - | - | - | - | - | - |
          | .0011 | .03 | 2.79 | .39 | 1.61 | .013 | .00 | .00 | PIPE |
7337.858 | 1080.822 | 2.661 | 1083.483 | 31.00 | 3.95 | .24 | 1083.72 | .00 | 1.72 | 2.99 | 3.500 | .000 | .00 | 1 .0 |
          | .0050 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
24.883 | .0050 | - | - | - | - | - | - | - | - | - | - | - | - | - |
          | .0012 | .03 | 2.66 | .43 | 1.61 | .013 | .00 | .00 | PIPE |
7362.741 | 1080.946 | 2.541 | 1083.488 | 31.00 | 4.14 | .27 | 1083.75 | .00 | 1.72 | 3.12 | 3.500 | .000 | .00 | 1 .0 |
          | .0050 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
10.689 | .0050 | - | - | - | - | - | - | - | - | - | - | - | - | - |
          | .0013 | .01 | 2.54 | .47 | 1.61 | .013 | .00 | .00 | PIPE |
7373.430 | 1081.000 | 2.489 | 1083.489 | 31.00 | 4.24 | .28 | 1083.77 | .00 | 1.72 | 3.17 | 3.500 | .000 | .00 | 1 .0 |
          | .0048 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
14.500 | .0048 | - | - | - | - | - | - | - | - | - | - | - | - | - |
          | .0013 | .02 | 2.49 | .49 | 1.63 | .013 | .00 | .00 | PIPE |

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Date: 1-16-2005 Time: 5:33:13

FONTANA / SIERRA AVE. LINE"D"
25 YEAR STORM
JN 04339

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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height | Base Wt | | No Wth
      | Elev | (FT) | Elev | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip
L/Elem | Ch Slope | | | | | | | | | | | | | | |
*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****
7387.930 | 1081.070 | 2.422 | 1083.492 | 31.00 | 4.36 | .30 | 1083.79 | .00 | 1.72 | 3.23 | 3.500 | .000 | .00 | 1 | .0
      | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | -
```



FONTANA

JOB No. 04339
BY HERMAN
DATE 1/19/05
SHT. 99
OF

◆ LAND PLANNING ◆ CIVIL ENGINEERING ◆ SURVEYING

HYDRAULICS

FOR

INDIVIDUAL PIPES



Hall & Foreman, Inc.

Subject CHECK MASTER PLAN

STORM DRAIN PIPE SIZES

By HERMAN

Dept. IRVINE

Date 8/6/04

Project Name FONTANA

Project No. 04339

Page No. (1) of

NODES	ΔH	L	S	Q_{25}	Given Size	?	Proposed Size
* DZ-2A							
55-54	1.7	340	0.0045	125	63"	✓	
54-53	4.3	860	0.0045	112	60"	✓	
53-52	2.5	500	0.0045	82	42"	X	48"
52-116	7.7	650	0.0108	51	39"	✓	
* DZ-2							
63-57	1.8	560	0.0029	404	87"	✓	
57-56	2.0	640	0.0029	343	84"	✓	
56-55	3.2	1000	0.0029	259	78"	✓	
55-51	8.9	900	0.009	70	42"	✓	
51-50	8.2	1,320	0.0056	49	39"	✓	
* 50-102	5.8	460	0.0117		24"	Built	
* 50-105	4.3	570	0.0068		30"	Built	
* DZ-1							
71-70	4.0	800	0.0045	* 408	102"	✓	
70-69	4.2	880	0.0043	* 280	102"	✓	
69-68	2.0	400	0.0045	* 250	93"	✓	
68-67	3.8	760	0.0045	* 160	84"	✓	
67-66	3.8	760	0.0045	* 131	75"	✓	
66-65	3.3	660	0.0045	* 67	57"	✓	
65-302	3.3	660	0.0045	* 49	36"	X	42"
70-331	4.0	800	0.0045	* 71	42"	✓	
68-319	13.0	900	0.0126	* 75	48"	✓	
* DZ-4							
90-45	15.0	750	0.018	104	42"	✓	
45-607	6.0	660	0.0081	70	36"	X	42"



Hall & Foreman, Inc.

Subject _____

Date _____

By _____

Project Name _____

Dept. _____

Project No. _____

Page No. (2) of _____

* DZ-4A							
91-46	11.5	750	0.0135	79	42"	✓	
46-629	7.3	660	0.0099	52	36"	✓	
* DZ-6							
35-34	6.2	660	0.0085	167	39"	X	54"
34-33	12.8	990	0.0117	122	39"	X	48"
33-717	14.0	990	0.0126	71	39"	✓	
* DZ-7							
38-37	5.5	660	0.0075	153	42"	X	54"
37-36	10.5	990	0.0095	118	42"	X	48"
36-803	15.0	990	0.0135	68	42"	✓	
* DZ-5							
94-40	7.3	900	0.0072		102"	Built	
40-39	13.8	1,720	0.0072	* 707	84"	X	96"
39-38	8.4	990	0.0077	* 680	84"	X	90"
38-35	8.0	1,320	0.0054	* 444	84"	✓	
35-32	11.0	1,320	0.0075	146	51"	✓	
32-31	4.6	660	0.0063	119	39"	X	48"
31-30	3.8	990	0.0034	82	39"	X	48"
30-704	10.0	990	0.0101	56	36"	✓	

*722 Indicates Q₁₀₀

LINE "DZ-2A"

Circular Channel Analysis & Design
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2A / INDIVIDUAL PIPE 55-54

Solve For Actual Depth

Given Input Data:

Diameter.....	5.25 ft
Slope.....	0.0045 ft/ft
Manning's n.....	0.013
Discharge.....	123.00 cfs

Computed Results:

Depth.....	2.99 ft
Velocity.....	9.67 fps
Flow Area.....	12.71 sf
Critical Depth....	3.13 ft
Critical Slope....	0.0039 ft/ft
Percent Full.....	56.88 %
Full Capacity.....	198.99 cfs
QMAX @.94D.....	214.05 cfs
Froude Number.....	1.09 (flow is Supercritical)

Circular Channel Analysis & Design
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2A / INDIVIDUAL PIPE 54-53

Solve For Actual Depth

Given Input Data:

Diameter.....	5.00 ft
Slope.....	0.0045 ft/ft
Manning's n.....	0.013
Discharge.....	109.00 cfs

Computed Results:

Depth.....	2.86 ft
Velocity.....	9.38 fps
Flow Area.....	11.61 sf
Critical Depth....	2.98 ft
Critical Slope....	0.0040 ft/ft
Percent Full.....	57.21 %
Full Capacity.....	174.71 cfs
QMAX @.94D.....	187.94 cfs
Froude Number.....	1.08 (flow is Supercritical)

Circular Channel Analysis & Design
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2A / INDIVIDUAL PIPE 53-52

Solve For Actual Depth

Given Input Data:

Diameter.....	4.00 ft
Slope.....	0.0045 ft/ft
Manning's n.....	0.013
Discharge.....	80.00 cfs

Computed Results:

Depth.....	2.78 ft
Velocity.....	8.57 fps
Flow Area.....	9.33 sf
Critical Depth....	2.71 ft
Critical Slope....	0.0048 ft/ft
Percent Full.....	69.55 %
Full Capacity.....	96.36 cfs
QMAX @.94D.....	103.65 cfs
Froude Number.....	0.95 (flow is Subcritical)

Circular Channel Analysis & Design
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2A / INDIVIDUAL PIPE 52-116

Solve For Actual Depth

Given Input Data:

Diameter.....	3.75 ft
Slope.....	0.0108 ft/ft
Manning's n.....	0.013
Discharge.....	49.00 cfs

Computed Results:

Depth.....	1.63 ft
Velocity.....	10.67 fps
Flow Area.....	4.59 sf
Critical Depth....	2.14 ft
Critical Slope....	0.0042 ft/ft
Percent Full.....	43.36 %
Full Capacity.....	125.68 cfs
QMAX @.94D.....	135.19 cfs
Froude Number.....	1.69 (flow is Supercritical)

LINE "DZ-2"

Circular Channel Analysis & Design
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2 / INDIVIDUAL PIPE 63-57

Solve For Actual Depth

Given Input Data:

Diameter.....	7.25 ft
Slope.....	0.0029 ft/ft
Manning's n.....	0.013
Discharge.....	398.00 cfs

Computed Results:

Depth.....	6.37 ft
Velocity.....	10.35 fps
Flow Area.....	38.44 sf
Critical Depth....	5.21 ft
Critical Slope....	0.0043 ft/ft
Percent Full.....	87.91 %
Full Capacity.....	377.77 cfs
QMAX @.94D.....	406.37 cfs
Froude Number.....	0.64 (flow is Subcritical)

Circular Channel Analysis & Design
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2 / INDIVIDUAL PIPE 57-56

Solve For Actual Depth

Given Input Data:

Diameter.....	7.00 ft
Slope.....	0.0029 ft/ft
Manning's n.....	0.013
Discharge.....	339.00 cfs

Computed Results:

Depth.....	5.65 ft
Velocity.....	10.19 fps
Flow Area.....	33.27 sf
Critical Depth....	4.85 ft
Critical Slope....	0.0041 ft/ft
Percent Full.....	80.67 %
Full Capacity.....	344.02 cfs
QMAX @.94D.....	370.07 cfs
Froude Number.....	0.73 (flow is Subcritical)

Circular Channel Analysis & Design
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2 / INDIVIDUAL PIPE 56-55

Solve For Actual Depth

Given Input Data:

Diameter.....	6.50 ft
Slope.....	0.0029 ft/ft
Manning's n.....	0.013
Discharge.....	256.00 cfs

Computed Results:

Depth.....	4.85 ft
Velocity.....	9.64 fps
Flow Area.....	26.56 sf
Critical Depth....	4.29 ft
Critical Slope....	0.0040 ft/ft
Percent Full.....	74.64 %
Full Capacity.....	282.33 cfs
QMAX @.94D.....	303.71 cfs
Froude Number.....	0.78 (flow is Subcritical)