

**CITY OF FONTANA**  
**SOUTH FONTANA MASTER DRAINAGE PLAN**  
**MASTER PLAN DRAINAGE STUDY**  
**FOR**

**EMPIRE CENTER AREA**

**FACILITIES:**

**P1, P2, P3, DZ-1, DZ-2, DZ-2A, DZ-3, DZ-4, DZ-5, DZ-6, & DZ-7**

**VOLUME NO. 2**

**PREPARED FOR: THE CITY OF FONTANA**

**STEVEN NAWAR, P.E. – PROJECT MANAGER**

**PREPARED BY: HALL & FOREMAN, INC.**

**43513 RIDGE PARK DRIVE  
TEMECULA, CA 92590  
(951) 676-6726**

**GERALD J. BARIL, P.E. – PROJECT MANAGER**

**HERMAN HOVAGIMYAN, P.E. – PROJECT ENGINEER**

**JANUARY 2005  
JN 04339**

**APPROVED**  
SN 3/22/05

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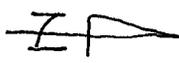
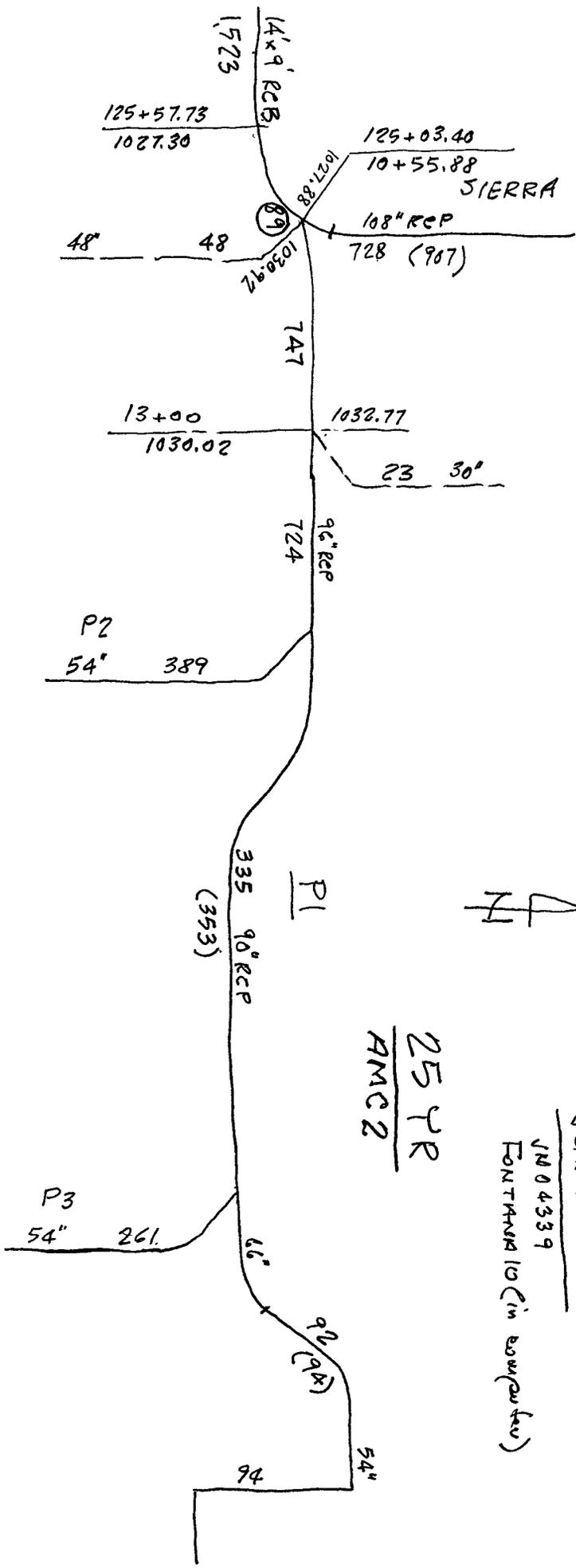
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## VOLUME NO. 2

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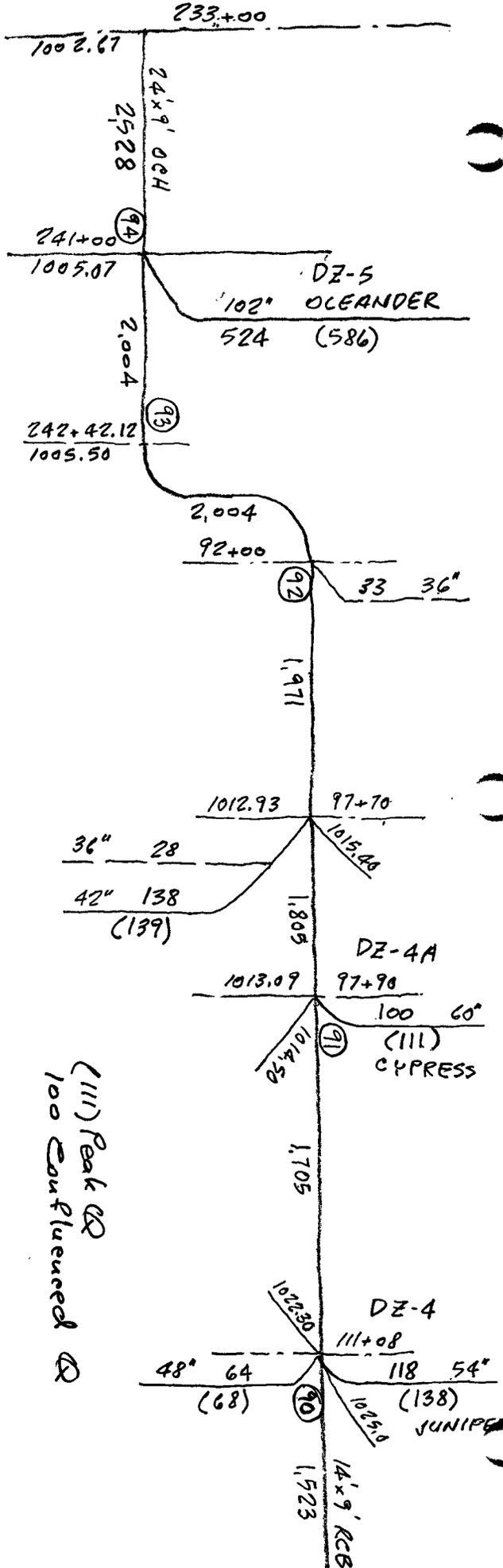
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25 YR  
AMC 2

JURUPA AVE  
JM04339  
FONTANA 10 (in sewer line)



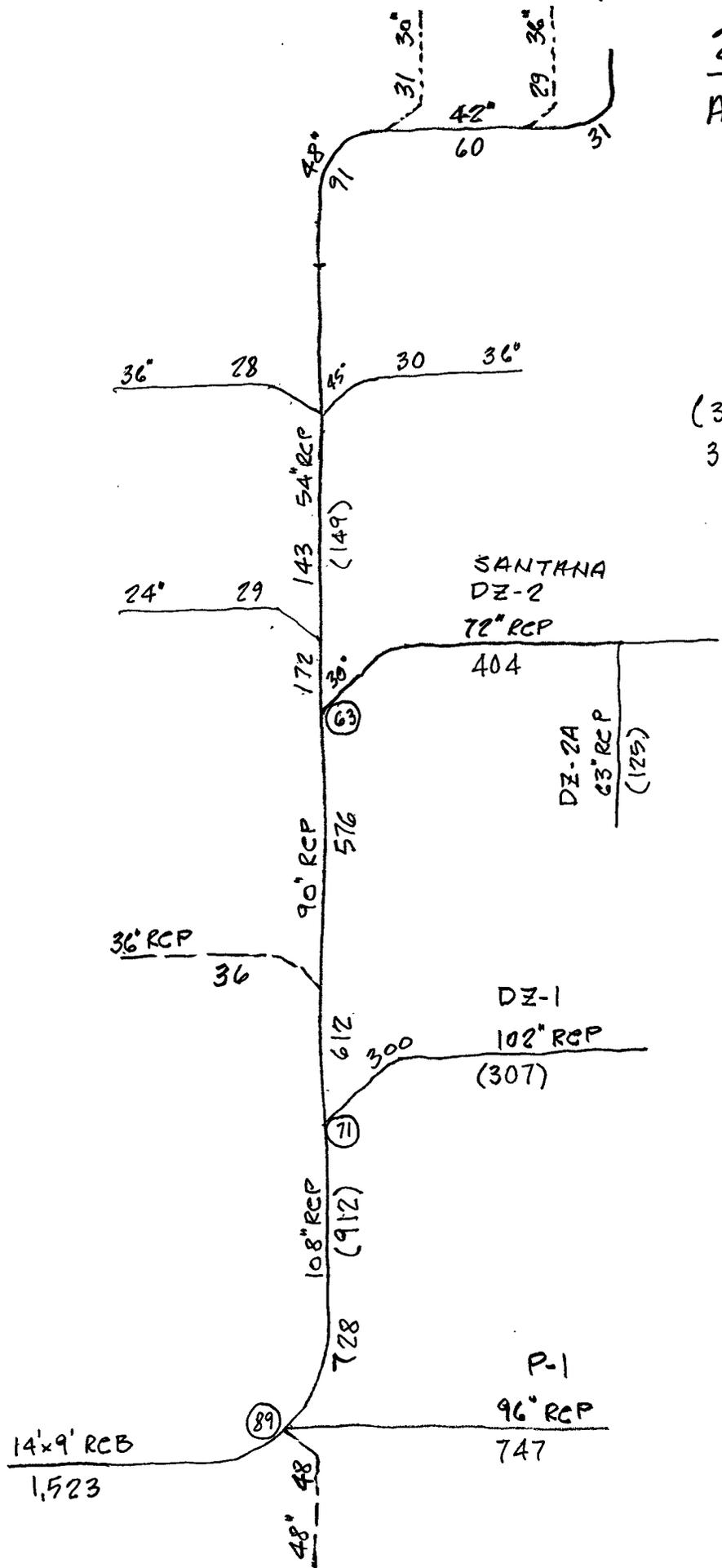
(III) Peak @  
100 Confluent @

SIERRA AVE. W/O DETENTION  
FONTANA 7 (in computer)

25 YR.  
AMC 2



(307) Peak Q  
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FONTANA

JOB No. 04339  
BY HERMAN  
DATE 8/2/04  
SHT. 149  
OF

◆ LAND PLANNING ◆ CIVIL ENGINEERING ◆ SURVEYING

**25 YEAR**

W/AMCZ

LINE "DZ-2A"

## San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
 Rational Hydrology Study Date: 01/13/05

-----  
 FONTANA / LINE DZ-2A HYDROLOGY  
 25 YEAR STORM  
 JN 04339

-----  
 Hall & Forman, Inc. - S/N 950  
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\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

-----  
 Rational hydrology study storm event year is 25.0  
 10 Year storm 1 hour rainfall = 0.930(In.)  
 100 Year storm 1 hour rainfall = 1.350(In.)  
 Computed rainfall intensity:  
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
 Slope used for rainfall intensity curve b = 0.6000  
 Soil antecedent moisture condition (AMC) = 2

-----  
 +-----+  
 Process from Point/Station 112.000 to Point/Station 113.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

SCHOOL subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.6000 Max loss rate(Fm)= 0.440(In/Hr)  
 Initial subarea data:  
 Top of initial area elevation = 1085.300(Ft.)  
 Bottom (of initial area) elevation = 1080.300(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00625 s(%)= 0.63  
 $TC = k(0.412)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 16.480 min.  
 Rainfall intensity = 2.382(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.734  
 Subarea runoff = 9.612(CFS)  
 Total initial stream area = 5.500(Ac.)  
 Pervious area fraction = 0.600  
 Initial area Fm value = 0.440(In/Hr)

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 +-----+  
 Process from Point/Station 113.000 to Point/Station 116.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

-----  
 Top of street segment elevation = 1080.300(Ft.)  
 End of street segment elevation = 1076.600(Ft.)  
 Length of street segment = 730.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 19.224(CFS)  
 Depth of flow = 0.492(Ft.), Average velocity = 2.391(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 19.873(Ft.)  
 Flow velocity = 2.39(Ft/s)  
 Travel time = 5.09 min. TC = 21.57 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.027(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.813  
 Subarea runoff = 17.582(CFS) for 11.000(Ac.)  
 Total runoff = 27.194(CFS)  
 Effective area this stream = 16.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 16.50(Ac.)  
 Area averaged Fm value = 0.196(In/Hr)  
 Street flow at end of street = 27.194(CFS)  
 Half street flow at end of street = 13.597(CFS)  
 Depth of flow = 0.540(Ft.), Average velocity = 2.737(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 116.000 to Point/Station 116.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 16.500(Ac.)  
 Runoff from this stream = 27.194(CFS)  
 Time of concentration = 21.57 min.  
 Rainfall intensity = 2.027(In/Hr)  
 Area averaged loss rate (Fm) = 0.1957(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.2667

++++++  
 Process from Point/Station 114.000 to Point/Station 115.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000      Max loss rate(Fm)=      0.073(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1093.600(Ft.)  
 Bottom (of initial area) elevation = 1084.400(Ft.)  
 Difference in elevation =      9.200(Ft.)  
 Slope =      0.00920    s(%)=      0.92  
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration =      12.306 min.  
 Rainfall intensity =      2.838(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.877  
 Subarea runoff =      13.687(CFS)  
 Total initial stream area =      5.500(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value =      0.073(In/Hr)

++++++  
 Process from Point/Station      115.000 to Point/Station      116.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

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Top of street segment elevation = 1084.400(Ft.)  
 End of street segment elevation = 1076.600(Ft.)  
 Length of street segment =      600.000(Ft.)  
 Height of curb above gutter flowline =      8.0(In.)  
 Width of half street (curb to crown) =      20.000(Ft.)  
 Distance from crown to crossfall grade break =      18.500(Ft.)  
 Slope from gutter to grade break (v/hz) =      0.020  
 Slope from grade break to crown (v/hz) =      0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line =      10.000(Ft.)  
 Slope from curb to property line (v/hz) =      0.020  
 Gutter width =      1.500(Ft.)  
 Gutter hike from flowline =      1.500(In.)  
 Manning's N in gutter =      0.0150  
 Manning's N from gutter to grade break =      0.0150  
 Manning's N from grade break to crown =      0.0150  
 Estimated mean flow rate at midpoint of street =      22.397(CFS)  
 Depth of flow =      0.447(Ft.), Average velocity =      3.539(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width =      17.587(Ft.)  
 Flow velocity =      3.54(Ft/s)  
 Travel time =      2.83 min.      TC =      15.13 min.

Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000      Max loss rate(Fm)=      0.073(In/Hr)  
 Rainfall intensity =      2.507(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.874  
 Subarea runoff =      13.695(CFS) for      7.000(Ac.)  
 Total runoff =      27.382(CFS)  
 Effective area this stream =      12.50(Ac.)

Total Study Area (Main Stream No. 1) = 29.00(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 27.382(CFS)  
 Half street flow at end of street = 13.691(CFS)  
 Depth of flow = 0.475(Ft.), Average velocity = 3.719(Ft/s)  
 Flow width (from curb towards crown)= 19.000(Ft.)

++++  
 Process from Point/Station 116.000 to Point/Station 116.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
 Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 12.500(Ac.)  
 Runoff from this stream = 27.382(CFS)  
 Time of concentration = 15.13 min.  
 Rainfall intensity = 2.507(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	27.194	21.57	2.027
2	27.382	15.13	2.507
Qmax(1) =	1.000 * 0.803 *	1.000 * 1.000 *	27.194) + 27.382) + = 49.172
Qmax(2) =	1.262 * 1.000 *	0.702 * 1.000 *	27.194) + 27.382) + = 51.465

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 27.194 27.382  
 Maximum flow rates at confluence using above data:  
 49.172 51.465  
 Area of streams before confluence:  
 16.500 12.500  
 Effective area values after confluence:  
 29.000 24.075  
 Results of confluence:  
 Total flow rate = 51.465(CFS)  
 Time of concentration = 15.132 min.  
 Effective stream area after confluence = 24.075(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.195  
 Stream Area average soil loss rate(Fm) = 0.143(In/Hr)  
 Study area (this main stream) = 29.00(Ac.)

++++  
 Process from Point/Station 116.000 to Point/Station 52.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

-----  
 Upstream point/station elevation = 1069.600(Ft.)  
 Downstream point/station elevation = 1061.900(Ft.)  
 Pipe length = 650.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 51.465(CFS)  
 Given pipe size = 39.00(In.)

Calculated individual pipe flow = 51.465(CFS)  
 Normal flow depth in pipe = 21.16(In.)  
 Flow top width inside pipe = 38.86(In.)  
 Critical Depth = 27.48(In.)  
 Pipe flow velocity = 11.20(Ft/s)  
 Travel time through pipe = 0.97 min.  
 Time of concentration (TC) = 16.10 min.

++++  
 Process from Point/Station 52.000 to Point/Station 52.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
 Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 24.075(Ac.)  
 Runoff from this stream = 51.465(CFS)  
 Time of concentration = 16.10 min.  
 Rainfall intensity = 2.416(In/Hr)  
 Area averaged loss rate (Fm) = 0.1430(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1948

++++  
 Process from Point/Station 117.000 to Point/Station 118.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

-----  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1076.000(Ft.)  
 Bottom (of initial area) elevation = 1071.000(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%)= 0.50  
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.902 min.  
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875  
 Subarea runoff = 11.541(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073(In/Hr)

++++  
 Process from Point/Station 118.000 to Point/Station 119.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

-----  
 Top of street segment elevation = 1071.000(Ft.)  
 End of street segment elevation = 1068.900(Ft.)  
 Length of street segment = 420.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020

Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 23.083(CFS)  
 Depth of flow = 0.517(Ft.), Average velocity = 2.554(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 2.55(Ft/s)  
 Travel time = 2.74 min. TC = 16.64 min.

Adding area flow to street

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.368(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.872  
 Subarea runoff = 19.438(CFS) for 10.000(Ac.)  
 Total runoff = 30.980(CFS)  
 Effective area this stream = 15.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 44.00(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 30.980(CFS)  
 Half street flow at end of street = 15.490(CFS)  
 Depth of flow = 0.561(Ft.), Average velocity = 2.871(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++  
 Process from Point/Station 119.000 to Point/Station 119.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 15.000(Ac.)  
 Runoff from this stream = 30.980(CFS)  
 Time of concentration = 16.64 min.  
 Rainfall intensity = 2.368(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	51.465	16.10	2.416
2	30.980	16.64	2.368
Qmax(1) =	1.000 *	1.000 *	51.465) +
	1.021 *	0.967 *	30.980) + = 82.054
Qmax(2) =			

0.979 *	1.000 *	51.465) +	
1.000 *	1.000 *	30.980) + =	81.364

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
     51.465          30.980  
 Maximum flow rates at confluence using above data:  
     82.054          81.364  
 Area of streams before confluence:  
     24.075          15.000  
 Effective area values after confluence:  
     38.585          39.075

Results of confluence:  
 Total flow rate = 82.054(CFS)  
 Time of concentration = 16.099 min.  
 Effective stream area after confluence = 38.585 (Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.158  
 Stream Area average soil loss rate(Fm) = 0.116(In/Hr)  
 Study area (this main stream) = 39.08 (Ac.)

++++  
 Process from Point/Station 52.000 to Point/Station 53.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

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Upstream point/station elevation = 1061.900(Ft.)  
 Downstream point/station elevation = 1059.400(Ft.)  
 Pipe length = 500.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 82.054(CFS)  
 Given pipe size = 42.00(In.)  
 NOTE: Normal flow is pressure flow in user selected pipe size.  
 The approximate hydraulic grade line above the pipe invert is  
     2.519(Ft.) at the headworks or inlet of the pipe(s)  
     Pipe friction loss = 3.325(Ft.)  
     Minor friction loss = 1.694(Ft.) K-factor = 1.50  
     Pipe flow velocity = 8.53(Ft/s)  
     Travel time through pipe = 0.98 min.  
     Time of concentration (TC) = 17.08 min.

++++  
 Process from Point/Station 53.000 to Point/Station 53.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

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Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 38.585(Ac.)  
 Runoff from this stream = 82.054(CFS)  
 Time of concentration = 17.08 min.  
 Rainfall intensity = 2.332(In/Hr)  
 Area averaged loss rate (Fm) = 0.1163(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1584

++++  
 Process from Point/Station 120.000 to Point/Station 121.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

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COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000      Max loss rate(Fm)=      0.073(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1072.000(Ft.)  
 Bottom (of initial area) elevation = 1067.000(Ft.)  
 Difference in elevation =      5.000(Ft.)  
 Slope =      0.00500    s(%)=      0.50  
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration =    13.902 min.  
 Rainfall intensity =      2.638(In/Hr) for a    25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875  
 Subarea runoff =      12.696(CFS)  
 Total initial stream area =      5.500(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value =      0.073(In/Hr)

++++++  
 Process from Point/Station      121.000 to Point/Station      122.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

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Top of street segment elevation = 1067.000(Ft.)  
 End of street segment elevation = 1064.700(Ft.)  
 Length of street segment =    450.000(Ft.)  
 Height of curb above gutter flowline =    8.0(In.)  
 Width of half street (curb to crown) =    20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) =    0.020  
 Slope from grade break to crown (v/hz) =    0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) =    0.020  
 Gutter width =    1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
   Manning's N in gutter = 0.0150  
   Manning's N from gutter to grade break = 0.0150  
   Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street =    23.083(CFS)  
 Depth of flow = 0.516(Ft.), Average velocity = 2.571(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 2.57(Ft/s)  
 Travel time =    2.92 min.      TC =    16.82 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000      Max loss rate(Fm)=      0.073(In/Hr)  
 Rainfall intensity =      2.353(In/Hr) for a    25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.872  
 Subarea runoff =      17.056(CFS) for      9.000(Ac.)  
 Total runoff =      29.752(CFS)  
 Effective area this stream =      14.50(Ac.)  
 Total Study Area (Main Stream No. 1) =      58.50(Ac.)

Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 29.752(CFS)  
 Half street flow at end of street = 14.876(CFS)  
 Depth of flow = 0.553(Ft.), Average velocity = 2.844(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

\*\*\*\*\*  
 Process from Point/Station 122.000 to Point/Station 122.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
 Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 14.500(Ac.)  
 Runoff from this stream = 29.752(CFS)  
 Time of concentration = 16.82 min.  
 Rainfall intensity = 2.353(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	82.054	17.08	2.332
2	29.752	16.82	2.353
Qmax(1) =			
	1.000 *	1.000 *	82.054) +
	0.991 *	1.000 *	29.752) + = 111.529
Qmax(2) =			
	1.010 *	0.985 *	82.054) +
	1.000 *	1.000 *	29.752) + = 111.350

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 82.054      29.752  
 Maximum flow rates at confluence using above data:  
 111.529      111.350  
 Area of streams before confluence:  
 38.585      14.500  
 Effective area values after confluence:  
 53.085      52.505  
 Results of confluence:  
 Total flow rate = 111.529(CFS)  
 Time of concentration = 17.076 min.  
 Effective stream area after confluence = 53.085(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.142  
 Stream Area average soil loss rate(Fm) = 0.105(In/Hr)  
 Study area (this main stream) = 53.08(Ac.)

\*\*\*\*\*  
 Process from Point/Station 53.000 to Point/Station 54.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

-----  
 Upstream point/station elevation = 1052.500(Ft.)  
 Downstream point/station elevation = 1048.200(Ft.)  
 Pipe length = 860.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 111.529(CFS)  
 Given pipe size = 60.00(In.)

Calculated individual pipe flow = 111.529(CFS)  
 Normal flow depth in pipe = 33.70(In.)  
 Flow top width inside pipe = 59.54(In.)  
 Critical Depth = 36.14(In.)  
 Pipe flow velocity = 9.83(Ft/s)  
 Travel time through pipe = 1.46 min.  
 Time of concentration (TC) = 18.53 min.

++++++  
 Process from Point/Station 54.000 to Point/Station 54.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 53.085(Ac.)  
 Runoff from this stream = 111.529(CFS)  
 Time of concentration = 18.53 min.  
 Rainfall intensity = 2.220(In/Hr)  
 Area averaged loss rate (Fm) = 0.1046(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1425

++++++  
 Process from Point/Station 123.000 to Point/Station 124.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1064.700(Ft.)  
 Bottom (of initial area) elevation = 1059.700(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%)= 0.50  
 $TC = k(0.304) * [(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.902 min.  
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875  
 Subarea runoff = 16.158(CFS)  
 Total initial stream area = 7.000(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073(In/Hr)

++++++  
 Process from Point/Station 124.000 to Point/Station 124.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 7.000(Ac.)  
 Runoff from this stream = 16.158(CFS)  
 Time of concentration = 13.90 min.  
 Rainfall intensity = 2.638(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	111.529	18.53	2.220
2	16.158	13.90	2.638
Qmax(1) =			
	1.000 *	1.000 *	111.529) +
	0.837 *	1.000 *	16.158) + = 125.052
Qmax(2) =			
	1.198 *	0.750 *	111.529) +
	1.000 *	1.000 *	16.158) + = 116.346

Total of 2 streams to confluence:

Flow rates before confluence point:

111.529      16.158

Maximum flow rates at confluence using above data:

125.052      116.346

Area of streams before confluence:

53.085      7.000

Effective area values after confluence:

60.085      46.817

Results of confluence:

Total flow rate = 125.052(CFS)

Time of concentration = 18.535 min.

Effective stream area after confluence = 60.085 (Ac.)

Stream Area average Pervious fraction(Ap) = 0.138

Stream Area average soil loss rate(Fm) = 0.101(In/Hr)

Study area (this main stream) = 60.08 (Ac.)

+++++  
 Process from Point/Station      54.000 to Point/Station      55.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1048.200(Ft.)

Downstream point/station elevation = 1046.500(Ft.)

Pipe length = 340.00(Ft.)      Manning's N = 0.013

No. of pipes = 1      Required pipe flow = 125.052(CFS)

Given pipe size = 63.00(In.)

Calculated individual pipe flow = 125.052(CFS)

Normal flow depth in pipe = 35.02(In.)

Flow top width inside pipe = 62.61(In.)

Critical Depth = 37.85(In.)

Pipe flow velocity = 10.11(Ft/s)

Travel time through pipe = 0.56 min.

Time of concentration (TC) = 19.10 min.

End of computations, Total Study Area = 65.50 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area

effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.142

Area averaged SCS curve number = 56.0

LINE "DZ-2"

## San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
 Rational Hydrology Study Date: 01/13/05

FONTANA / LINE DZ-2 HYDROLOGY  
 25 YEAR STORM  
 JN 04339

Hall & Forman, Inc. - S/N 950

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

Rational hydrology study storm event year is 25.0  
 10 Year storm 1 hour rainfall = 0.930(In.)  
 100 Year storm 1 hour rainfall = 1.350(In.)  
 Computed rainfall intensity:  
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
 Slope used for rainfall intensity curve b = 0.6000  
 Soil antecedent moisture condition (AMC) = 2

\*\*\*\*\*  
 Process from Point/Station 100.000 to Point/Station 101.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

COMMERCIAL subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.098 (In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 960.000(Ft.)  
 Top (of initial area) elevation = 1103.000(Ft.)  
 Bottom (of initial area) elevation = 1098.400(Ft.)  
 Difference in elevation = 4.600(Ft.)  
 Slope = 0.00479 s(%) = 0.48  
 $TC = k(0.304) * [(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.794 min.  
 Rainfall intensity = 2.651(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.867  
 Subarea runoff = 11.488(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.098(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 101.000 to Point/Station 102.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1098.400(Ft.)  
 End of street segment elevation = 1093.600(Ft.)  
 Length of street segment = 590.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 17.231(CFS)  
 Depth of flow = 0.443(Ft.), Average velocity = 2.781(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 17.399(Ft.)  
 Flow velocity = 2.78(Ft/s)  
 Travel time = 3.54 min. TC = 17.33 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.311(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.867  
 Subarea runoff = 8.544(CFS) for 5.000(Ac.)  
 Total runoff = 20.032(CFS)  
 Effective area this stream = 10.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 10.00(Ac.)  
 Area averaged Fm value = 0.086(In/Hr)  
 Street flow at end of street = 20.032(CFS)  
 Half street flow at end of street = 10.016(CFS)  
 Depth of flow = 0.464(Ft.), Average velocity = 2.886(Ft/s)  
 Flow width (from curb towards crown)= 18.438(Ft.)

++++++  
 Process from Point/Station 102.000 to Point/Station 50.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1085.300(Ft.)  
 Downstream point/station elevation = 1079.500(Ft.)  
 Pipe length = 460.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 20.032(CFS)  
 Given pipe size = 24.00(In.)  
 Calculated individual pipe flow = 20.032(CFS)  
 Normal flow depth in pipe = 16.08(In.)  
 Flow top width inside pipe = 22.57(In.)  
 Critical Depth = 19.29(In.)  
 Pipe flow velocity = 8.96(Ft/s)  
 Travel time through pipe = 0.86 min.  
 Time of concentration (TC) = 18.19 min.

++++++  
 Process from Point/Station 50.000 to Point/Station 50.000

\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 10.000(Ac.)  
 Runoff from this stream = 20.032(CFS)  
 Time of concentration = 18.19 min.  
 Rainfall intensity = 2.245(In/Hr)  
 Area averaged loss rate (Fm) = 0.0856(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000

++++  
 Process from Point/Station 103.000 to Point/Station 104.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

COMMERCIAL subarea type

Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1103.000(Ft.)  
 Bottom (of initial area) elevation = 1098.400(Ft.)  
 Difference in elevation = 4.600(Ft.)  
 Slope = 0.00460 s(%) = 0.46  
 $TC = k(0.304) * [(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 14.136 min.  
 Rainfall intensity = 2.612(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.866  
 Subarea runoff = 12.445(CFS)  
 Total initial stream area = 5.500(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.098(In/Hr)

++++  
 Process from Point/Station 104.000 to Point/Station 105.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1098.400(Ft.)  
 End of street segment elevation = 1092.200(Ft.)  
 Length of street segment = 700.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 23.193(CFS)  
 Depth of flow = 0.479(Ft.), Average velocity = 3.090(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:

Halfstreet flow width = 19.189(Ft.)  
 Flow velocity = 3.09(Ft/s)  
 Travel time = 3.78 min. TC = 17.91 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)  
 Rainfall intensity = 2.266(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.861  
 Subarea runoff = 16.826(CFS) for 9.500(Ac.)  
 Total runoff = 29.271(CFS)  
 Effective area this stream = 15.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 25.00(Ac.)  
 Area averaged Fm value = 0.098(In/Hr)  
 Street flow at end of street = 29.271(CFS)  
 Half street flow at end of street = 14.636(CFS)  
 Depth of flow = 0.511(Ft.), Average velocity = 3.335(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

\*\*\*\*\*  
 Process from Point/Station 105.000 to Point/Station 50.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1083.800(Ft.)  
 Downstream point/station elevation = 1079.500(Ft.)  
 Pipe length = 570.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 29.271(CFS)  
 Given pipe size = 30.00(In.)  
 Calculated individual pipe flow = 29.271(CFS)  
 Normal flow depth in pipe = 20.70(In.)  
 Flow top width inside pipe = 27.75(In.)  
 Critical Depth = 22.15(In.)  
 Pipe flow velocity = 8.10(Ft/s)  
 Travel time through pipe = 1.17 min.  
 Time of concentration (TC) = 19.08 min.

\*\*\*\*\*  
 Process from Point/Station 50.000 to Point/Station 50.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 15.000(Ac.)  
 Runoff from this stream = 29.271(CFS)  
 Time of concentration = 19.08 min.  
 Rainfall intensity = 2.181(In/Hr)  
 Area averaged loss rate (Fm) = 0.0978(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
------------	-----------------	----------	----------------------------

1	20.032	18.19	2.245	
2	29.271	19.08	2.181	
Qmax(1) =				
	1.000 *	1.000 *	20.032) +	
	1.031 *	0.953 *	29.271) + =	48.782
Qmax(2) =				
	0.970 *	1.000 *	20.032) +	
	1.000 *	1.000 *	29.271) + =	48.709

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
     20.032          29.271  
 Maximum flow rates at confluence using above data:  
     48.782          48.709  
 Area of streams before confluence:  
     10.000          15.000  
 Effective area values after confluence:  
     24.293          25.000  
 Results of confluence:  
 Total flow rate = 48.782(CFS)  
 Time of concentration = 18.186 min.  
 Effective stream area after confluence = 24.293(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.100  
 Stream Area average soil loss rate(Fm) = 0.093(In/Hr)  
 Study area (this main stream) = 25.00(Ac.)

\*\*\*\*\*  
 Process from Point/Station          50.000 to Point/Station          51.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1079.500(Ft.)  
 Downstream point/station elevation = 1071.300(Ft.)  
 Pipe length = 1320.00(Ft.)      Manning's N = 0.013  
 No. of pipes = 1      Required pipe flow = 48.782(CFS)  
 Given pipe size = 39.00(In.)  
 Calculated individual pipe flow = 48.782(CFS)  
 Normal flow depth in pipe = 25.20(In.)  
 Flow top width inside pipe = 37.30(In.)  
 Critical Depth = 26.75(In.)  
 Pipe flow velocity = 8.61(Ft/s)  
 Travel time through pipe = 2.56 min.  
 Time of concentration (TC) = 20.74 min.

\*\*\*\*\*  
 Process from Point/Station          51.000 to Point/Station          51.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 24.293(Ac.)  
 Runoff from this stream = 48.782(CFS)  
 Time of concentration = 20.74 min.  
 Rainfall intensity = 2.075(In/Hr)  
 Area averaged loss rate (Fm) = 0.0929(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000

\*\*\*\*\*  
 Process from Point/Station          106.000 to Point/Station          107.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

 COMMERCIAL subarea type

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000      Max loss rate(Fm)=      0.073(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1093.600(Ft.)  
 Bottom (of initial area) elevation = 1085.400(Ft.)  
 Difference in elevation =      8.200(Ft.)  
 Slope =      0.00820    s(%)=      0.82  
 $TC = k(0.304) * [(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 12.592 min.  
 Rainfall intensity =      2.800(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.876  
 Subarea runoff =      13.494(CFS)  
 Total initial stream area =      5.500(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value =      0.073(In/Hr)

++++++  
 Process from Point/Station      107.000 to Point/Station      108.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1085.400(Ft.)  
 End of street segment elevation = 1078.300(Ft.)  
 Length of street segment = 700.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street =      20.855(CFS)  
 Depth of flow = 0.454(Ft.), Average velocity =      3.167(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 17.948(Ft.)  
 Flow velocity = 3.17(Ft/s)  
 Travel time = 3.68 min.      TC = 16.28 min.  
 Adding area flow to street

## COMMERCIAL subarea type

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000      Max loss rate(Fm)=      0.073(In/Hr)  
 Rainfall intensity =      2.400(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.872

Subarea runoff = 10.586(CFS) for 6.000(Ac.)  
 Total runoff = 24.081(CFS)  
 Effective area this stream = 11.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 36.50(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 24.081(CFS)  
 Half street flow at end of street = 12.040(CFS)  
 Depth of flow = 0.474(Ft.), Average velocity = 3.282(Ft/s)  
 Flow width (from curb towards crown)= 18.968(Ft.)

++++  
 Process from Point/Station 108.000 to Point/Station 108.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
 Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 11.500(Ac.)  
 Runoff from this stream = 24.081(CFS)  
 Time of concentration = 16.28 min.  
 Rainfall intensity = 2.400(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	48.782	20.74	2.075
2	24.081	16.28	2.400
Qmax(1) =	1.000 * 0.860 *	1.000 * 1.000 *	48.782) + 24.081) + = 69.500
Qmax(2) =	1.164 * 1.000 *	0.785 * 1.000 *	48.782) + 24.081) + = 68.635

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 48.782      24.081  
 Maximum flow rates at confluence using above data:  
 69.500      68.635  
 Area of streams before confluence:  
 24.293      11.500  
 Effective area values after confluence:  
 35.793      30.564  
 Results of confluence:  
 Total flow rate = 69.500(CFS)  
 Time of concentration = 20.741 min.  
 Effective stream area after confluence = 35.793(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.100  
 Stream Area average soil loss rate(Fm) = 0.087(In/Hr)  
 Study area (this main stream) = 35.79(Ac.)

++++  
 Process from Point/Station 51.000 to Point/Station 55.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

-----  
 Upstream point/station elevation = 1071.300(Ft.)  
 Downstream point/station elevation = 1062.400(Ft.)

Pipe length = 900.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 69.500(CFS)  
 Given pipe size = 42.00(In.)  
 Calculated individual pipe flow = 69.500(CFS)  
 Normal flow depth in pipe = 25.76(In.)  
 Flow top width inside pipe = 40.91(In.)  
 Critical Depth = 31.34(In.)  
 Pipe flow velocity = 11.23(Ft/s)  
 Travel time through pipe = 1.34 min.  
 Time of concentration (TC) = 22.08 min.

++++++  
 Process from Point/Station 55.000 to Point/Station 55.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 35.793(Ac.)  
 Runoff from this stream = 69.500(CFS)  
 Time of concentration = 22.08 min.  
 Rainfall intensity = 1.999(In/Hr)  
 Area averaged loss rate (Fm) = 0.0866(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000

++++++  
 Process from Point/Station 109.000 to Point/Station 110.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1080.000(Ft.)  
 Bottom (of initial area) elevation = 1073.700(Ft.)  
 Difference in elevation = 6.300(Ft.)  
 Slope = 0.00630 s(%)= 0.63  
 $TC = k(0.304) * [(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.274 min.  
 Rainfall intensity = 2.712(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.876  
 Subarea runoff = 10.688(CFS)  
 Total initial stream area = 4.500(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073(In/Hr)

++++++  
 Process from Point/Station 110.000 to Point/Station 111.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1073.700(Ft.)  
 End of street segment elevation = 1069.400(Ft.)  
 Length of street segment = 350.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)

Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 15.438(CFS)  
 Depth of flow = 0.403(Ft.), Average velocity = 3.161(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 15.396(Ft.)  
 Flow velocity = 3.16(Ft/s)  
 Travel time = 1.85 min. TC = 15.12 min.

Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.509(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.874  
 Subarea runoff = 7.941(CFS) for 4.000(Ac.)  
 Total runoff = 18.629(CFS)  
 Effective area this stream = 8.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 45.00(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 18.629(CFS)  
 Half street flow at end of street = 9.315(CFS)  
 Depth of flow = 0.426(Ft.), Average velocity = 3.311(Ft/s)  
 Flow width (from curb towards crown)= 16.560(Ft.)

\*\*\*\*\*  
 Process from Point/Station 111.000 to Point/Station 111.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 8.500(Ac.)  
 Runoff from this stream = 18.629(CFS)  
 Time of concentration = 15.12 min.  
 Rainfall intensity = 2.509(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000

\*\*\*\*\*  
 Process from Point/Station 125.000 to Point/Station 126.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1093.200(Ft.)  
 Bottom (of initial area) elevation = 1085.300(Ft.)  
 Difference in elevation = 7.900(Ft.)  
 Slope = 0.00790 s(%)= 0.79  
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 12.687 min.  
 Rainfall intensity = 2.787(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.876  
 Subarea runoff = 13.433(CFS)  
 Total initial stream area = 5.500(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 126.000 to Point/Station 127.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1085.300(Ft.)  
 End of street segment elevation = 1076.300(Ft.)  
 Length of street segment = 900.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 28.086(CFS)  
 Depth of flow = 0.498(Ft.), Average velocity = 3.402(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 3.40(Ft/s)  
 Travel time = 4.41 min. TC = 17.10 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.330(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.872  
 Subarea runoff = 22.115(CFS) for 12.000(Ac.)  
 Total runoff = 35.547(CFS)  
 Effective area this stream = 17.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 62.50(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)

Street flow at end of street = 35.547(CFS)  
 Half street flow at end of street = 17.774(CFS)  
 Depth of flow = 0.529(Ft.), Average velocity = 3.736(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

\*\*\*\*\*  
 Process from Point/Station 127.000 to Point/Station 55.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1069.300(Ft.)  
 Downstream point/station elevation = 1046.500(Ft.)  
 Pipe length = 1000.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 35.547(CFS)  
 Given pipe size = 30.00(In.)  
 Calculated individual pipe flow = 35.547(CFS)  
 Normal flow depth in pipe = 16.29(In.)  
 Flow top width inside pipe = 29.89(In.)  
 Critical Depth = 24.28(In.)  
 Pipe flow velocity = 13.05(Ft/s)  
 Travel time through pipe = 1.28 min.  
 Time of concentration (TC) = 18.37 min.

\*\*\*\*\*  
 Process from Point/Station 55.000 to Point/Station 55.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 17.500(Ac.)  
 Runoff from this stream = 35.547(CFS)  
 Time of concentration = 18.37 min.  
 Rainfall intensity = 2.232(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000

\*\*\*\*\*  
 Process from Point/Station 128.000 to Point/Station 129.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1078.300(Ft.)  
 Bottom (of initial area) elevation = 1069.400(Ft.)  
 Difference in elevation = 8.900(Ft.)  
 Slope = 0.00890 s(%)= 0.89  
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 12.388 min.  
 Rainfall intensity = 2.827(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.877  
 Subarea runoff = 22.306(CFS)  
 Total initial stream area = 9.000(Ac.)

Pervious area fraction = 0.100  
 Initial area Fm value = 0.073(In/Hr)

Process from Point/Station 129.000 to Point/Station 129.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 4  
 Stream flow area = 9.000(Ac.)  
 Runoff from this stream = 22.306(CFS)  
 Time of concentration = 12.39 min.  
 Rainfall intensity = 2.827(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000

Process from Point/Station 55.000 to Point/Station 55.000  
 \*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

Soil classification AP and SCS values input by user  
 USER INPUT of soil data for subarea  
 SCS curve number for soil(AMC 2) = 56.16  
 Pervious ratio(Ap) = 0.1380 Max loss rate(Fm)= 0.101(In/Hr)  
 Rainfall intensity = 2.220(In/Hr) for a 25.0 year storm  
 User specified values are as follows:  
 TC = 18.54 min. Rain intensity = 2.22(In/Hr)  
 Total area this stream = 60.09(Ac.)  
 Total Study Area (Main Stream No. 1) = 131.59(Ac.)  
 Total runoff = 125.05(CFS)

Process from Point/Station 55.000 to Point/Station 55.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 5  
 Stream flow area = 60.090(Ac.)  
 Runoff from this stream = 125.050(CFS)  
 Time of concentration = 18.54 min.  
 Rainfall intensity = 2.220(In/Hr)  
 Area averaged loss rate (Fm) = 0.1010(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1380  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	69.500	22.08	1.999
2	18.629	15.12	2.509
3	35.547	18.37	2.232
4	22.306	12.39	2.827
5	125.050	18.54	2.220
Qmax(1) =			
	1.000 *	1.000 *	69.500) +
	0.791 *	1.000 *	18.629) +
	0.892 *	1.000 *	35.547) +
	0.699 *	1.000 *	22.306) +
	0.896 *	1.000 *	125.050) + = 243.559

$Q_{max}(2) =$   
 1.267 \* 0.685 \* 69.500) +  
 1.000 \* 1.000 \* 18.629) +  
 1.128 \* 0.823 \* 35.547) +  
 0.884 \* 1.000 \* 22.306) +  
 1.136 \* 0.816 \* 125.050) + = 247.530  
 $Q_{max}(3) =$   
 1.122 \* 0.832 \* 69.500) +  
 0.886 \* 1.000 \* 18.629) +  
 1.000 \* 1.000 \* 35.547) +  
 0.784 \* 1.000 \* 22.306) +  
 1.006 \* 0.991 \* 125.050) + = 259.054  
 $Q_{max}(4) =$   
 1.433 \* 0.561 \* 69.500) +  
 1.131 \* 0.819 \* 18.629) +  
 1.276 \* 0.674 \* 35.547) +  
 1.000 \* 1.000 \* 22.306) +  
 1.287 \* 0.668 \* 125.050) + = 233.550  
 $Q_{max}(5) =$   
 1.115 \* 0.840 \* 69.500) +  
 0.881 \* 1.000 \* 18.629) +  
 0.994 \* 1.000 \* 35.547) +  
 0.779 \* 1.000 \* 22.306) +  
 1.000 \* 1.000 \* 125.050) + = 259.305

Total of 5 streams to confluence:  
 Flow rates before confluence point:  
 69.500 18.629 35.547 22.306 125.050  
 Maximum flow rates at confluence using above data:  
 243.559 247.530 259.054 233.550 259.305  
 Area of streams before confluence:  
 35.793 8.500 17.500 9.000 60.090  
 Effective area values after confluence:  
 130.883 105.418 124.336 87.999 125.149  
 Results of confluence:  
 Total flow rate = 259.305(CFS)  
 Time of concentration = 18.540 min.  
 Effective stream area after confluence = 125.149(Ac.)  
 Stream Area average Pervious fraction( $A_p$ ) = 0.117  
 Stream Area average soil loss rate( $F_m$ ) = 0.090(In/Hr)  
 Study area (this main stream) = 130.88(Ac.)

++++++  
 Process from Point/Station 55.000 to Point/Station 56.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1046.500(Ft.)  
 Downstream point/station elevation = 1043.300(Ft.)  
 Pipe length = 1000.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 259.305(CFS)  
 Given pipe size = 81.00(In.)  
 Calculated individual pipe flow = 259.305(CFS)  
 Normal flow depth in pipe = 54.33(In.)  
 Flow top width inside pipe = 76.13(In.)  
 Critical Depth = 51.19(In.)  
 Pipe flow velocity = 10.16(Ft/s)  
 Travel time through pipe = 1.64 min.  
 Time of concentration (TC) = 20.18 min.

+++++  
 Process from Point/Station 56.000 to Point/Station 56.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
 Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 125.149(Ac.)  
 Runoff from this stream = 259.305(CFS)  
 Time of concentration = 20.18 min.  
 Rainfall intensity = 2.110(In/Hr)  
 Area averaged loss rate (Fm) = 0.0897(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1174

+++++  
 Process from Point/Station 130.000 to Point/Station 131.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

-----  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1092.200(Ft.)  
 Bottom (of initial area) elevation = 1084.100(Ft.)  
 Difference in elevation = 8.100(Ft.)  
 Slope = 0.00810 s(%)= 0.81  
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 12.623 min.  
 Rainfall intensity = 2.795(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.876  
 Subarea runoff = 13.474(CFS)  
 Total initial stream area = 5.500(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073(In/Hr)

+++++  
 Process from Point/Station 131.000 to Point/Station 132.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

-----  
 Top of street segment elevation = 1084.100(Ft.)  
 End of street segment elevation = 1075.000(Ft.)  
 Length of street segment = 900.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 28.173(CFS)

Depth of flow = 0.498(Ft.), Average velocity = 3.418(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 3.42(Ft/s)  
 Travel time = 4.39 min. TC = 17.01 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.337(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.872  
 Subarea runoff = 22.181(CFS) for 12.000(Ac.)  
 Total runoff = 35.655(CFS)  
 Effective area this stream = 17.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 149.09(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 35.655(CFS)  
 Half street flow at end of street = 17.827(CFS)  
 Depth of flow = 0.529(Ft.), Average velocity = 3.753(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 132.000 to Point/Station 56.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1068.000(Ft.)  
 Downstream point/station elevation = 1043.300(Ft.)  
 Pipe length = 1100.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 35.655(CFS)  
 Given pipe size = 30.00(In.)  
 Calculated individual pipe flow = 35.655(CFS)  
 Normal flow depth in pipe = 16.41(In.)  
 Flow top width inside pipe = 29.87(In.)  
 Critical Depth = 24.30(In.)  
 Pipe flow velocity = 12.99(Ft/s)  
 Travel time through pipe = 1.41 min.  
 Time of concentration (TC) = 18.42 min.

++++++  
 Process from Point/Station 56.000 to Point/Station 56.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 17.500(Ac.)  
 Runoff from this stream = 35.655(CFS)  
 Time of concentration = 18.42 min.  
 Rainfall intensity = 2.228(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000

+++++

Process from Point/Station 133.000 to Point/Station 134.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1076.300(Ft.)  
 Bottom (of initial area) elevation = 1070.900(Ft.)  
 Difference in elevation = 5.400(Ft.)  
 Slope = 0.00540 s(%) = 0.54  
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.690 min.  
 Rainfall intensity = 2.663(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875  
 Subarea runoff = 12.817(CFS)  
 Total initial stream area = 5.500(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073(In/Hr)

+++++  
 Process from Point/Station 134.000 to Point/Station 135.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1070.900(Ft.)  
 End of street segment elevation = 1064.100(Ft.)  
 Length of street segment = 800.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 38.450(CFS)  
 Depth of flow = 0.553(Ft.), Average velocity = 3.670(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 3.67(Ft/s)  
 Travel time = 3.63 min. TC = 17.32 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)

Rainfall intensity = 2.312(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.871  
 Subarea runoff = 42.588(CFS) for 22.000(Ac.)  
 Total runoff = 55.405(CFS)  
 Effective area this stream = 27.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 176.59(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 55.405(CFS)  
 Half street flow at end of street = 27.703(CFS)  
 Depth of flow = 0.618(Ft.), Average velocity = 4.242(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 135.000 to Point/Station 135.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 27.500(Ac.)  
 Runoff from this stream = 55.405(CFS)  
 Time of concentration = 17.32 min.  
 Rainfall intensity = 2.312(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	259.305	20.18	2.110
2	35.655	18.42	2.228
3	55.405	17.32	2.312
Qmax(1) =			
	1.000 *	1.000 *	259.305) +
	0.945 *	1.000 *	35.655) +
	0.910 *	1.000 *	55.405) + = 343.395
Qmax(2) =			
	1.059 *	0.913 *	259.305) +
	1.000 *	1.000 *	35.655) +
	0.962 *	1.000 *	55.405) + = 339.603
Qmax(3) =			
	1.100 *	0.858 *	259.305) +
	1.039 *	0.940 *	35.655) +
	1.000 *	1.000 *	55.405) + = 335.124

Total of 3 streams to confluence:  
 Flow rates before confluence point:  
 259.305      35.655      55.405  
 Maximum flow rates at confluence using above data:  
 343.395      339.603      335.124  
 Area of streams before confluence:  
 125.149      17.500      27.500  
 Effective area values after confluence:  
 170.149      159.257      151.380  
 Results of confluence:  
 Total flow rate = 343.395(CFS)  
 Time of concentration = 20.180 min.  
 Effective stream area after confluence = 170.149(Ac.)

Stream Area average Pervious fraction(Ap) = 0.113  
 Stream Area average soil loss rate(Fm) = 0.085(In/Hr)  
 Study area (this main stream) = 170.15(Ac.)

+++++  
 Process from Point/Station 56.000 to Point/Station 57.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1043.300(Ft.)  
 Downstream point/station elevation = 1041.300(Ft.)  
 Pipe length = 640.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 343.395(CFS)  
 Given pipe size = 84.00(In.)  
 Calculated individual pipe flow = 343.395(CFS)  
 Normal flow depth in pipe = 66.09(In.)  
 Flow top width inside pipe = 68.80(In.)  
 Critical Depth = 58.60(In.)  
 Pipe flow velocity = 10.57(Ft/s)  
 Travel time through pipe = 1.01 min.  
 Time of concentration (TC) = 21.19 min.

+++++  
 Process from Point/Station 57.000 to Point/Station 57.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 170.149(Ac.)  
 Runoff from this stream = 343.395(CFS)  
 Time of concentration = 21.19 min.  
 Rainfall intensity = 2.049(In/Hr)  
 Area averaged loss rate (Fm) = 0.0854(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1128

+++++  
 Process from Point/Station 136.000 to Point/Station 137.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1091.600(Ft.)  
 Bottom (of initial area) elevation = 1086.600(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%)= 0.50  
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.902 min.  
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875  
 Subarea runoff = 12.696(CFS)  
 Total initial stream area = 5.500(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073(In/Hr)

+++++  
 Process from Point/Station 137.000 to Point/Station 138.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1086.600(Ft.)  
 End of street segment elevation = 1074.600(Ft.)  
 Length of street segment = 875.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 25.391(CFS)  
 Depth of flow = 0.460(Ft.), Average velocity = 3.725(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 18.268(Ft.)  
 Flow velocity = 3.72(Ft/s)  
 Travel time = 3.92 min. TC = 17.82 min.

Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.273(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.871  
 Subarea runoff = 19.972(CFS) for 11.000(Ac.)  
 Total runoff = 32.668(CFS)  
 Effective area this stream = 16.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 193.09(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 32.668(CFS)  
 Half street flow at end of street = 16.334(CFS)  
 Depth of flow = 0.497(Ft.), Average velocity = 3.974(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++  
 Process from Point/Station 138.000 to Point/Station 57.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1067.600(Ft.)  
 Downstream point/station elevation = 1041.300(Ft.)  
 Pipe length = 1320.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 32.668(CFS)  
 Given pipe size = 30.00(In.)  
 Calculated individual pipe flow = 32.668(CFS)

Normal flow depth in pipe = 16.13(In.)  
 Flow top width inside pipe = 29.92(In.)  
 Critical Depth = 23.34(In.)  
 Pipe flow velocity = 12.15(Ft/s)  
 Travel time through pipe = 1.81 min.  
 Time of concentration (TC) = 19.63 min.

\*\*\*\*\*  
 Process from Point/Station 57.000 to Point/Station 57.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
 Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 16.500(Ac.)  
 Runoff from this stream = 32.668(CFS)  
 Time of concentration = 19.63 min.  
 Rainfall intensity = 2.145(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000

\*\*\*\*\*  
 Process from Point/Station 139.000 to Point/Station 140.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

-----  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1074.700(Ft.)  
 Bottom (of initial area) elevation = 1069.700(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%) = 0.50  
 $TC = k(0.304) * [(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.902 min.  
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875  
 Subarea runoff = 12.696(CFS)  
 Total initial stream area = 5.500(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 140.000 to Point/Station 141.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

-----  
 Top of street segment elevation = 1069.700(Ft.)  
 End of street segment elevation = 1065.300(Ft.)  
 Length of street segment = 875.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street

Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 25.391 (CFS)  
 Depth of flow = 0.530(Ft.), Average velocity = 2.657(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 2.66(Ft/s)  
 Travel time = 5.49 min. TC = 19.39 min.

Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.161(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.869  
 Subarea runoff = 18.301(CFS) for 11.000(Ac.)  
 Total runoff = 30.997(CFS)  
 Effective area this stream = 16.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 209.59(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 30.997(CFS)  
 Half street flow at end of street = 15.498(CFS)  
 Depth of flow = 0.561(Ft.), Average velocity = 2.876(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++  
 Process from Point/Station 141.000 to Point/Station 141.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 16.500(Ac.)  
 Runoff from this stream = 30.997(CFS)  
 Time of concentration = 19.39 min.  
 Rainfall intensity = 2.161(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	343.395	21.19	2.049
2	32.668	19.63	2.145
3	30.997	19.39	2.161
Qmax(1) =			
	1.000 *	1.000 *	343.395) +
	0.954 *	1.000 *	32.668) +
	0.946 *	1.000 *	30.997) + = 403.878

$Q_{max}(2) =$   
     1.049 \*    0.926 \*    343.395) +  
     1.000 \*    1.000 \*    32.668) +  
     0.992 \*    1.000 \*    30.997) + =       397.121  
 $Q_{max}(3) =$   
     1.057 \*    0.915 \*    343.395) +  
     1.008 \*    0.988 \*    32.668) +  
     1.000 \*    1.000 \*    30.997) + =       395.682

Total of 3 streams to confluence:

Flow rates before confluence point:

    343.395       32.668       30.997

Maximum flow rates at confluence using above data:

    403.878       397.121       395.682

Area of streams before confluence:

    170.149       16.500       16.500

Effective area values after confluence:

    203.149       190.611       188.502

Results of confluence:

Total flow rate =    403.878(CFS)

Time of concentration =   21.190 min.

Effective stream area after confluence =    203.149(Ac.)

Stream Area average Pervious fraction( $A_p$ ) =   0.111

Stream Area average soil loss rate( $F_m$ ) =    0.083(In/Hr)

Study area (this main stream) =       203.15(Ac.)

++++++  
 Process from Point/Station           57.000 to Point/Station       63.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1041.300(Ft.)  
 Downstream point/station elevation = 1039.500(Ft.)  
 Pipe length = 560.00(Ft.)   Manning's N = 0.013  
 No. of pipes = 1   Required pipe flow = 403.878(CFS)  
 Given pipe size = 92.00(In.)  
 Calculated individual pipe flow = 403.878(CFS)  
 Normal flow depth in pipe = 66.66(In.)  
 Flow top width inside pipe = 82.20(In.)  
 Critical Depth = 62.03(In.)  
 Pipe flow velocity = 11.27(Ft/s)  
 Travel time through pipe = 0.83 min.  
 Time of concentration (TC) = 22.02 min.  
 End of computations, Total Study Area =           209.59 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction( $A_p$ ) = 0.111

Area averaged SCS curve number = 53.8

LINE "DZ-1"

## San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
 Rational Hydrology Study Date: 01/13/05

FONTANA / LINE DZ-1 HYDROLOGY  
 25 YEAR STORM  
 JN 04339

Hall & Forman, Inc. - S/N 950

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

Rational hydrology study storm event year is 25.0  
 10 Year storm 1 hour rainfall = 0.930(In.)  
 100 Year storm 1 hour rainfall = 1.350(In.)  
 Computed rainfall intensity:  
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
 Slope used for rainfall intensity curve b = 0.6000  
 Soil antecedent moisture condition (AMC) = 2

\*\*\*\*\*  
 Process from Point/Station 300.000 to Point/Station 301.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1068.100(Ft.)  
 Bottom (of initial area) elevation = 1063.100(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%) = 0.50  
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.902 min.  
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875  
 Subarea runoff = 11.541(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 301.000 to Point/Station 302.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1063.100(Ft.)  
 End of street segment elevation = 1060.000(Ft.)  
 Length of street segment = 620.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 28.277(CFS)  
 Depth of flow = 0.703(Ft.), Average velocity = 3.027(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 1.81(Ft.)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 30.392(Ft.)  
 Flow velocity = 3.03(Ft/s)  
 Travel time = 3.41 min. TC = 17.32 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073(In/Hr)  
 Rainfall intensity = 2.313(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.871  
 Subarea runoff = 27.756(CFS) for 14.500(Ac.)  
 Total runoff = 39.297(CFS)  
 Effective area this stream = 19.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 19.50(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 39.297(CFS)  
 Half street flow at end of street = 39.297(CFS)  
 Depth of flow = 0.789(Ft.), Average velocity = 3.146(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 6.12(Ft.)  
 Flow width (from curb towards crown)= 34.707(Ft.)

++++++  
 Process from Point/Station 302.000 to Point/Station 65.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1055.000(Ft.)  
 Downstream point/station elevation = 1051.700(Ft.)  
 Pipe length = 660.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 39.297(CFS)  
 Given pipe size = 36.00(In.)  
 Calculated individual pipe flow = 39.297(CFS)  
 Normal flow depth in pipe = 25.13(In.)  
 Flow top width inside pipe = 33.06(In.)  
 Critical Depth = 24.50(In.)  
 Pipe flow velocity = 7.47(Ft/s)  
 Travel time through pipe = 1.47 min.  
 Time of concentration (TC) = 18.79 min.

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+++++
Process from Point/Station      65.000 to Point/Station      65.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 1
Stream flow area =      19.500(Ac.)
Runoff from this stream =      39.297(CFS)
Time of concentration =      18.79 min.
Rainfall intensity =      2.202(In/Hr)
Area averaged loss rate (Fm) =      0.0734(In/Hr)
Area averaged Pervious ratio (Ap) = 0.1000

```

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+++++
Process from Point/Station      303.000 to Point/Station      304.000
**** INITIAL AREA EVALUATION ****

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RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 56.00
Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1064.500(Ft.)
Bottom (of initial area) elevation = 1060.000(Ft.)
Difference in elevation =      4.500(Ft.)
Slope =      0.00450 s(%)=      0.45
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 18.168 min.
Rainfall intensity =      2.247(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.753
Subarea runoff =      13.535(CFS)
Total initial stream area =      8.000(Ac.)
Pervious area fraction = 0.500
Initial area Fm value =      0.367(In/Hr)

```

```

+++++
Process from Point/Station      304.000 to Point/Station      304.000
**** CONFLUENCE OF MINOR STREAMS ****

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```

Along Main Stream number: 1 in normal stream number 2
Stream flow area =      8.000(Ac.)
Runoff from this stream =      13.535(CFS)
Time of concentration =      18.17 min.
Rainfall intensity =      2.247(In/Hr)
Area averaged loss rate (Fm) =      0.3670(In/Hr)
Area averaged Pervious ratio (Ap) = 0.5000
Summary of stream data:

```

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	39.297	18.79	2.202
2	13.535	18.17	2.247

$Q_{max}(1) =$   
           1.000 \*    1.000 \*    39.297) +  
           0.976 \*    1.000 \*    13.535) + =        52.509  
 $Q_{max}(2) =$   
           1.021 \*    0.967 \*    39.297) +  
           1.000 \*    1.000 \*    13.535) + =        52.334

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
           39.297        13.535  
 Maximum flow rates at confluence using above data:  
           52.509        52.334  
 Area of streams before confluence:  
           19.500        8.000  
 Effective area values after confluence:  
           27.500        26.856

Results of confluence:  
 Total flow rate =        52.509(CFS)  
 Time of concentration =    18.789 min.  
 Effective stream area after confluence =    27.500(Ac.)  
 Stream Area average Pervious fraction( $A_p$ ) = 0.216  
 Stream Area average soil loss rate( $F_m$ ) = 0.159(In/Hr)  
 Study area (this main stream) =        27.50(Ac.)

++++++  
 Process from Point/Station        65.000 to Point/Station        66.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1051.700(Ft.)  
 Downstream point/station elevation = 1048.400(Ft.)  
 Pipe length = 660.00(Ft.)    Manning's N = 0.013  
 No. of pipes = 1    Required pipe flow = 52.509(CFS)  
 Given pipe size = 48.00(In.)  
 Calculated individual pipe flow = 52.509(CFS)  
 Normal flow depth in pipe = 24.47(In.)  
 Flow top width inside pipe = 47.99(In.)  
 Critical Depth = 26.14(In.)  
 Pipe flow velocity = 8.15(Ft/s)  
 Travel time through pipe = 1.35 min.  
 Time of concentration (TC) = 20.14 min.

++++++  
 Process from Point/Station        66.000 to Point/Station        66.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 27.500(Ac.)  
 Runoff from this stream = 52.509(CFS)  
 Time of concentration = 20.14 min.  
 Rainfall intensity = 2.112(In/Hr)  
 Area averaged loss rate ( $F_m$ ) = 0.1588(In/Hr)  
 Area averaged Pervious ratio ( $A_p$ ) = 0.2164

++++++  
 Process from Point/Station        305.000 to Point/Station        306.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

SCHOOL subarea

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.6000      Max loss rate(Fm)=      0.440(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1062.000(Ft.)  
 Bottom (of initial area) elevation = 1055.400(Ft.)  
 Difference in elevation =      6.600(Ft.)  
 Slope =      0.00660    s(%)=      0.66  
 $TC = k(0.412)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 17.823 min.  
 Rainfall intensity = 2.273(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.726  
 Subarea runoff = 13.193(CFS)  
 Total initial stream area = 8.000(Ac.)  
 Pervious area fraction = 0.600  
 Initial area Fm value = 0.440(In/Hr)

++++++  
 Process from Point/Station      306.000 to Point/Station      306.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 8.000(Ac.)  
 Runoff from this stream = 13.193(CFS)  
 Time of concentration = 17.82 min.  
 Rainfall intensity = 2.273(In/Hr)  
 Area averaged loss rate (Fm) = 0.4404(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.6000

++++++  
 Process from Point/Station      307.000 to Point/Station      308.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1070.100(Ft.)  
 Bottom (of initial area) elevation = 1065.100(Ft.)  
 Difference in elevation =      5.000(Ft.)  
 Slope =      0.00500    s(%)=      0.50  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 17.789 min.  
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755  
 Subarea runoff = 8.588(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

+++++  
 Process from Point/Station 308.000 to Point/Station 309.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1065.100(Ft.)  
 End of street segment elevation = 1062.700(Ft.)  
 Length of street segment = 650.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 17.176(CFS)  
 Depth of flow = 0.499(Ft.), Average velocity = 2.073(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 2.07(Ft/s)  
 Travel time = 5.23 min. TC = 23.02 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 1.950(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.731  
 Subarea runoff = 12.777(CFS) for 10.000(Ac.)  
 Total runoff = 21.365(CFS)  
 Effective area this stream = 15.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 50.50(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 21.365(CFS)  
 Half street flow at end of street = 10.682(CFS)  
 Depth of flow = 0.528(Ft.), Average velocity = 2.260(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++  
 Process from Point/Station 309.000 to Point/Station 310.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1062.700(Ft.)  
 End of street segment elevation = 1055.400(Ft.)  
 Length of street segment = 1450.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)

Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 32.047(CFS)  
 Depth of flow = 0.566(Ft.), Average velocity = 2.915(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 2.92(Ft/s)  
 Travel time = 8.29 min. TC = 31.31 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 1.621(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.696  
 Subarea runoff = 12.494(CFS) for 15.000(Ac.)  
 Total runoff = 33.859(CFS)  
 Effective area this stream = 30.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 65.50(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 33.859(CFS)  
 Half street flow at end of street = 16.929(CFS)  
 Depth of flow = 0.576(Ft.), Average velocity = 2.980(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++  
 Process from Point/Station 310.000 to Point/Station 310.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 30.000(Ac.)  
 Runoff from this stream = 33.859(CFS)  
 Time of concentration = 31.31 min.  
 Rainfall intensity = 1.621(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	52.509	20.14	2.112
2	13.193	17.82	2.273
3	33.859	31.31	1.621
Qmax(1) =			

	1.000 *	1.000 *	52.509) +	
	0.912 *	1.000 *	13.193) +	
	1.392 *	0.643 *	33.859) + =	94.859
Qmax(2) =				
	1.082 *	0.885 *	52.509) +	
	1.000 *	1.000 *	13.193) +	
	1.520 *	0.569 *	33.859) + =	92.783
Qmax(3) =				
	0.749 *	1.000 *	52.509) +	
	0.644 *	1.000 *	13.193) +	
	1.000 *	1.000 *	33.859) + =	81.665

Total of 3 streams to confluence:

Flow rates before confluence point:

52.509      13.193      33.859

Maximum flow rates at confluence using above data:

94.859      92.783      81.665

Area of streams before confluence:

27.500      8.000      30.000

Effective area values after confluence:

54.799      49.419      65.500

Results of confluence:

Total flow rate = 94.859(CFS)

Time of concentration = 20.139 min.

Effective stream area after confluence = 54.799(Ac.)

Stream Area average Pervious fraction(Ap) = 0.393

Stream Area average soil loss rate(Fm) = 0.289(In/Hr)

Study area (this main stream) = 65.50(Ac.)

\*\*\*\*\*  
 Process from Point/Station      66.000 to Point/Station      67.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1048.400(Ft.)  
 Downstream point/station elevation = 1044.600(Ft.)  
 Pipe length = 760.00(Ft.)      Manning's N = 0.013  
 No. of pipes = 1      Required pipe flow = 94.859(CFS)  
 Given pipe size = 54.00(In.)  
 Calculated individual pipe flow = 94.859(CFS)  
 Normal flow depth in pipe = 32.72(In.)  
 Flow top width inside pipe = 52.77(In.)  
 Critical Depth = 34.30(In.)  
 Pipe flow velocity = 9.41(Ft/s)  
 Travel time through pipe = 1.35 min.  
 Time of concentration (TC) = 21.49 min.

\*\*\*\*\*  
 Process from Point/Station      67.000 to Point/Station      67.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 54.799(Ac.)  
 Runoff from this stream = 94.859(CFS)  
 Time of concentration = 21.49 min.  
 Rainfall intensity = 2.032(In/Hr)  
 Area averaged loss rate (Fm) = 0.2885(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.3931

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+++++
Process from Point/Station      311.000 to Point/Station      312.000
**** INITIAL AREA EVALUATION ****

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RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 56.00
Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1062.400(Ft.)
Bottom (of initial area) elevation = 1057.400(Ft.)
Difference in elevation =      5.000(Ft.)
Slope =      0.00500  s(%)=      0.50
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 17.789 min.
Rainfall intensity =      2.275(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
Subarea runoff =      13.741(CFS)
Total initial stream area =      8.000(Ac.)
Pervious area fraction = 0.500
Initial area Fm value =      0.367(In/Hr)

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+++++
Process from Point/Station      312.000 to Point/Station      313.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

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Top of street segment elevation = 1057.400(Ft.)
End of street segment elevation = 1052.600(Ft.)
Length of street segment = 960.000(Ft.)
Height of curb above gutter flowline = 8.0(In.)
Width of half street (curb to crown) = 20.000(Ft.)
Distance from crown to crossfall grade break = 18.500(Ft.)
Slope from gutter to grade break (v/hz) = 0.020
Slope from grade break to crown (v/hz) = 0.020
Street flow is on [2] side(s) of the street
Distance from curb to property line = 10.000(Ft.)
Slope from curb to property line (v/hz) = 0.020
Gutter width = 1.500(Ft.)
Gutter hike from flowline = 1.500(In.)
Manning's N in gutter = 0.0150
Manning's N from gutter to grade break = 0.0150
Manning's N from grade break to crown = 0.0150
Estimated mean flow rate at midpoint of street = 20.611(CFS)
Depth of flow = 0.502(Ft.), Average velocity = 2.442(Ft/s)
Note: depth of flow exceeds top of street crown.
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width = 20.000(Ft.)
Flow velocity = 2.44(Ft/s)
Travel time = 6.55 min.      TC = 24.34 min.
Adding area flow to street
SCHOOL subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 56.00

```

Pervious ratio(Ap) = 0.6000      Max loss rate(Fm)=      0.440(In/Hr)  
 Rainfall intensity =      1.885(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area,(total area with modified  
 rational method) (Q=KCIA) is C = 0.707  
 Subarea runoff =      7.592(CFS) for      8.000(Ac.)  
 Total runoff =      21.333(CFS)  
 Effective area this stream =      16.00(Ac.)  
 Total Study Area (Main Stream No. 1) =      81.50(Ac.)  
 Area averaged Fm value =      0.404(In/Hr)  
 Street flow at end of street =      21.333(CFS)  
 Half street flow at end of street =      10.666(CFS)  
 Depth of flow =      0.507(Ft.), Average velocity =      2.475(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)=      20.000(Ft.)

++++  
 Process from Point/Station      313.000 to Point/Station      313.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
 Along Main Stream number: 1 in normal stream number 2  
 Stream flow area =      16.000(Ac.)  
 Runoff from this stream =      21.333(CFS)  
 Time of concentration =      24.34 min.  
 Rainfall intensity =      1.885(In/Hr)  
 Area averaged loss rate (Fm) =      0.4037(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5500  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	94.859	21.49	2.032
2	21.333	24.34	1.885
Qmax(1) =	1.000 *	1.000 *	94.859) +
	1.099 *	0.883 *	21.333) + =      115.552
Qmax(2) =	0.916 *	1.000 *	94.859) +
	1.000 *	1.000 *	21.333) + =      108.212

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
     94.859      21.333  
 Maximum flow rates at confluence using above data:  
     115.552      108.212  
 Area of streams before confluence:  
     54.799      16.000  
 Effective area values after confluence:  
     68.921      70.799  
 Results of confluence:  
 Total flow rate =      115.552(CFS)  
 Time of concentration =      21.485 min.  
 Effective stream area after confluence =      68.921(Ac.)  
 Stream Area average Pervious fraction(Ap) =      0.429  
 Stream Area average soil loss rate(Fm) =      0.315(In/Hr)  
 Study area (this main stream) =      70.80(Ac.)

++++

Process from Point/Station 67.000 to Point/Station 68.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1044.600(Ft.)  
 Downstream point/station elevation = 1040.800(Ft.)  
 Pipe length = 760.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 115.552(CFS)  
 Given pipe size = 60.00(In.)  
 Calculated individual pipe flow = 115.552(CFS)  
 Normal flow depth in pipe = 34.45(In.)  
 Flow top width inside pipe = 59.34(In.)  
 Critical Depth = 36.80(In.)  
 Pipe flow velocity = 9.91(Ft/s)  
 Travel time through pipe = 1.28 min.  
 Time of concentration (TC) = 22.76 min.

+++++  
 Process from Point/Station 68.000 to Point/Station 68.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

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The following data inside Main Stream is listed:

In Main Stream number: 1  
 Effective stream flow area = 68.921(Ac.)  
 Total study area this main stream = 81.500(Ac.)  
 Runoff from this stream = 115.552(CFS)  
 Time of concentration = 22.76 min.  
 Rainfall intensity = 1.962(In/Hr)  
 Area averaged loss rate (Fm) = 0.3146(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.4286  
 Program is now starting with Main Stream No. 2

+++++  
 Process from Point/Station 314.000 to Point/Station 315.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

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RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1079.500(Ft.)  
 Bottom (of initial area) elevation = 1074.500(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%)= 0.50  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 17.789 min.  
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755  
 Subarea runoff = 8.588(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

+++++

Process from Point/Station 315.000 to Point/Station 318.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1074.500(Ft.)  
 End of street segment elevation = 1069.500(Ft.)  
 Length of street segment = 1000.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 15.888(CFS)  
 Depth of flow = 0.465(Ft.), Average velocity = 2.269(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 18.520(Ft.)  
 Flow velocity = 2.27(Ft/s)  
 Travel time = 7.35 min. TC = 25.13 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 1.849(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.721  
 Subarea runoff = 9.421(CFS) for 8.500(Ac.)  
 Total runoff = 18.009(CFS)  
 Effective area this stream = 13.50(Ac.)  
 Total Study Area (Main Stream No. 2) = 13.50(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 18.009(CFS)  
 Half street flow at end of street = 9.005(CFS)  
 Depth of flow = 0.484(Ft.), Average velocity = 2.340(Ft/s)  
 Flow width (from curb towards crown)= 19.433(Ft.)

+++++  
 Process from Point/Station 318.000 to Point/Station 318.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 2 in normal stream number 1  
 Stream flow area = 13.500(Ac.)  
 Runoff from this stream = 18.009(CFS)  
 Time of concentration = 25.13 min.  
 Rainfall intensity = 1.849(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000

+++++

Process from Point/Station 316.000 to Point/Station 317.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1079.500(Ft.)  
 Bottom (of initial area) elevation = 1074.500(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%) = 0.50  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 17.789 min.  
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755  
 Subarea runoff = 8.588(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

+++++  
 Process from Point/Station 317.000 to Point/Station 318.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1074.500(Ft.)  
 End of street segment elevation = 1069.500(Ft.)  
 Length of street segment = 1000.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 16.317(CFS)  
 Depth of flow = 0.469(Ft.), Average velocity = 2.284(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 18.711(Ft.)  
 Flow velocity = 2.28(Ft/s)  
 Travel time = 7.30 min. TC = 25.09 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 1.851(In/Hr) for a 25.0 year storm

Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.722  
 Subarea runoff = 10.115(CFS) for 9.000(Ac.)  
 Total runoff = 18.703(CFS)  
 Effective area this stream = 14.00(Ac.)  
 Total Study Area (Main Stream No. 2) = 27.50(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 18.703(CFS)  
 Half street flow at end of street = 9.351(CFS)  
 Depth of flow = 0.489(Ft.), Average velocity = 2.362(Ft/s)  
 Flow width (from curb towards crown)= 19.717(Ft.)

++++  
 Process from Point/Station 318.000 to Point/Station 318.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 14.000(Ac.)  
 Runoff from this stream = 18.703(CFS)  
 Time of concentration = 25.09 min.  
 Rainfall intensity = 1.851(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	18.009	25.13	1.849
2	18.703	25.09	1.851
Qmax(1) =			
	1.000 *	1.000 *	18.009) +
	0.999 *	1.000 *	18.703) + = 36.685
Qmax(2) =			
	1.001 *	0.998 *	18.009) +
	1.000 *	1.000 *	18.703) + = 36.703

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 18.009 18.703  
 Maximum flow rates at confluence using above data:  
 36.685 36.703  
 Area of streams before confluence:  
 13.500 14.000  
 Effective area values after confluence:  
 27.500 27.474  
 Results of confluence:  
 Total flow rate = 36.703(CFS)  
 Time of concentration = 25.087 min.  
 Effective stream area after confluence = 27.474(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.500  
 Stream Area average soil loss rate(Fm) = 0.367(In/Hr)  
 Study area (this main stream) = 27.50(Ac.)

++++  
 Process from Point/Station 318.000 to Point/Station 319.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1069.500(Ft.)  
 End of street segment elevation = 1063.000(Ft.)  
 Length of street segment = 1300.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 49.061(CFS)  
 Depth of flow = 0.648(Ft.), Average velocity = 3.444(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 3.44(Ft/s)  
 Travel time = 6.29 min. TC = 31.38 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 1.619(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.696  
 Subarea runoff = 15.091(CFS) for 18.500(Ac.)  
 Total runoff = 51.795(CFS)  
 Effective area this stream = 45.97(Ac.)  
 Total Study Area (Main Stream No. 2) = 46.00(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 51.795(CFS)  
 Half street flow at end of street = 25.897(CFS)  
 Depth of flow = 0.659(Ft.), Average velocity = 3.519(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 319.000 to Point/Station 68.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1054.800(Ft.)  
 Downstream point/station elevation = 1041.800(Ft.)  
 Pipe length = 900.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 51.795(CFS)  
 Given pipe size = 48.00(In.)  
 Calculated individual pipe flow = 51.795(CFS)  
 Normal flow depth in pipe = 18.02(In.)  
 Flow top width inside pipe = 46.49(In.)  
 Critical Depth = 25.91(In.)  
 Pipe flow velocity = 12.01(Ft/s)  
 Travel time through pipe = 1.25 min.

Time of concentration (TC) = 32.63 min.

\*\*\*\*\*  
 Process from Point/Station 68.000 to Point/Station 68.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 2  
 Effective stream flow area = 45.974 (Ac.)  
 Total study area this main stream = 46.000 (Ac.)  
 Runoff from this stream = 51.795 (CFS)  
 Time of concentration = 32.63 min.  
 Rainfall intensity = 1.581 (In/Hr)  
 Area averaged loss rate (Fm) = 0.3670 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	115.552	22.76	1.962
2	51.795	32.63	1.581
Qmax(1) =			
	1.000 *	1.000 *	115.552) +
	1.314 *	0.698 *	51.795) + = 163.034
Qmax(2) =			
	0.769 *	1.000 *	115.552) +
	1.000 *	1.000 *	51.795) + = 140.618

Total of 2 main streams to confluence:

Flow rates before confluence point:

116.552      52.795

Maximum flow rates at confluence using above data:

163.034      140.618

Effective Area of streams before confluence:

68.921      45.974

Effective area values after confluence:

100.998      114.895

Results of confluence:

Total flow rate = 163.034 (CFS)

Time of concentration = 22.764 min.

Effective stream area after confluence = 100.998 (Ac.)

Stream Area average Pervious fraction (Ap) = 0.457

Stream Area average soil loss rate (Fm) = 0.336 (In/Hr)

Stream effective area = 114.90 (Ac.)

\*\*\*\*\*  
 Process from Point/Station 68.000 to Point/Station 68.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 100.998 (Ac.)

Runoff from this stream = 163.034 (CFS)

Time of concentration = 22.76 min.

Rainfall intensity = 1.962 (In/Hr)

Area averaged loss rate (Fm) = 0.3355 (In/Hr)

Area averaged Pervious ratio (Ap) = 0.4572

+++++  
 Process from Point/Station 320.000 to Point/Station 321.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1057.100(Ft.)  
 Bottom (of initial area) elevation = 1052.100(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%)= 0.50  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 17.789 min.  
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755  
 Subarea runoff = 11.164(CFS)  
 Total initial stream area = 6.500(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

+++++  
 Process from Point/Station 321.000 to Point/Station 321.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 6.500(Ac.)  
 Runoff from this stream = 11.164(CFS)  
 Time of concentration = 17.79 min.  
 Rainfall intensity = 2.275(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000

+++++  
 Process from Point/Station 322.000 to Point/Station 323.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1057.100(Ft.)  
 Bottom (of initial area) elevation = 1052.100(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%)= 0.50  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$

Initial area time of concentration = 17.789 min.  
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755  
 Subarea runoff = 8.588(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

++++  
 Process from Point/Station 323.000 to Point/Station 323.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 5.000(Ac.)  
 Runoff from this stream = 8.588(CFS)  
 Time of concentration = 17.79 min.  
 Rainfall intensity = 2.275(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	163.034	22.76	1.962
2	11.164	17.79	2.275
3	8.588	17.79	2.275
Qmax(1) =			
	1.000 *	1.000 *	163.034) +
	0.836 *	1.000 *	11.164) +
	0.836 *	1.000 *	8.588) + = 179.547
Qmax(2) =			
	1.192 *	0.781 *	163.034) +
	1.000 *	1.000 *	11.164) +
	1.000 *	1.000 *	8.588) + = 171.663
Qmax(3) =			
	1.192 *	0.781 *	163.034) +
	1.000 *	1.000 *	11.164) +
	1.000 *	1.000 *	8.588) + = 171.663

Total of 3 streams to confluence:  
 Flow rates before confluence point:  
 163.034      11.164      8.588  
 Maximum flow rates at confluence using above data:  
 179.547      171.663      171.663  
 Area of streams before confluence:  
 100.998      6.500      5.000  
 Effective area values after confluence:  
 112.498      90.426      90.426  
 Results of confluence:  
 Total flow rate = 179.547(CFS)  
 Time of concentration = 22.764 min.  
 Effective stream area after confluence = 112.498(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.462  
 Stream Area average soil loss rate(Fm) = 0.339(In/Hr)  
 Study area (this main stream) = 112.50(Ac.)

++++

Process from Point/Station 68.000 to Point/Station 69.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1040.800(Ft.)  
Downstream point/station elevation = 1038.800(Ft.)  
Pipe length = 400.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 179.547(CFS)  
Given pipe size = 84.00(In.)  
Calculated individual pipe flow = 179.547(CFS)  
Normal flow depth in pipe = 36.80(In.)  
Flow top width inside pipe = 83.35(In.)  
Critical Depth = 41.80(In.)  
Pipe flow velocity = 11.06(Ft/s)  
Travel time through pipe = 0.60 min.  
Time of concentration (TC) = 23.37 min.

+++++  
Process from Point/Station 69.000 to Point/Station 69.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
Stream flow area = 112.498(Ac.)  
Runoff from this stream = 179.547(CFS)  
Time of concentration = 23.37 min.  
Rainfall intensity = 1.932(In/Hr)  
Area averaged loss rate (Fm) = 0.3387(In/Hr)  
Area averaged Pervious ratio (Ap) = 0.4615

+++++  
Process from Point/Station 324.000 to Point/Station 325.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

RESIDENTIAL(5 - 7 dwl/acre)  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
SCS curve number for soil(AMC 2) = 56.00  
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
Initial subarea data:  
Initial area flow distance = 1000.000(Ft.)  
Top (of initial area) elevation = 1055.000(Ft.)  
Bottom (of initial area) elevation = 1050.000(Ft.)  
Difference in elevation = 5.000(Ft.)  
Slope = 0.00500 s(%)= 0.50  
TC = k(0.389)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 17.789 min.  
Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
Effective runoff coefficient used for area (Q=KCIA) is C = 0.755  
Subarea runoff = 13.741(CFS)  
Total initial stream area = 8.000(Ac.)  
Pervious area fraction = 0.500  
Initial area Fm value = 0.367(In/Hr)

+++++  
Process from Point/Station 325.000 to Point/Station 325.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 8.000(Ac.)  
 Runoff from this stream = 13.741(CFS)  
 Time of concentration = 17.79 min.  
 Rainfall intensity = 2.275(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000

++++  
 Process from Point/Station 326.000 to Point/Station 327.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1055.000(Ft.)  
 Bottom (of initial area) elevation = 1050.000(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%)= 0.50  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 17.789 min.  
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755  
 Subarea runoff = 12.023(CFS)  
 Total initial stream area = 7.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

++++  
 Process from Point/Station 327.000 to Point/Station 327.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 7.000(Ac.)  
 Runoff from this stream = 12.023(CFS)  
 Time of concentration = 17.79 min.  
 Rainfall intensity = 2.275(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	179.547	23.37	1.932
2	13.741	17.79	2.275
3	12.023	17.79	2.275
Qmax(1) =			
	1.000 *	1.000 *	179.547) +
	0.820 *	1.000 *	13.741) +
	0.820 *	1.000 *	12.023) + = 200.674
Qmax(2) =			

	1.216 *	0.761 *	179.547) +	
	1.000 *	1.000 *	13.741) +	
	1.000 *	1.000 *	12.023) + =	191.922
Qmax(3) =				
	1.216 *	0.761 *	179.547) +	
	1.000 *	1.000 *	13.741) +	
	1.000 *	1.000 *	12.023) + =	191.922

Total of 3 streams to confluence:  
Flow rates before confluence point:  
179.547      13.741      12.023  
Maximum flow rates at confluence using above data:  
200.674      191.922      191.922  
Area of streams before confluence:  
112.498      8.000      7.000  
Effective area values after confluence:  
127.498      100.646      100.646  
Results of confluence:  
Total flow rate = 200.674(CFS)  
Time of concentration = 23.366 min.  
Effective stream area after confluence = 127.498(Ac.)  
Stream Area average Pervious fraction(Ap) = 0.466  
Stream Area average soil loss rate(Fm) = 0.342(In/Hr)  
Study area (this main stream) = 127.50(Ac.)

\*\*\*\*\*  
Process from Point/Station      69.000 to Point/Station      70.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1038.800(Ft.)  
Downstream point/station elevation = 1034.600(Ft.)  
Pipe length = 880.00(Ft.)      Manning's N = 0.013  
No. of pipes = 1      Required pipe flow = 200.674(CFS)  
Given pipe size = 96.00(In.)  
Calculated individual pipe flow = 200.674(CFS)  
Normal flow depth in pipe = 37.22(In.)  
Flow top width inside pipe = 93.55(In.)  
Critical Depth = 42.53(In.)  
Pipe flow velocity = 11.14(Ft/s)  
Travel time through pipe = 1.32 min.  
Time of concentration (TC) = 24.68 min.

\*\*\*\*\*  
Process from Point/Station      70.000 to Point/Station      70.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
Stream flow area = 127.498(Ac.)  
Runoff from this stream = 200.674(CFS)  
Time of concentration = 24.68 min.  
Rainfall intensity = 1.869(In/Hr)  
Area averaged loss rate (Fm) = 0.3421(In/Hr)  
Area averaged Pervious ratio (Ap) = 0.4661

\*\*\*\*\*  
Process from Point/Station      328.000 to Point/Station      329.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1057.800(Ft.)  
 Bottom (of initial area) elevation = 1052.800(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%)= 0.50  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 17.789 min.  
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755  
 Subarea runoff = 8.588(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

+++++  
 Process from Point/Station 329.000 to Point/Station 330.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1052.800(Ft.)  
 End of street segment elevation = 1048.800(Ft.)  
 Length of street segment = 800.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 18.893(CFS)  
 Depth of flow = 0.491(Ft.), Average velocity = 2.368(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 19.793(Ft.)  
 Flow velocity = 2.37(Ft/s)  
 Travel time = 5.63 min.      TC = 23.42 min.

Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)  
 Rainfall intensity = 1.929(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.729  
 Subarea runoff = 15.316(CFS) for 12.000(Ac.)

Total runoff = 23.904(CFS)  
 Effective area this stream = 17.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 89.50(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 23.904(CFS)  
 Half street flow at end of street = 11.952(CFS)  
 Depth of flow = 0.522(Ft.), Average velocity = 2.590(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 330.000 to Point/Station 331.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1048.800(Ft.)  
 End of street segment elevation = 1045.500(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 35.856(CFS)  
 Depth of flow = 0.586(Ft.), Average velocity = 3.042(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 3.04(Ft/s)  
 Travel time = 3.62 min. TC = 27.04 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 1.770(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.713  
 Subarea runoff = 19.031(CFS) for 17.000(Ac.)  
 Total runoff = 42.935(CFS)  
 Effective area this stream = 34.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 106.50(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 42.935(CFS)  
 Half street flow at end of street = 21.467(CFS)  
 Depth of flow = 0.620(Ft.), Average velocity = 3.267(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

```

+++++
Process from Point/Station      331.000 to Point/Station      70.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****

```

```

Upstream point/station elevation = 1038.600(Ft.)
Downstream point/station elevation = 1034.600(Ft.)
Pipe length = 800.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 42.935(CFS)
Given pipe size = 42.00(In.)
Calculated individual pipe flow = 42.935(CFS)
Normal flow depth in pipe = 23.53(In.)
Flow top width inside pipe = 41.69(In.)
Critical Depth = 24.51(In.)
Pipe flow velocity = 7.74(Ft/s)
Travel time through pipe = 1.72 min.
Time of concentration (TC) = 28.76 min.

```

```

+++++
Process from Point/Station      70.000 to Point/Station      70.000
**** CONFLUENCE OF MINOR STREAMS ****

```

```

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 34.000(Ac.)
Runoff from this stream = 42.935(CFS)
Time of concentration = 28.76 min.
Rainfall intensity = 1.706(In/Hr)
Area averaged loss rate (Fm) = 0.3670(In/Hr)
Area averaged Pervious ratio (Ap) = 0.5000

```

```

+++++
Process from Point/Station      332.000 to Point/Station      333.000
**** INITIAL AREA EVALUATION ****

```

```

RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 56.00
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1053.200(Ft.)
Bottom (of initial area) elevation = 1048.200(Ft.)
Difference in elevation = 5.000(Ft.)
Slope = 0.00500 s(%)= 0.50
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 17.789 min.
Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
Subarea runoff = 8.588(CFS)
Total initial stream area = 5.000(Ac.)
Pervious area fraction = 0.500
Initial area Fm value = 0.367(In/Hr)

```

```

+++++
Process from Point/Station      333.000 to Point/Station      334.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

```

Top of street segment elevation = 1048.200(Ft.)  
 End of street segment elevation = 1045.600(Ft.)  
 Length of street segment = 520.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 15.458(CFS)  
 Depth of flow = 0.462(Ft.), Average velocity = 2.254(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 18.326(Ft.)  
 Flow velocity = 2.25(Ft/s)  
 Travel time = 3.85 min. TC = 21.63 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 2.023(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.737  
 Subarea runoff = 10.791(CFS) for 8.000(Ac.)  
 Total runoff = 19.379(CFS)  
 Effective area this stream = 13.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 119.50(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 19.379(CFS)  
 Half street flow at end of street = 9.689(CFS)  
 Depth of flow = 0.495(Ft.), Average velocity = 2.383(Ft/s)  
 Flow width (from curb towards crown)= 19.986(Ft.)

++++++  
 Process from Point/Station 334.000 to Point/Station 334.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 13.000(Ac.)  
 Runoff from this stream = 19.379(CFS)  
 Time of concentration = 21.63 min.  
 Rainfall intensity = 2.023(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000

++++++  
 Process from Point/Station 335.000 to Point/Station 336.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

## RESIDENTIAL(5 - 7 dwl/acre)

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1053.200(Ft.)  
 Bottom (of initial area) elevation = 1048.200(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500    s(%)= 0.50  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 17.789 min.  
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755  
 Subarea runoff = 10.306(CFS)  
 Total initial stream area = 6.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

++++++  
 Process from Point/Station      336.000 to Point/Station      337.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1048.200(Ft.)  
 End of street segment elevation = 1045.600(Ft.)  
 Length of street segment = 520.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 21.470(CFS)  
 Depth of flow = 0.508(Ft.), Average velocity = 2.482(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 2.48(Ft/s)  
 Travel time = 3.49 min.      TC = 21.28 min.  
 Adding area flow to street

## RESIDENTIAL(5 - 7 dwl/acre)

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)  
 Rainfall intensity = 2.043(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified

rational method) (Q=KCIA) is C = 0.738  
 Subarea runoff = 18.361(CFS) for 13.000(Ac.)  
 Total runoff = 28.667(CFS)  
 Effective area this stream = 19.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 138.50(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 28.667(CFS)  
 Half street flow at end of street = 14.333(CFS)  
 Depth of flow = 0.549(Ft.), Average velocity = 2.783(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++  
 Process from Point/Station 337.000 to Point/Station 337.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 4  
 Stream flow area = 19.000(Ac.)  
 Runoff from this stream = 28.667(CFS)  
 Time of concentration = 21.28 min.  
 Rainfall intensity = 2.043(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	200.674	24.68	1.869
2	42.935	28.76	1.706
3	19.379	21.63	2.023
4	28.667	21.28	2.043
Qmax(1) =			
	1.000 *	1.000 *	200.674) +
	1.122 *	0.858 *	42.935) +
	0.907 *	1.000 *	19.379) +
	0.896 *	1.000 *	28.667) + = 285.304
Qmax(2) =			
	0.893 *	1.000 *	200.674) +
	1.000 *	1.000 *	42.935) +
	0.808 *	1.000 *	19.379) +
	0.799 *	1.000 *	28.667) + = 260.649
Qmax(3) =			
	1.101 *	0.876 *	200.674) +
	1.237 *	0.752 *	42.935) +
	1.000 *	1.000 *	19.379) +
	0.988 *	1.000 *	28.667) + = 281.275
Qmax(4) =			
	1.114 *	0.862 *	200.674) +
	1.252 *	0.740 *	42.935) +
	1.012 *	0.984 *	19.379) +
	1.000 *	1.000 *	28.667) + = 280.471

Total of 4 streams to confluence:  
 Flow rates before confluence point:  
 200.674      42.935      19.379      28.667  
 Maximum flow rates at confluence using above data:  
 285.304      260.649      281.275      280.471  
 Area of streams before confluence:

127.498	34.000	13.000	19.000
Effective area values after confluence:			
188.681	193.498	169.329	166.874

Results of confluence:  
 Total flow rate = 285.304 (CFS)  
 Time of concentration = 24.684 min.  
 Effective stream area after confluence = 188.681 (Ac.)  
 Stream Area average Pervious fraction (Ap) = 0.478  
 Stream Area average soil loss rate (Fm) = 0.351 (In/Hr)  
 Study area (this main stream) = 193.50 (Ac.)

+++++  
 Process from Point/Station 70.000 to Point/Station 71.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1034.600 (Ft.)  
 Downstream point/station elevation = 1030.600 (Ft.)  
 Pipe length = 800.00 (Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 285.304 (CFS)  
 Given pipe size = 102.00 (In.)  
 Calculated individual pipe flow = 285.304 (CFS)  
 Normal flow depth in pipe = 43.36 (In.)  
 Flow top width inside pipe = 100.85 (In.)  
 Critical Depth = 50.20 (In.)  
 Pipe flow velocity = 12.41 (Ft/s)  
 Travel time through pipe = 1.07 min.  
 Time of concentration (TC) = 25.76 min.

+++++  
 Process from Point/Station 71.000 to Point/Station 71.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 188.681 (Ac.)  
 Runoff from this stream = 285.304 (CFS)  
 Time of concentration = 25.76 min.  
 Rainfall intensity = 1.822 (In/Hr)  
 Area averaged loss rate (Fm) = 0.3506 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.4776

+++++  
 Process from Point/Station 338.000 to Point/Station 339.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 56.00  
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.073 (In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000 (Ft.)  
 Top (of initial area) elevation = 1056.000 (Ft.)  
 Bottom (of initial area) elevation = 1051.000 (Ft.)  
 Difference in elevation = 5.000 (Ft.)  
 Slope = 0.00500 s(%) = 0.50  
 TC = k(0.304)\*[(length^3)/(elevation change)]^0.2

Initial area time of concentration = 13.902 min.  
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875  
 Subarea runoff = 11.541(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073(In/Hr)

++++  
 Process from Point/Station 339.000 to Point/Station 340.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1051.000(Ft.)  
 End of street segment elevation = 1048.600(Ft.)  
 Length of street segment = 480.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 21.929(CFS)  
 Depth of flow = 0.511(Ft.), Average velocity = 2.503(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 2.50(Ft/s)  
 Travel time = 3.20 min. TC = 17.10 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.330(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.872  
 Subarea runoff = 16.893(CFS) for 9.000(Ac.)  
 Total runoff = 28.434(CFS)  
 Effective area this stream = 14.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 152.50(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 28.434(CFS)  
 Half street flow at end of street = 14.217(CFS)  
 Depth of flow = 0.548(Ft.), Average velocity = 2.775(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++  
 Process from Point/Station 340.000 to Point/Station 340.000

\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 14.000 (Ac.)  
 Runoff from this stream = 28.434 (CFS)  
 Time of concentration = 17.10 min.  
 Rainfall intensity = 2.330 (In/Hr)  
 Area averaged loss rate (Fm) = 0.0734 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	285.304	25.76	1.822
2	28.434	17.10	2.330
Qmax(1) =			
	1.000 *	1.000 *	285.304) +
	0.775 *	1.000 *	28.434) + = 307.340
Qmax(2) =			
	1.345 *	0.664 *	285.304) +
	1.000 *	1.000 *	28.434) + = 283.184

Total of 2 streams to confluence:

Flow rates before confluence point:

285.304      28.434

Maximum flow rates at confluence using above data:

307.340      283.184

Area of streams before confluence:

188.681      14.000

Effective area values after confluence:

202.681      139.253

Results of confluence:

Total flow rate = 307.340 (CFS)

Time of concentration = 25.758 min.

Effective stream area after confluence = 202.681 (Ac.)

Stream Area average Pervious fraction (Ap) = 0.452

Stream Area average soil loss rate (Fm) = 0.331 (In/Hr)

Study area (this main stream) = 202.68 (Ac.)

End of computations, Total Study Area = 234.00 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction (Ap) = 0.450

Area averaged SCS curve number = 56.0

LINE 'P3'

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
Rational Hydrology Study Date: 01/13/05

-----  
FONTANA / LINE P3 HYDROLOGY  
25 YEAR STORM  
JN 04339  
-----

Hall & Forman, Inc. - S/N 950  
-----

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

-----  
Rational hydrology study storm event year is 25.0  
10 Year storm 1 hour rainfall = 0.930(In.)  
100 Year storm 1 hour rainfall = 1.350(In.)  
Computed rainfall intensity:  
Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
Slope used for rainfall intensity curve b = 0.6000  
Soil antecedent moisture condition (AMC) = 2

-----  
+++++  
Process from Point/Station 409.000 to Point/Station 410.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*  
-----

UNDEVELOPED (poor cover) subarea  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
SCS curve number for soil(AMC 2) = 78.00  
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404 (In/Hr)  
Initial subarea data:  
Initial area flow distance = 1000.000(Ft.)  
Top (of initial area) elevation = 1860.000(Ft.)  
Bottom (of initial area) elevation = 1460.000(Ft.)  
Difference in elevation = 400.000(Ft.)  
Slope = 0.40000 s(%)= 40.00  
TC = k(0.525)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 9.994 min.  
Rainfall intensity = 3.216(In/Hr) for a 25.0 year storm  
Effective runoff coefficient used for area (Q=KCIA) is C = 0.787  
Subarea runoff = 18.984(CFS)  
Total initial stream area = 7.500(Ac.)  
Pervious area fraction = 1.000  
Initial area Fm value = 0.404(In/Hr)

-----  
+++++  
Process from Point/Station 410.000 to Point/Station 411.000  
\*\*\*\* IRREGULAR CHANNEL FLOW TRAVEL TIME \*\*\*\*  
-----

-----  
Estimated mean flow rate at midpoint of channel = 42.397(CFS)  
Depth of flow = 0.229(Ft.), Average velocity = 9.149(Ft/s)  
\*\*\*\*\* Irregular Channel Data \*\*\*\*\*  
-----

```

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
    1              0.00              20.00
    2              20.00             0.00
    3              40.00             0.00
    4              60.00             20.00
Manning's 'N' friction factor = 0.035
-----

```

```

Sub-Channel flow = 42.397(CFS)
'   '   flow top width = 20.458(Ft.)
'   '   velocity= 9.149(Ft/s)
'   '   area = 4.634(Sq.Ft)
'   '   Froude number = 3.387

```

```

Upstream point elevation = 1460.000(Ft.)
Downstream point elevation = 1300.000(Ft.)
Flow length = 470.000(Ft.)
Travel time = 0.86 min.
Time of concentration = 10.85 min.
Depth of flow = 0.229(Ft.)
Average velocity = 9.149(Ft/s)
Total irregular channel flow = 42.397(CFS)
Irregular channel normal depth above invert elev. = 0.229(Ft.)
Average velocity of channel(s) = 9.149(Ft/s)

```

```

Sub-Channel No. 1 Critical depth = 0.516(Ft.)
'   '   '   Critical flow top width = 21.031(Ft.)
'   '   '   Critical flow velocity= 4.008(Ft/s)
'   '   '   Critical flow area = 10.578(Sq.Ft)

```

```

Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Rainfall intensity = 3.061(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method)(Q=KCIA) is C = 0.781
Subarea runoff = 43.205(CFS) for 18.500(Ac.)
Total runoff = 62.188(CFS)
Effective area this stream = 26.00(Ac.)
Total Study Area (Main Stream No. 1) = 26.00(Ac.)
Area averaged Fm value = 0.404(In/Hr)

```

```

+++++
Process from Point/Station 411.000 to Point/Station 412.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

```

```

-----
Estimated mean flow rate at midpoint of channel = 86.107(CFS)
Depth of flow = 0.421(Ft.), Average velocity = 10.005(Ft/s)
***** Irregular Channel Data *****
-----

```

```

Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
    1              0.00              20.00
    2              20.00             0.00

```

3	40.00	0.00
4	60.00	20.00

Manning's 'N' friction factor = 0.035

---

Sub-Channel flow = 86.107 (CFS)  
 ' ' flow top width = 20.843 (Ft.)  
 ' ' velocity = 10.005 (Ft/s)  
 ' ' area = 8.607 (Sq.Ft)  
 ' ' Froude number = 2.744

Upstream point elevation = 1300.000 (Ft.)  
 Downstream point elevation = 1180.000 (Ft.)  
 Flow length = 650.000 (Ft.)  
 Travel time = 1.08 min.  
 Time of concentration = 11.93 min.  
 Depth of flow = 0.421 (Ft.)  
 Average velocity = 10.005 (Ft/s)  
 Total irregular channel flow = 86.107 (CFS)  
 Irregular channel normal depth above invert elev. = 0.421 (Ft.)  
 Average velocity of channel(s) = 10.005 (Ft/s)

Sub-Channel No. 1 Critical depth = 0.820 (Ft.)  
 ' ' Critical flow top width = 21.641 (Ft.)  
 ' ' Critical flow velocity = 5.042 (Ft/s)  
 ' ' Critical flow area = 17.079 (Sq.Ft)

Adding area flow to channel  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404 (In/Hr)  
 Rainfall intensity = 2.891 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.774  
 Subarea runoff = 40.807 (CFS) for 20.000 (Ac.)  
 Total runoff = 102.995 (CFS)  
 Effective area this stream = 46.00 (Ac.)  
 Total Study Area (Main Stream No. 1) = 46.00 (Ac.)  
 Area averaged Fm value = 0.404 (In/Hr)

+++++  
 Process from Point/Station 412.000 to Point/Station 77.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1152.000 (Ft.)  
 Downstream point/station elevation = 1122.500 (Ft.)  
 Pipe length = 450.00 (Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 102.995 (CFS)  
 Given pipe size = 30.00 (In.)  
 Calculated individual pipe flow = 102.995 (CFS)  
 Normal flow depth in pipe = 24.09 (In.)  
 Flow top width inside pipe = 23.86 (In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 24.39 (Ft/s)  
 Travel time through pipe = 0.31 min.  
 Time of concentration (TC) = 12.24 min.

++++  
 Process from Point/Station 77.000 to Point/Station 77.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 46.000(Ac.)  
 Runoff from this stream = 102.995(CFS)  
 Time of concentration = 12.24 min.  
 Rainfall intensity = 2.848(In/Hr)  
 Area averaged loss rate (Fm) = 0.4035(In/Hr)  
 Area averaged Pervious ratio (Ap) = 1.0000

++++  
 Process from Point/Station 413.000 to Point/Station 414.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 500.000(Ft.)  
 Top (of initial area) elevation = 1163.300(Ft.)  
 Bottom (of initial area) elevation = 1129.000(Ft.)  
 Difference in elevation = 34.300(Ft.)  
 Slope = 0.06860 s(%)= 6.86  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 7.985 min.  
 Rainfall intensity = 3.679(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.810  
 Subarea runoff = 13.416(CFS)  
 Total initial stream area = 4.500(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

++++  
 Process from Point/Station 414.000 to Point/Station 414.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 4.500(Ac.)  
 Runoff from this stream = 13.416(CFS)  
 Time of concentration = 7.98 min.  
 Rainfall intensity = 3.679(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	102.995	12.24	2.848
2	13.416	7.98	3.679
Qmax(1) =			

	1.000 *	1.000 *	102.995) +	
	0.749 *	1.000 *	13.416) + =	113.041
Qmax(2) =	1.340 *	0.652 *	102.995) +	
	1.000 *	1.000 *	13.416) + =	103.473

Total of 2 streams to confluence:

Flow rates before confluence point:

102.995      13.416

Maximum flow rates at confluence using above data:

113.041      103.473

Area of streams before confluence:

46.000      4.500

Effective area values after confluence:

50.500      34.507

Results of confluence:

Total flow rate = 113.041(CFS)

Time of concentration = 12.241 min.

Effective stream area after confluence = 50.500(Ac.)

Stream Area average Pervious fraction(Ap) = 0.955

Stream Area average soil loss rate(Fm) = 0.400(In/Hr)

Study area (this main stream) = 50.50(Ac.)

+++++

Process from Point/Station      77.000 to Point/Station      78.000

\*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1122.500(Ft.)

Downstream point/station elevation = 1090.500(Ft.)

Pipe length = 550.00(Ft.)      Manning's N = 0.013

No. of pipes = 1      Required pipe flow = 113.041(CFS)

Given pipe size = 39.00(In.)

Calculated individual pipe flow = 113.041(CFS)

Normal flow depth in pipe = 21.05(In.)

Flow top width inside pipe = 38.88(In.)

Critical depth could not be calculated.

Pipe flow velocity = 24.77(Ft/s)

Travel time through pipe = 0.37 min.

Time of concentration (TC) = 12.61 min.

+++++

Process from Point/Station      78.000 to Point/Station      78.000

\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 50.500(Ac.)

Runoff from this stream = 113.041(CFS)

Time of concentration = 12.61 min.

Rainfall intensity = 2.797(In/Hr)

Area averaged loss rate (Fm) = 0.4003(In/Hr)

Area averaged Pervious ratio (Ap) = 0.9554

+++++

Process from Point/Station      415.000 to Point/Station      416.000

\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 550.000(Ft.)  
 Top (of initial area) elevation = 1129.000(Ft.)  
 Bottom (of initial area) elevation = 1097.000(Ft.)  
 Difference in elevation = 32.000(Ft.)  
 Slope = 0.05818 s(%)= 5.82  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 8.573 min.  
 Rainfall intensity = 3.526(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.806  
 Subarea runoff = 19.901(CFS)  
 Total initial stream area = 7.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

++++++  
 Process from Point/Station      416.000 to Point/Station      416.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 7.000(Ac.)  
 Runoff from this stream = 19.901(CFS)  
 Time of concentration = 8.57 min.  
 Rainfall intensity = 3.526(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000

++++++  
 Process from Point/Station      417.000 to Point/Station      418.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000      Max loss rate(Fm)=      0.404(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 650.000(Ft.)  
 Top (of initial area) elevation = 1420.000(Ft.)  
 Bottom (of initial area) elevation = 1120.000(Ft.)  
 Difference in elevation = 300.000(Ft.)  
 Slope = 0.46154 s(%)= 46.15  
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 8.175 min.  
 Rainfall intensity = 3.628(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.800  
 Subarea runoff = 29.020(CFS)  
 Total initial stream area = 10.000(Ac.)  
 Pervious area fraction = 1.000  
 Initial area Fm value = 0.404(In/Hr)

++++  
 Process from Point/Station 418.000 to Point/Station 418.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
 Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 10.000(Ac.)  
 Runoff from this stream = 29.020(CFS)  
 Time of concentration = 8.17 min.  
 Rainfall intensity = 3.628(In/Hr)  
 Area averaged loss rate (Fm) = 0.4035(In/Hr)  
 Area averaged Pervious ratio (Ap) = 1.0000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	113.041	12.61	2.797
2	19.901	8.57	3.526
3	29.020	8.17	3.628
Qmax(1) =			
	1.000 *	1.000 *	113.041) +
	0.769 *	1.000 *	19.901) +
	0.742 *	1.000 *	29.020) + = 149.893
Qmax(2) =			
	1.304 *	0.680 *	113.041) +
	1.000 *	1.000 *	19.901) +
	0.968 *	1.000 *	29.020) + = 148.217
Qmax(3) =			
	1.347 *	0.648 *	113.041) +
	1.032 *	0.954 *	19.901) +
	1.000 *	1.000 *	29.020) + = 147.290

Total of 3 streams to confluence:  
 Flow rates before confluence point:  
 113.041 19.901 29.020  
 Maximum flow rates at confluence using above data:  
 149.893 148.217 147.290  
 Area of streams before confluence:  
 50.500 7.000 10.000  
 Effective area values after confluence:  
 67.500 51.331 49.411  
 Results of confluence:  
 Total flow rate = 149.893(CFS)  
 Time of concentration = 12.611 min.  
 Effective stream area after confluence = 67.500(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.915  
 Stream Area average soil loss rate(Fm) = 0.397(In/Hr)  
 Study area (this main stream) = 67.50(Ac.)

++++  
 Process from Point/Station 78.000 to Point/Station 79.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

-----  
 Upstream point/station elevation = 1090.500(Ft.)  
 Downstream point/station elevation = 1060.200(Ft.)  
 Pipe length = 900.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 149.893(CFS)  
 Given pipe size = 48.00(In.)  
 Calculated individual pipe flow = 149.893(CFS)

Normal flow depth in pipe = 25.92(In.)  
 Flow top width inside pipe = 47.85(In.)  
 Critical Depth = 43.16(In.)  
 Pipe flow velocity = 21.64(Ft/s)  
 Travel time through pipe = 0.69 min.  
 Time of concentration (TC) = 13.30 min.

++++  
 Process from Point/Station 79.000 to Point/Station 79.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 67.500(Ac.)  
 Runoff from this stream = 149.893(CFS)  
 Time of concentration = 13.30 min.  
 Rainfall intensity = 2.709(In/Hr)  
 Area averaged loss rate (Fm) = 0.3973(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.9148

++++  
 Process from Point/Station 400.000 to Point/Station 420.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1850.000(Ft.)  
 Bottom (of initial area) elevation = 1320.000(Ft.)  
 Difference in elevation = 530.000(Ft.)  
 Slope = 0.53000 s(%)= 53.00  
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 9.447 min.  
 Rainfall intensity = 3.326(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.791  
 Subarea runoff = 24.990(CFS)  
 Total initial stream area = 9.500(Ac.)  
 Pervious area fraction = 1.000  
 Initial area Fm value = 0.404(In/Hr)

++++  
 Process from Point/Station 420.000 to Point/Station 421.000  
 \*\*\*\* IRREGULAR CHANNEL FLOW TRAVEL TIME \*\*\*\*

---

Estimated mean flow rate at midpoint of channel = 37.485(CFS)  
 Depth of flow = 0.883(Ft.), Average velocity = 12.826(Ft/s)  
 \*\*\*\*\* Irregular Channel Data \*\*\*\*\*

---

Information entered for subchannel number 1 :  

Point number	'X' coordinate	'Y' coordinate
1	0.00	20.00
2	100.00	0.00
3	150.00	20.00

Manning's 'N' friction factor = 0.035

```

-----
Sub-Channel flow = 37.485(CFS)
'   '   flow top width = 6.621(Ft.)
'   '   velocity= 12.826(Ft/s)
'   '   area = 2.923(Sq.Ft)
'   '   Froude number = 3.402

```

```

Upstream point elevation = 1320.000(Ft.)
Downstream point elevation = 1140.000(Ft.)
Flow length = 630.000(Ft.)
Travel time = 0.82 min.
Time of concentration = 10.27 min.
Depth of flow = 0.883(Ft.)
Average velocity = 12.826(Ft/s)
Total irregular channel flow = 37.485(CFS)
Irregular channel normal depth above invert elev. = 0.883(Ft.)
Average velocity of channel(s) = 12.826(Ft/s)

```

```

Sub-Channel No. 1 Critical depth = 1.438(Ft.)
'   '   '   Critical flow top width = 10.781(Ft.)
'   '   '   Critical flow velocity= 4.837(Ft/s)
'   '   '   Critical flow area = 7.749(Sq.Ft)

```

```

Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Rainfall intensity = 3.165(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method)(Q=KCIA) is C = 0.785
Subarea runoff = 22.224(CFS) for 9.500(Ac.)
Total runoff = 47.214(CFS)
Effective area this stream = 19.00(Ac.)
Total Study Area (Main Stream No. 1) = 86.50(Ac.)
Area averaged Fm value = 0.404(In/Hr)

```

```

+++++
Process from Point/Station 421.000 to Point/Station 422.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

```

```

-----
Estimated mean flow rate at midpoint of channel = 63.366(CFS)
Depth of flow = 1.089(Ft.), Average velocity = 8.545(Ft/s)
***** Irregular Channel Data *****

```

```

-----
Information entered for subchannel number 1 :
Point number   'X' coordinate   'Y' coordinate
1              0.00             20.00
2             100.00             0.00
3             250.00             20.00
Manning's 'N' friction factor = 0.035

```

```

-----
Sub-Channel flow = 63.366(CFS)
'   '   flow top width = 13.616(Ft.)
'   '   velocity= 8.545(Ft/s)
'   '   area = 7.416(Sq.Ft)

```

Froude number = 2.040  
 Upstream point elevation = 1140.000(Ft.)  
 Downstream point elevation = 1064.000(Ft.)  
 Flow length = 820.000(Ft.)  
 Travel time = 1.60 min.  
 Time of concentration = 11.87 min.  
 Depth of flow = 1.089(Ft.)  
 Average velocity = 8.545(Ft/s)  
 Total irregular channel flow = 63.366(CFS)  
 Irregular channel normal depth above invert elev. = 1.089(Ft.)  
 Average velocity of channel(s) = 8.545(Ft/s)

Sub-Channel No. 1 Critical depth = 1.453(Ft.)  
 Critical flow top width = 18.164(Ft.)  
 Critical flow velocity = 4.801(Ft/s)  
 Critical flow area = 13.197(Sq.Ft)

Adding area flow to channel  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404(In/Hr)  
 Rainfall intensity = 2.901(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.775  
 Subarea runoff = 24.721(CFS) for 13.000(Ac.)  
 Total runoff = 71.935(CFS)  
 Effective area this stream = 32.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 99.50(Ac.)  
 Area averaged Fm value = 0.404(In/Hr)

++++++  
 Process from Point/Station 422.000 to Point/Station 422.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 32.000(Ac.)  
 Runoff from this stream = 71.935(CFS)  
 Time of concentration = 11.87 min.  
 Rainfall intensity = 2.901(In/Hr)  
 Area averaged loss rate (Fm) = 0.4035(In/Hr)  
 Area averaged Pervious ratio (Ap) = 1.0000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	149.893	13.30	2.709
2	71.935	11.87	2.901
Qmax(1) =	1.000 * 149.893 +	1.000 * 71.935 +	216.282
	0.923 * 149.893 +	1.000 * 71.935 +	
Qmax(2) =	1.083 * 149.893 +	1.000 * 71.935 +	216.754
	1.000 * 149.893 +	1.000 * 71.935 +	

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
     149.893          71.935  
 Maximum flow rates at confluence using above data:  
     216.282          216.754  
 Area of streams before confluence:  
     67.500          32.000  
 Effective area values after confluence:  
     99.500          92.201  
 Results of confluence:  
 Total flow rate = 216.754(CFS)  
 Time of concentration = 11.865 min.  
 Effective stream area after confluence = 92.201(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.942  
 Stream Area average soil loss rate(Fm) = 0.399(In/Hr)  
 Study area (this main stream) = 99.50(Ac.)

+++++  
 Process from Point/Station          79.000 to Point/Station          80.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1052.000(Ft.)  
 Downstream point/station elevation = 1040.200(Ft.)  
 Pipe length = 440.00(Ft.)      Manning's N = 0.013  
 No. of pipes = 1      Required pipe flow = 216.754(CFS)  
 Given pipe size = 54.00(In.)  
 Calculated individual pipe flow = 216.754(CFS)  
 Normal flow depth in pipe = 32.44(In.)  
 Flow top width inside pipe = 52.89(In.)  
 Critical Depth = 49.65(In.)  
 Pipe flow velocity = 21.72(Ft/s)  
 Travel time through pipe = 0.34 min.  
 Time of concentration (TC) = 12.20 min.

+++++  
 Process from Point/Station          80.000 to Point/Station          80.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 92.201(Ac.)  
 Runoff from this stream = 216.754(CFS)  
 Time of concentration = 12.20 min.  
 Rainfall intensity = 2.853(In/Hr)  
 Area averaged loss rate (Fm) = 0.3993(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.9422

+++++  
 Process from Point/Station          423.000 to Point/Station          424.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)= 0.367(In/Hr)

## Initial subarea data:

Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1102.500(Ft.)  
 Bottom (of initial area) elevation = 1060.500(Ft.)  
 Difference in elevation = 42.000(Ft.)  
 Slope = 0.04200 s(%) = 4.20  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 11.623 min.  
 Rainfall intensity = 2.937(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.788  
 Subarea runoff = 20.821(CFS)  
 Total initial stream area = 9.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

++++++  
 Process from Point/Station 424.000 to Point/Station 425.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1060.500(Ft.)  
 End of street segment elevation = 1049.000(Ft.)  
 Length of street segment = 800.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 38.172(CFS)  
 Depth of flow = 0.514(Ft.), Average velocity = 4.288(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 4.29(Ft/s)  
 Travel time = 3.11 min. TC = 14.73 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367(In/Hr)  
 Rainfall intensity = 2.548(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.770  
 Subarea runoff = 26.288(CFS) for 15.000(Ac.)  
 Total runoff = 47.109(CFS)  
 Effective area this stream = 24.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 123.50(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 47.109(CFS)  
 Half street flow at end of street = 23.555(CFS)

Depth of flow = 0.544(Ft.), Average velocity = 4.661(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++  
 Process from Point/Station 425.000 to Point/Station 425.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 24.000(Ac.)  
 Runoff from this stream = 47.109(CFS)  
 Time of concentration = 14.73 min.  
 Rainfall intensity = 2.548(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	216.754	12.20	2.853
2	47.109	14.73	2.548
Qmax(1) =	1.000 * 216.754) +	1.000 * 47.109) + =	261.229
Qmax(2) =	0.876 * 216.754) +	1.000 * 47.109) + =	236.929

Total of 2 streams to confluence:

Flow rates before confluence point:  
 216.754 47.109

Maximum flow rates at confluence using above data:  
 261.229 236.929

Area of streams before confluence:  
 92.201 24.000

Effective area values after confluence:  
 112.080 116.201

Results of confluence:

Total flow rate = 261.229(CFS)

Time of concentration = 12.203 min.

Effective stream area after confluence = 112.080(Ac.)

Stream Area average Pervious fraction(Ap) = 0.851

Stream Area average soil loss rate(Fm) = 0.393(In/Hr)

Study area (this main stream) = 116.20(Ac.)

End of computations, Total Study Area = 123.50 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.856

Area averaged SCS curve number = 71.7

LINE "P2"

## San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
 Rational Hydrology Study Date: 01/13/05

FONTANA / LINE P2 HYDROLOGY  
 25 YEAR STORM  
 JN 04339

Hall & Forman, Inc. - S/N 950

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

Rational hydrology study storm event year is 25.0  
 10 Year storm 1 hour rainfall = 0.930(In.)  
 100 Year storm 1 hour rainfall = 1.350(In.)  
 Computed rainfall intensity:  
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
 Slope used for rainfall intensity curve b = 0.6000  
 Soil antecedent moisture condition (AMC) = 2

\*\*\*\*\*  
 Process from Point/Station 500.000 to Point/Station 501.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1620.000(Ft.)  
 Bottom (of initial area) elevation = 1350.000(Ft.)  
 Difference in elevation = 270.000(Ft.)  
 Slope = 0.27000 s(%)= 27.00  
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 10.812 min.  
 Rainfall intensity = 3.068(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.782  
 Subarea runoff = 14.387(CFS)  
 Total initial stream area = 6.000(Ac.)  
 Pervious area fraction = 1.000  
 Initial area Fm value = 0.404(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 501.000 to Point/Station 502.000  
 \*\*\*\* IRREGULAR CHANNEL FLOW TRAVEL TIME \*\*\*\*

Estimated mean flow rate at midpoint of channel = 25.177(CFS)  
 Depth of flow = 0.658(Ft.), Average velocity = 11.641(Ft/s)  
 \*\*\*\*\* Irregular Channel Data \*\*\*\*\*

-----  
 Information entered for subchannel number 1 :  
 Point number        'X' coordinate        'Y' coordinate  
                   1                    0.00                    20.00  
                   2                    100.00                   0.00  
                   3                    200.00                   20.00  
 Manning's 'N' friction factor =    0.035  
 -----

Sub-Channel flow =        25.177(CFS)  
 '                    flow top width =        6.577(Ft.)  
 '                    velocity=        11.641(Ft/s)  
 '                    area =        2.163(Sq.Ft)  
 '                    Froude number =        3.578

Upstream point elevation = 1350.000(Ft.)  
 Downstream point elevation = 1180.000(Ft.)  
 Flow length = 500.000(Ft.)  
 Travel time = 0.72 min.  
 Time of concentration = 11.53 min.  
 Depth of flow = 0.658(Ft.)  
 Average velocity = 11.641(Ft/s)  
 Total irregular channel flow = 25.177(CFS)  
 Irregular channel normal depth above invert elev. = 0.658(Ft.)  
 Average velocity of channel(s) = 11.641(Ft/s)

Sub-Channel No. 1 Critical depth =        1.094(Ft.)  
 '                    '                    Critical flow top width =        10.938(Ft.)  
 '                    '                    Critical flow velocity=        4.209(Ft/s)  
 '                    '                    Critical flow area =        5.981(Sq.Ft)

Adding area flow to channel  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000        Max loss rate(Fm)=        0.404(In/Hr)  
 Rainfall intensity =        2.952(In/Hr) for a        25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.777  
 Subarea runoff =        20.017(CFS) for        9.000(Ac.)  
 Total runoff =        34.404(CFS)  
 Effective area this stream =        15.00(Ac.)  
 Total Study Area (Main Stream No. 1) =        15.00(Ac.)  
 Area averaged Fm value =        0.404(In/Hr)

+++++  
 Process from Point/Station        502.000 to Point/Station        83.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1167.600(Ft.)  
 Downstream point/station elevation = 1126.000(Ft.)  
 Pipe length = 660.00(Ft.)        Manning's N = 0.013  
 No. of pipes = 1        Required pipe flow =        34.404(CFS)  
 Given pipe size =        24.00(In.)  
 Calculated individual pipe flow =        34.404(CFS)  
 Normal flow depth in pipe =        13.48(In.)  
 Flow top width inside pipe =        23.82(In.)  
 Critical depth could not be calculated.

Pipe flow velocity = 18.94 (Ft/s)  
 Travel time through pipe = 0.58 min.  
 Time of concentration (TC) = 12.11 min.

++++  
 Process from Point/Station 83.000 to Point/Station 83.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
 Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 15.000 (Ac.)  
 Runoff from this stream = 34.404 (CFS)  
 Time of concentration = 12.11 min.  
 Rainfall intensity = 2.866 (In/Hr)  
 Area averaged loss rate (Fm) = 0.4035 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 1.0000

++++  
 Process from Point/Station 503.000 to Point/Station 504.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

-----  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 78.00  
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000 (Ft.)  
 Top (of initial area) elevation = 1520.000 (Ft.)  
 Bottom (of initial area) elevation = 1180.000 (Ft.)  
 Difference in elevation = 340.000 (Ft.)  
 Slope = 0.34000 s(%) = 34.00  
 $TC = k(0.525) * [(length^3) / (elevation\ change)]^{0.2}$   
 Initial area time of concentration = 10.324 min.  
 Rainfall intensity = 3.154 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.785  
 Subarea runoff = 24.752 (CFS)  
 Total initial stream area = 10.000 (Ac.)  
 Pervious area fraction = 1.000  
 Initial area Fm value = 0.404 (In/Hr)

++++  
 Process from Point/Station 504.000 to Point/Station 505.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

-----  
 Top of street segment elevation = 1167.600 (Ft.)  
 End of street segment elevation = 1126.000 (Ft.)  
 Length of street segment = 660.000 (Ft.)  
 Height of curb above gutter flowline = 8.0 (In.)  
 Width of half street (curb to crown) = 20.000 (Ft.)  
 Distance from crown to crossfall grade break = 18.500 (Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000 (Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500 (Ft.)

Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 27.228(CFS)  
 Depth of flow = 0.374(Ft.), Average velocity = 6.735(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 13.965(Ft.)  
 Flow velocity = 6.73(Ft/s)  
 Travel time = 1.63 min. TC = 11.96 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 2.888(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.776  
 Subarea runoff = 2.143(CFS) for 2.000(Ac.)  
 Total runoff = 26.896(CFS)  
 Effective area this stream = 12.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 27.00(Ac.)  
 Area averaged Fm value = 0.397(In/Hr)  
 Street flow at end of street = 26.896(CFS)  
 Half street flow at end of street = 13.448(CFS)  
 Depth of flow = 0.373(Ft.), Average velocity = 6.714(Ft/s)  
 Flow width (from curb towards crown)= 13.898(Ft.)

+++++  
 Process from Point/Station 505.000 to Point/Station 505.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 12.000(Ac.)  
 Runoff from this stream = 26.896(CFS)  
 Time of concentration = 11.96 min.  
 Rainfall intensity = 2.888(In/Hr)  
 Area averaged loss rate (Fm) = 0.3974(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.9167  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	34.404	12.11	2.866
2	26.896	11.96	2.888
Qmax(1) =			
	1.000 *	1.000 *	34.404) +
	0.991 *	1.000 *	26.896) + = 61.067
Qmax(2) =			
	1.009 *	0.988 *	34.404) +
	1.000 *	1.000 *	26.896) + = 61.170

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 34.404 26.896

Maximum flow rates at confluence using above data:

61.067 61.170  
Area of streams before confluence:  
15.000 12.000  
Effective area values after confluence:  
27.000 26.814

Results of confluence:

Total flow rate = 61.170 (CFS)  
Time of concentration = 11.958 min.  
Effective stream area after confluence = 26.814 (Ac.)  
Stream Area average Pervious fraction (Ap) = 0.963  
Stream Area average soil loss rate (Fm) = 0.401 (In/Hr)  
Study area (this main stream) = 27.00 (Ac.)

\*\*\*\*\*  
Process from Point/Station 83.000 to Point/Station 85.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1126.000 (Ft.)  
Downstream point/station elevation = 1092.300 (Ft.)  
Pipe length = 450.00 (Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 61.170 (CFS)  
Given pipe size = 36.00 (In.)  
Calculated individual pipe flow = 61.170 (CFS)  
Normal flow depth in pipe = 14.36 (In.)  
Flow top width inside pipe = 35.25 (In.)  
Critical Depth = 30.26 (In.)  
Pipe flow velocity = 23.26 (Ft/s)  
Travel time through pipe = 0.32 min.  
Time of concentration (TC) = 12.28 min.

\*\*\*\*\*  
Process from Point/Station 85.000 to Point/Station 85.000  
\*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 1  
Effective stream flow area = 26.814 (Ac.)  
Total study area this main stream = 27.000 (Ac.)  
Runoff from this stream = 61.170 (CFS)  
Time of concentration = 12.28 min.  
Rainfall intensity = 2.842 (In/Hr)  
Area averaged loss rate (Fm) = 0.4008 (In/Hr)  
Area averaged Pervious ratio (Ap) = 0.9630  
Program is now starting with Main Stream No. 2

\*\*\*\*\*  
Process from Point/Station 506.000 to Point/Station 507.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

UNDEVELOPED (poor cover) subarea  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
SCS curve number for soil (AMC 2) = 78.00  
Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)  
Initial subarea data:

Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 2040.000(Ft.)  
 Bottom (of initial area) elevation = 1680.000(Ft.)  
 Difference in elevation = 360.000(Ft.)  
 Slope = 0.36000 s(%) = 36.00  
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 10.207 min.  
 Rainfall intensity = 3.175(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.786  
 Subarea runoff = 19.958(CFS)  
 Total initial stream area = 8.000(Ac.)  
 Pervious area fraction = 1.000  
 Initial area Fm value = 0.404(In/Hr)

++++++  
 Process from Point/Station 507.000 to Point/Station 508.000  
 \*\*\*\* IRREGULAR CHANNEL FLOW TRAVEL TIME \*\*\*\*

-----  
 Estimated mean flow rate at midpoint of channel = 34.927(CFS)  
 Depth of flow = 0.950(Ft.), Average velocity = 15.488(Ft/s)  
 \*\*\*\*\* Irregular Channel Data \*\*\*\*\*

-----  
 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	20.00
2	50.00	0.00
3	100.00	20.00

Manning's 'N' friction factor = 0.035

-----  
 Sub-Channel flow = 34.927(CFS)  
 ' ' flow top width = 4.749(Ft.)  
 ' ' velocity = 15.488(Ft/s)  
 ' ' area = 2.255(Sq.Ft)  
 ' ' Froude number = 3.961

Upstream point elevation = 1680.000(Ft.)  
 Downstream point elevation = 1450.000(Ft.)  
 Flow length = 580.000(Ft.)  
 Travel time = 0.62 min.  
 Time of concentration = 10.83 min.  
 Depth of flow = 0.950(Ft.)  
 Average velocity = 15.488(Ft/s)  
 Total irregular channel flow = 34.927(CFS)  
 Irregular channel normal depth above invert elev. = 0.950(Ft.)  
 Average velocity of channel(s) = 15.488(Ft/s)

Sub-Channel No. 1 Critical depth = 1.641(Ft.)  
 ' ' ' Critical flow top width = 8.203(Ft.)  
 ' ' ' Critical flow velocity = 5.190(Ft/s)  
 ' ' ' Critical flow area = 6.729(Sq.Ft)

Adding area flow to channel  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404(In/Hr)  
 Rainfall intensity = 3.064(In/Hr) for a 25.0 year storm

Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.781  
 Subarea runoff = 27.938 (CFS) for 12.000 (Ac.)  
 Total runoff = 47.896 (CFS)  
 Effective area this stream = 20.00 (Ac.)  
 Total Study Area (Main Stream No. 2) = 20.00 (Ac.)  
 Area averaged Fm value = 0.404 (In/Hr)

+++++  
 Process from Point/Station 508.000 to Point/Station 509.000  
 \*\*\*\* IRREGULAR CHANNEL FLOW TRAVEL TIME \*\*\*\*

-----  
 Estimated mean flow rate at midpoint of channel = 80.825 (CFS)  
 Depth of flow = 1.362 (Ft.), Average velocity = 17.418 (Ft/s)  
 \*\*\*\*\* Irregular Channel Data \*\*\*\*\*

-----  
 Information entered for subchannel number 1 :  
 Point number 'X' coordinate 'Y' coordinate  
 1 0.00 20.00  
 2 50.00 0.00  
 3 100.00 20.00  
 Manning's 'N' friction factor = 0.035  
 -----

Sub-Channel flow = 80.825 (CFS)  
 ' ' flow top width = 6.812 (Ft.)  
 ' ' velocity = 17.418 (Ft/s)  
 ' ' area = 4.640 (Sq.Ft)  
 ' ' Froude number = 3.719

Upstream point elevation = 1450.000 (Ft.)  
 Downstream point elevation = 1140.000 (Ft.)  
 Flow length = 1000.000 (Ft.)  
 Travel time = 0.96 min.  
 Time of concentration = 11.79 min.  
 Depth of flow = 1.362 (Ft.)  
 Average velocity = 17.418 (Ft/s)  
 Total irregular channel flow = 80.825 (CFS)  
 Irregular channel normal depth above invert elev. = 1.362 (Ft.)  
 Average velocity of channel(s) = 17.418 (Ft/s)

Sub-Channel No. 1 Critical depth = 2.313 (Ft.)  
 ' ' ' Critical flow top width = 11.563 (Ft.)  
 ' ' ' Critical flow velocity = 6.046 (Ft/s)  
 ' ' ' Critical flow area = 13.369 (Sq.Ft)

Adding area flow to channel  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 78.00  
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)  
 Rainfall intensity = 2.913 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.775  
 Subarea runoff = 59.369 (CFS) for 27.500 (Ac.)  
 Total runoff = 107.265 (CFS)  
 Effective area this stream = 47.50 (Ac.)  
 Total Study Area (Main Stream No. 2) = 47.50 (Ac.)

Area averaged Fm value = 0.404(In/Hr)

+++++  
 Process from Point/Station 509.000 to Point/Station 509.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 2 in normal stream number 1  
 Stream flow area = 47.500(Ac.)  
 Runoff from this stream = 107.265(CFS)  
 Time of concentration = 11.79 min.  
 Rainfall intensity = 2.913(In/Hr)  
 Area averaged loss rate (Fm) = 0.4035(In/Hr)  
 Area averaged Pervious ratio (Ap) = 1.0000

+++++  
 Process from Point/Station 510.000 to Point/Station 511.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1560.000(Ft.)  
 Bottom (of initial area) elevation = 1180.000(Ft.)  
 Difference in elevation = 380.000(Ft.)  
 Slope = 0.38000 s(%)= 38.00  
 $TC = k(0.525) * [(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 10.097 min.  
 Rainfall intensity = 3.196(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.786  
 Subarea runoff = 23.877(CFS)  
 Total initial stream area = 9.500(Ac.)  
 Pervious area fraction = 1.000  
 Initial area Fm value = 0.404(In/Hr)

+++++  
 Process from Point/Station 511.000 to Point/Station 512.000  
 \*\*\*\* IMPROVED CHANNEL TRAVEL TIME \*\*\*\*

---

Upstream point elevation = 1180.000(Ft.)  
 Downstream point elevation = 1140.000(Ft.)  
 Channel length thru subarea = 530.000(Ft.)  
 Channel base width = 0.000(Ft.)  
 Slope or 'Z' of left channel bank = 1.500  
 Slope or 'Z' of right channel bank = 1.500  
 Estimated mean flow rate at midpoint of channel = 54.666(CFS)  
 Manning's 'N' = 0.015  
 Maximum depth of channel = 2.000(Ft.)  
 Flow(q) thru subarea = 54.666(CFS)  
 Depth of flow = 1.389(Ft.), Average velocity = 18.883(Ft/s)  
 Channel flow top width = 4.168(Ft.)  
 Flow Velocity = 18.88(Ft/s)  
 Travel time = 0.47 min.

Time of concentration = 10.57 min.  
 Critical depth = 2.375 (Ft.)  
 Adding area flow to channel  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 78.00  
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)  
 Rainfall intensity = 3.110 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.783  
 Subarea runoff = 58.956 (CFS) for 24.500 (Ac.)  
 Total runoff = 82.833 (CFS)  
 Effective area this stream = 34.00 (Ac.)  
 Total Study Area (Main Stream No. 2) = 81.50 (Ac.)  
 Area averaged Fm value = 0.404 (In/Hr)

++++++  
 Process from Point/Station 512.000 to Point/Station 512.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2

Stream flow area = 34.000 (Ac.)  
 Runoff from this stream = 82.833 (CFS)  
 Time of concentration = 10.57 min.  
 Rainfall intensity = 3.110 (In/Hr)  
 Area averaged loss rate (Fm) = 0.4035 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 1.0000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	107.265	11.79	2.913
2	82.833	10.57	3.110
Qmax(1) =			
	1.000 *	1.000 *	107.265) +
	0.927 *	1.000 *	82.833) + = 184.044
Qmax(2) =			
	1.079 *	0.896 *	107.265) +
	1.000 *	1.000 *	82.833) + = 186.550

Total of 2 streams to confluence:

Flow rates before confluence point:

107.265      82.833

Maximum flow rates at confluence using above data:

184.044      186.550

Area of streams before confluence:

47.500      34.000

Effective area values after confluence:

81.500      76.572

Results of confluence:

Total flow rate = 186.550 (CFS)

Time of concentration = 10.565 min.

Effective stream area after confluence = 76.572 (Ac.)

Stream Area average Pervious fraction (Ap) = 1.000

Stream Area average soil loss rate (Fm) = 0.404 (In/Hr)

Study area (this main stream) = 81.50 (Ac.)

+++++  
Process from Point/Station 512.000 to Point/Station 84.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

-----  
Upstream point/station elevation = 1137.500 (Ft.)  
Downstream point/station elevation = 1110.000 (Ft.)  
Pipe length = 450.00 (Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 186.550 (CFS)  
Given pipe size = 30.00 (In.)  
NOTE: Normal flow is pressure flow in user selected pipe size.  
The approximate hydraulic grade line above the pipe invert is  
99.193 (Ft.) at the headworks or inlet of the pipe(s)  
Pipe friction loss = 93.053 (Ft.)  
Minor friction loss = 33.640 (Ft.) K-factor = 1.50  
Pipe flow velocity = 38.00 (Ft/s)  
Travel time through pipe = 0.20 min.  
Time of concentration (TC) = 10.76 min.

+++++  
Process from Point/Station 84.000 to Point/Station 84.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
Along Main Stream number: 2 in normal stream number 1  
Stream flow area = 76.572 (Ac.)  
Runoff from this stream = 186.550 (CFS)  
Time of concentration = 10.76 min.  
Rainfall intensity = 3.076 (In/Hr)  
Area averaged loss rate (Fm) = 0.4035 (In/Hr)  
Area averaged Pervious ratio (Ap) = 1.0000

+++++  
Process from Point/Station 513.000 to Point/Station 514.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

-----  
UNDEVELOPED (poor cover) subarea  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
SCS curve number for soil (AMC 2) = 78.00  
Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)  
Initial subarea data:  
Initial area flow distance = 1000.000 (Ft.)  
Top (of initial area) elevation = 1770.000 (Ft.)  
Bottom (of initial area) elevation = 1460.000 (Ft.)  
Difference in elevation = 310.000 (Ft.)  
Slope = 0.31000 s(%) = 31.00  
TC = k(0.525)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 10.517 min.  
Rainfall intensity = 3.119 (In/Hr) for a 25.0 year storm  
Effective runoff coefficient used for area (Q=KCIA) is C = 0.784  
Subarea runoff = 17.108 (CFS)  
Total initial stream area = 7.000 (Ac.)  
Pervious area fraction = 1.000  
Initial area Fm value = 0.404 (In/Hr)

++++  
 Process from Point/Station 514.000 to Point/Station 515.000  
 \*\*\*\* IRREGULAR CHANNEL FLOW TRAVEL TIME \*\*\*\*

-----  
 Estimated mean flow rate at midpoint of channel = 25.662 (CFS)  
 Depth of flow = 0.584 (Ft.), Average velocity = 10.023 (Ft/s)  
 \*\*\*\*\* Irregular Channel Data \*\*\*\*\*

-----  
 Information entered for subchannel number 1 :  
 Point number 'X' coordinate 'Y' coordinate  
 1 0.00 20.00  
 2 150.00 0.00  
 3 300.00 20.00  
 Manning's 'N' friction factor = 0.035

-----  
 Sub-Channel flow = 25.662 (CFS)  
 ' ' flow top width = 8.764 (Ft.)  
 ' ' velocity = 10.023 (Ft/s)  
 ' ' area = 2.560 (Sq.Ft)  
 ' ' Froude number = 3.268

Upstream point elevation = 1460.000 (Ft.)  
 Downstream point elevation = 1140.000 (Ft.)  
 Flow length = 1100.000 (Ft.)  
 Travel time = 1.83 min.  
 Time of concentration = 12.35 min.  
 Depth of flow = 0.584 (Ft.)  
 Average velocity = 10.023 (Ft/s)  
 Total irregular channel flow = 25.662 (CFS)  
 Irregular channel normal depth above invert elev. = 0.584 (Ft.)  
 Average velocity of channel (s) = 10.023 (Ft/s)

Sub-Channel No. 1 Critical depth = 0.938 (Ft.)  
 ' ' ' Critical flow top width = 14.063 (Ft.)  
 ' ' ' Critical flow velocity = 3.893 (Ft/s)  
 ' ' ' Critical flow area = 6.592 (Sq.Ft)

Adding area flow to channel  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 78.00  
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)  
 Rainfall intensity = 2.833 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.772  
 Subarea runoff = 13.503 (CFS) for 7.000 (Ac.)  
 Total runoff = 30.611 (CFS)  
 Effective area this stream = 14.00 (Ac.)  
 Total Study Area (Main Stream No. 2) = 95.50 (Ac.)  
 Area averaged Fm value = 0.404 (In/Hr)

++++  
 Process from Point/Station 515.000 to Point/Station 84.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

-----  
 Upstream point/station elevation = 1119.100 (Ft.)

Downstream point/station elevation = 1111.400(Ft.)  
 Pipe length = 280.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 30.611(CFS)  
 Given pipe size = 18.00(In.)  
 NOTE: Normal flow is pressure flow in user selected pipe size.  
 The approximate hydraulic grade line above the pipe invert is  
 23.058(Ft.) at the headworks or inlet of the pipe(s)  
 Pipe friction loss = 23.769(Ft.)  
 Minor friction loss = 6.989(Ft.) K-factor = 1.50  
 Pipe flow velocity = 17.32(Ft/s)  
 Travel time through pipe = 0.27 min.  
 Time of concentration (TC) = 12.62 min.

\*\*\*\*\*  
 Process from Point/Station 84.000 to Point/Station 84.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 2 in normal stream number 2  
 Stream flow area = 14.000(Ac.)  
 Runoff from this stream = 30.611(CFS)  
 Time of concentration = 12.62 min.  
 Rainfall intensity = 2.796(In/Hr)  
 Area averaged loss rate (Fm) = 0.4035(In/Hr)  
 Area averaged Pervious ratio (Ap) = 1.0000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	186.550	10.76	3.076
2	30.611	12.62	2.796
Qmax(1) =			
	1.000 *	1.000 *	186.550) +
	1.117 *	0.853 *	30.611) + = 215.717
Qmax(2) =			
	0.895 *	1.000 *	186.550) +
	1.000 *	1.000 *	30.611) + = 197.640

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 186.550 30.611  
 Maximum flow rates at confluence using above data:  
 215.717 197.640  
 Area of streams before confluence:  
 76.572 14.000  
 Effective area values after confluence:  
 88.515 90.572  
 Results of confluence:  
 Total flow rate = 215.717(CFS)  
 Time of concentration = 10.762 min.  
 Effective stream area after confluence = 88.515(Ac.)  
 Stream Area average Pervious fraction(Ap) = 1.000  
 Stream Area average soil loss rate(Fm) = 0.404(In/Hr)  
 Study area (this main stream) = 90.57(Ac.)

\*\*\*\*\*  
 Process from Point/Station 84.000 to Point/Station 85.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1110.700(Ft.)  
 Downstream point/station elevation = 1092.300(Ft.)  
 Pipe length = 600.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 215.717(CFS)  
 Given pipe size = 30.00(In.)  
 NOTE: Normal flow is pressure flow in user selected pipe size.  
 The approximate hydraulic grade line above the pipe invert is  
 192.481(Ft.) at the headworks or inlet of the pipe(s)  
 Pipe friction loss = 165.899(Ft.)  
 Minor friction loss = 44.981(Ft.) K-factor = 1.50  
 Pipe flow velocity = 43.95(Ft/s)  
 Travel time through pipe = 0.23 min.  
 Time of concentration (TC) = 10.99 min.

++++++  
 Process from Point/Station 85.000 to Point/Station 85.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

---

The following data inside Main Stream is listed:

In Main Stream number: 2  
 Effective stream flow area = 88.515(Ac.)  
 Total study area this main stream = 95.500(Ac.)  
 Runoff from this stream = 215.717(CFS)  
 Time of concentration = 10.99 min.  
 Rainfall intensity = 3.038(In/Hr)  
 Area averaged loss rate (Fm) = 0.4035(In/Hr)  
 Area averaged Pervious ratio (Ap) = 1.0000  
 Program is now starting with Main Stream No. 3

++++++  
 Process from Point/Station 516.000 to Point/Station 517.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1148.000(Ft.)  
 Bottom (of initial area) elevation = 1101.000(Ft.)  
 Difference in elevation = 47.000(Ft.)  
 Slope = 0.04700 s(%)= 4.70  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 11.364 min.  
 Rainfall intensity = 2.977(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.789  
 Subarea runoff = 16.446(CFS)  
 Total initial stream area = 7.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

++++++  
 Process from Point/Station 517.000 to Point/Station 517.000

\*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 3  
 Effective stream flow area = 7.000 (Ac.)  
 Total study area this main stream = 7.000 (Ac.)  
 Runoff from this stream = 16.446 (CFS)  
 Time of concentration = 11.36 min.  
 Rainfall intensity = 2.977 (In/Hr)  
 Area averaged loss rate (Fm) = 0.3670 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	61.170	12.28	2.842
2	215.717	10.99	3.038
3	16.446	11.36	2.977
Qmax(1) =			
	1.000 *	1.000 *	61.170) +
	0.926 *	1.000 *	215.717) +
	0.948 *	1.000 *	16.446) + = 276.451
Qmax(2) =			
	1.080 *	0.895 *	61.170) +
	1.000 *	1.000 *	215.717) +
	1.023 *	0.967 *	16.446) + = 291.121
Qmax(3) =			
	1.055 *	0.925 *	61.170) +
	0.977 *	1.000 *	215.717) +
	1.000 *	1.000 *	16.446) + = 286.961

Total of 3 main streams to confluence:  
 Flow rates before confluence point:  
 62.170      216.717      17.446  
 Maximum flow rates at confluence using above data:  
 276.451      291.121      286.961  
 Effective Area of streams before confluence:  
 26.814      88.515      7.000  
 Effective area values after confluence:  
 122.329      119.281      120.329

Results of confluence:  
 Total flow rate = 291.121 (CFS)  
 Time of concentration = 10.990 min.  
 Effective stream area after confluence = 119.281 (Ac.)  
 Stream Area average Pervious fraction (Ap) = 0.963  
 Stream Area average soil loss rate (Fm) = 0.401 (In/Hr)  
 Steam effective area = 122.33 (Ac.)

+++++  
 Process from Point/Station 85.000 to Point/Station 86.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1092.300 (Ft.)  
 Downstream point/station elevation = 1059.300 (Ft.)  
 Pipe length = 950.00 (Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 291.121 (CFS)

Given pipe size = 39.00(In.)  
 NOTE: Normal flow is pressure flow in user selected pipe size.  
 The approximate hydraulic grade line above the pipe invert is  
 113.743(Ft.) at the headworks or inlet of the pipe(s)  
 Pipe friction loss = 118.059(Ft.)  
 Minor friction loss = 28.684(Ft.) K-factor = 1.50  
 Pipe flow velocity = 35.09(Ft/s)  
 Travel time through pipe = 0.45 min.  
 Time of concentration (TC) = 11.44 min.

++++  
 Process from Point/Station 86.000 to Point/Station 86.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 119.281(Ac.)  
 Runoff from this stream = 291.121(CFS)  
 Time of concentration = 11.44 min.  
 Rainfall intensity = 2.965(In/Hr)  
 Area averaged loss rate (Fm) = 0.4008(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.9633

++++  
 Process from Point/Station 518.000 to Point/Station 519.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1148.000(Ft.)  
 Bottom (of initial area) elevation = 1101.000(Ft.)  
 Difference in elevation = 47.000(Ft.)  
 Slope = 0.04700 s(%)= 4.70  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 11.364 min.  
 Rainfall intensity = 2.977(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.789  
 Subarea runoff = 19.970(CFS)  
 Total initial stream area = 8.500(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

++++  
 Process from Point/Station 519.000 to Point/Station 520.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1101.000(Ft.)  
 End of street segment elevation = 1066.500(Ft.)  
 Length of street segment = 900.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)

Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 29.954 (CFS)  
 Depth of flow = 0.414(Ft.), Average velocity = 5.714(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 15.968(Ft.)  
 Flow velocity = 5.71(Ft/s)  
 Travel time = 2.62 min. TC = 13.99 min.

Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 2.628(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.774  
 Subarea runoff = 14.629(CFS) for 8.500(Ac.)  
 Total runoff = 34.599(CFS)  
 Effective area this stream = 17.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 24.00(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 34.599(CFS)  
 Half street flow at end of street = 17.299(CFS)  
 Depth of flow = 0.433(Ft.), Average velocity = 5.921(Ft/s)  
 Flow width (from curb towards crown)= 16.884(Ft.)

++++  
 Process from Point/Station 520.000 to Point/Station 520.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 17.000(Ac.)  
 Runoff from this stream = 34.599(CFS)  
 Time of concentration = 13.99 min.  
 Rainfall intensity = 2.628(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000

++++  
 Process from Point/Station 521.000 to Point/Station 522.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00

Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1111.000(Ft.)  
 Bottom (of initial area) elevation = 1101.000(Ft.)  
 Difference in elevation = 10.000(Ft.)  
 Slope = 0.01000 s(%)= 1.00  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 15.486 min.  
 Rainfall intensity = 2.473(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.766  
 Subarea runoff = 10.424(CFS)  
 Total initial stream area = 5.500(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

++++  
 Process from Point/Station 522.000 to Point/Station 523.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1101.000(Ft.)  
 End of street segment elevation = 1066.500(Ft.)  
 Length of street segment = 900.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 26.533(CFS)  
 Depth of flow = 0.400(Ft.), Average velocity = 5.547(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 15.233(Ft.)  
 Flow velocity = 5.55(Ft/s)  
 Travel time = 2.70 min.      TC = 18.19 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)  
 Rainfall intensity = 2.245(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.753  
 Subarea runoff = 27.609(CFS) for 17.000(Ac.)  
 Total runoff = 38.033(CFS)  
 Effective area this stream = 22.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 46.50(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 38.033(CFS)  
 Half street flow at end of street = 19.016(CFS)

Depth of flow = 0.445(Ft.), Average velocity = 6.060(Ft/s)  
 Flow width (from curb towards crown)= 17.511(Ft.)

\*\*\*\*\*  
 Process from Point/Station 523.000 to Point/Station 523.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 22.500(Ac.)  
 Runoff from this stream = 38.033(CFS)  
 Time of concentration = 18.19 min.  
 Rainfall intensity = 2.245(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	291.121	11.44	2.965
2	34.599	13.99	2.628
3	38.033	18.19	2.245
Qmax(1) =			
	1.000 *	1.000 *	291.121) +
	1.149 *	0.818 *	34.599) +
	1.383 *	0.629 *	38.033) + = 356.728
Qmax(2) =			
	0.869 *	1.000 *	291.121) +
	1.000 *	1.000 *	34.599) +
	1.204 *	0.769 *	38.033) + = 322.681
Qmax(3) =			
	0.719 *	1.000 *	291.121) +
	0.831 *	1.000 *	34.599) +
	1.000 *	1.000 *	38.033) + = 276.134

Total of 3 streams to confluence:  
 Flow rates before confluence point:  
 291.121      34.599      38.033  
 Maximum flow rates at confluence using above data:  
 356.728      322.681      276.134  
 Area of streams before confluence:  
 119.281      17.000      22.500  
 Effective area values after confluence:  
 147.337      153.584      158.781

Results of confluence:  
 Total flow rate = 356.728(CFS)  
 Time of concentration = 11.441 min.  
 Effective stream area after confluence = 147.337(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.848  
 Stream Area average soil loss rate(Fm) = 0.392(In/Hr)  
 Study area (this main stream) = 158.78(Ac.)

\*\*\*\*\*  
 Process from Point/Station 86.000 to Point/Station 87.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1059.300(Ft.)  
 Downstream point/station elevation = 1053.200(Ft.)

Pipe length = 445.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 356.728(CFS)  
 Given pipe size = 48.00(In.)  
 NOTE: Normal flow is pressure flow in user selected pipe size.  
 The approximate hydraulic grade line above the pipe invert is  
 40.106(Ft.) at the headworks or inlet of the pipe(s)  
 Pipe friction loss = 27.436(Ft.)  
 Minor friction loss = 18.770(Ft.) K-factor = 1.50  
 Pipe flow velocity = 28.39(Ft/s)  
 Travel time through pipe = 0.26 min.  
 Time of concentration (TC) = 11.70 min.

\*\*\*\*\*  
 Process from Point/Station 87.000 to Point/Station 87.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 147.337(Ac.)  
 Runoff from this stream = 356.728(CFS)  
 Time of concentration = 11.70 min.  
 Rainfall intensity = 2.925(In/Hr)  
 Area averaged loss rate (Fm) = 0.3924(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.8480

\*\*\*\*\*  
 Process from Point/Station 524.000 to Point/Station 525.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 750.000(Ft.)  
 Top (of initial area) elevation = 1072.300(Ft.)  
 Bottom (of initial area) elevation = 1065.000(Ft.)  
 Difference in elevation = 7.300(Ft.)  
 Slope = 0.00973 s(%)= 0.97  
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 18.730 min.  
 Rainfall intensity = 2.206(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.735  
 Subarea runoff = 14.601(CFS)  
 Total initial stream area = 9.000(Ac.)  
 Pervious area fraction = 1.000  
 Initial area Fm value = 0.404(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 525.000 to Point/Station 525.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 9.000(Ac.)  
 Runoff from this stream = 14.601(CFS)  
 Time of concentration = 18.73 min.

Rainfall intensity = 2.206(In/Hr)  
 Area averaged loss rate (Fm) = 0.4035(In/Hr)  
 Area averaged Pervious ratio (Ap) = 1.0000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	356.728	11.70	2.925
2	14.601	18.73	2.206
Qmax(1) =			
	1.000 *	1.000 *	356.728) +
	1.399 *	0.625 *	14.601) + = 369.491
Qmax(2) =			
	0.716 *	1.000 *	356.728) +
	1.000 *	1.000 *	14.601) + = 270.033

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 356.728      14.601  
 Maximum flow rates at confluence using above data:  
 369.491      270.033  
 Area of streams before confluence:  
 147.337      9.000  
 Effective area values after confluence:  
 152.960      156.337  
 Results of confluence:  
 Total flow rate = 369.491(CFS)  
 Time of concentration = 11.702 min.  
 Effective stream area after confluence = 152.960(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.857  
 Stream Area average soil loss rate(Fm) = 0.393(In/Hr)  
 Study area (this main stream) = 156.34(Ac.)

++++  
 Process from Point/Station 87.000 to Point/Station 88.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1050.900(Ft.)  
 Downstream point/station elevation = 1033.600(Ft.)  
 Pipe length = 370.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 369.491(CFS)  
 Given pipe size = 54.00(In.)  
 Calculated individual pipe flow = 369.491(CFS)  
 Normal flow depth in pipe = 38.91(In.)  
 Flow top width inside pipe = 48.47(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 30.11(Ft/s)  
 Travel time through pipe = 0.20 min.  
 Time of concentration (TC) = 11.91 min.

++++  
 Process from Point/Station 88.000 to Point/Station 88.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 152.960(Ac.)  
 Runoff from this stream = 369.491(CFS)

Time of concentration = 11.91 min.  
Rainfall intensity = 2.895(In/Hr)  
Area averaged loss rate (Fm) = 0.3930(In/Hr)  
Area averaged Pervious ratio (Ap) = 0.8568

++++  
Process from Point/Station 526.000 to Point/Station 527.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

RESIDENTIAL(5 - 7 dwl/acre)  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
SCS curve number for soil(AMC 2) = 56.00  
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
Initial subarea data:  
Initial area flow distance = 1000.000(Ft.)  
Top (of initial area) elevation = 1065.000(Ft.)  
Bottom (of initial area) elevation = 1060.000(Ft.)  
Difference in elevation = 5.000(Ft.)  
Slope = 0.00500 s(%)= 0.50  
TC = k(0.389)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 17.789 min.  
Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
Effective runoff coefficient used for area (Q=KCIA) is C = 0.755  
Subarea runoff = 11.164(CFS)  
Total initial stream area = 6.500(Ac.)  
Pervious area fraction = 0.500  
Initial area Fm value = 0.367(In/Hr)

++++  
Process from Point/Station 527.000 to Point/Station 527.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
Stream flow area = 6.500(Ac.)  
Runoff from this stream = 11.164(CFS)  
Time of concentration = 17.79 min.  
Rainfall intensity = 2.275(In/Hr)  
Area averaged loss rate (Fm) = 0.3670(In/Hr)  
Area averaged Pervious ratio (Ap) = 0.5000

++++  
Process from Point/Station 528.000 to Point/Station 529.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

RESIDENTIAL(5 - 7 dwl/acre)  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
SCS curve number for soil(AMC 2) = 56.00  
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
Initial subarea data:  
Initial area flow distance = 1000.000(Ft.)  
Top (of initial area) elevation = 1065.000(Ft.)  
Bottom (of initial area) elevation = 1060.000(Ft.)

Difference in elevation = 5.000 (Ft.)  
 Slope = 0.00500 s(%) = 0.50  
 $TC = k(0.389) * [(length^3) / (elevation\ change)]^{0.2}$   
 Initial area time of concentration = 17.789 min.  
 Rainfall intensity = 2.275 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755  
 Subarea runoff = 11.164 (CFS)  
 Total initial stream area = 6.500 (Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367 (In/Hr)

++++++  
 Process from Point/Station 529.000 to Point/Station 529.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 3

Stream flow area = 6.500 (Ac.)  
 Runoff from this stream = 11.164 (CFS)  
 Time of concentration = 17.79 min.  
 Rainfall intensity = 2.275 (In/Hr)  
 Area averaged loss rate (Fm) = 0.3670 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	369.491	11.91	2.895
2	11.164	17.79	2.275
3	11.164	17.79	2.275
Qmax(1) =			
	1.000 *	1.000 *	369.491) +
	1.325 *	0.669 *	11.164) +
	1.325 *	0.669 *	11.164) + = 389.290
Qmax(2) =			
	0.752 *	1.000 *	369.491) +
	1.000 *	1.000 *	11.164) +
	1.000 *	1.000 *	11.164) + = 300.304
Qmax(3) =			
	0.752 *	1.000 *	369.491) +
	1.000 *	1.000 *	11.164) +
	1.000 *	1.000 *	11.164) + = 300.304

Total of 3 streams to confluence:

Flow rates before confluence point:

369.491 11.164 11.164

Maximum flow rates at confluence using above data:

389.290 300.304 300.304

Area of streams before confluence:

152.960 6.500 6.500

Effective area values after confluence:

161.661 165.960 165.960

Results of confluence:

Total flow rate = 389.290 (CFS)

Time of concentration = 11.907 min.

Effective stream area after confluence = 161.661 (Ac.)

Stream Area average Pervious fraction (Ap) = 0.829

Stream Area average soil loss rate (Fm) = 0.391 (In/Hr)

Study area (this main stream) = 165.96 (Ac.)

End of computations, Total Study Area = 191.00 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction( $A_p$ ) = 0.839

Area averaged SCS curve number = 70.9

LINE 'P1'

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
Rational Hydrology Study Date: 01/13/05

FONTANA / LINE P1 HYDROLOGY  
25 YEAR STORM  
JN 04339

Hall & Forman, Inc. - S/N 950

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

Rational hydrology study storm event year is 25.0  
10 Year storm 1 hour rainfall = 0.930(In.)  
100 Year storm 1 hour rainfall = 1.350(In.)  
Computed rainfall intensity:  
Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
Slope used for rainfall intensity curve b = 0.6000  
Soil antecedent moisture condition (AMC) = 2

\*\*\*\*\*  
Process from Point/Station 400.000 to Point/Station 401.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

UNDEVELOPED (poor cover) subarea.  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
SCS curve number for soil(AMC 2) = 78.00  
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)  
Initial subarea data:  
Initial area flow distance = 1000.000(Ft.)  
Top (of initial area) elevation = 1850.000(Ft.)  
Bottom (of initial area) elevation = 1300.000(Ft.)  
Difference in elevation = 550.000(Ft.)  
Slope = 0.55000 s(%)= 55.00  
TC = k(0.525)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 9.377 min.  
Rainfall intensity = 3.341(In/Hr) for a 25.0 year storm  
Effective runoff coefficient used for area (Q=KCIA) is C = 0.791  
Subarea runoff = 15.863(CFS)  
Total initial stream area = 6.000(Ac.)  
Pervious area fraction = 1.000  
Initial area Fm value = 0.404(In/Hr)

\*\*\*\*\*  
Process from Point/Station 401.000 to Point/Station 402.000  
\*\*\*\* IRREGULAR CHANNEL FLOW TRAVEL TIME \*\*\*\*

Estimated mean flow rate at midpoint of channel = 28.422(CFS)  
Depth of flow = 0.589(Ft.), Average velocity = 9.365(Ft/s)  
\*\*\*\*\* Irregular Channel Data \*\*\*\*\*

```

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
1                 0.00                 20.00
2                 150.00              0.00
3                 350.00              20.00
Manning's 'N' friction factor = 0.035
-----

```

```

Sub-Channel flow = 28.422(CFS)
'   '   flow top width = 10.306(Ft.)
'   '   velocity= 9.366(Ft/s)
'   '   area = 3.035(Sq.Ft)
'   '   Froude number = 3.042

```

```

Upstream point elevation = 1300.000(Ft.)
Downstream point elevation = 1087.000(Ft.)
Flow length = 850.000(Ft.)
Travel time = 1.51 min.
Time of concentration = 10.89 min.
Depth of flow = 0.589(Ft.)
Average velocity = 9.365(Ft/s)
Total irregular channel flow = 28.422(CFS)
Irregular channel normal depth above invert elev. = 0.589(Ft.)
Average velocity of channel(s) = 9.365(Ft/s)

```

```

Sub-Channel No. 1 Critical depth = 0.922(Ft.)
'   '   '   Critical flow top width = 16.133(Ft.)
'   '   '   Critical flow velocity= 3.822(Ft/s)
'   '   '   Critical flow area = 7.436(Sq.Ft)

```

```

Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404 (In/Hr)
Rainfall intensity = 3.054(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method)(Q=KCIA) is C = 0.781
Subarea runoff = 21.117(CFS) for 9.500(Ac.)
Total runoff = 36.980(CFS)
Effective area this stream = 15.50(Ac.)
Total Study Area (Main Stream No. 1) = 15.50(Ac.)
Area averaged Fm value = 0.404(In/Hr)

```

```

+++++
Process from Point/Station 402.000 to Point/Station 75.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****

```

```

-----
Upstream point/station elevation = 1080.000(Ft.)
Downstream point/station elevation = 1077.000(Ft.)
Pipe length = 550.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 36.980(CFS)
Given pipe size = 36.00(In.)
Calculated individual pipe flow = 36.980(CFS)
Normal flow depth in pipe = 23.27(In.)
Flow top width inside pipe = 34.42(In.)
Critical Depth = 23.74(In.)

```

Pipe flow velocity = 7.65(Ft/s)  
Travel time through pipe = 1.20 min.  
Time of concentration (TC) = 12.09 min.

\*\*\*\*\*  
Process from Point/Station 75.000 to Point/Station 75.000  
\*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 1  
Effective stream flow area = 15.500(Ac.)  
Total study area this main stream = 15.500(Ac.)  
Runoff from this stream = 36.980(CFS)  
Time of concentration = 12.09 min.  
Rainfall intensity = 2.869(In/Hr)  
Area averaged loss rate (Fm) = 0.4035(In/Hr)  
Area averaged Pervious ratio (Ap) = 1.0000  
Program is now starting with Main Stream No. 2

\*\*\*\*\*  
Process from Point/Station 403.000 to Point/Station 404.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

UNDEVELOPED (poor cover) subarea  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
SCS curve number for soil(AMC 2) = 78.00  
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)  
Initial subarea data:  
Initial area flow distance = 1000.000(Ft.)  
Top (of initial area) elevation = 1600.000(Ft.)  
Bottom (of initial area) elevation = 1140.000(Ft.)  
Difference in elevation = 460.000(Ft.)  
Slope = 0.46000 s(%)= 46.00  
TC = k(0.525)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 9.719 min.  
Rainfall intensity = 3.270(In/Hr) for a 25.0 year storm  
Effective runoff coefficient used for area (Q=KCIA) is C = 0.789  
Subarea runoff = 14.191(CFS)  
Total initial stream area = 5.500(Ac.)  
Pervious area fraction = 1.000  
Initial area Fm value = 0.404(In/Hr)

\*\*\*\*\*  
Process from Point/Station 404.000 to Point/Station 405.000  
\*\*\*\* IRREGULAR CHANNEL FLOW TRAVEL TIME \*\*\*\*

Estimated mean flow rate at midpoint of channel = 25.801(CFS)  
Depth of flow = 0.623(Ft.), Average velocity = 6.651(Ft/s)  
\*\*\*\*\* Irregular Channel Data \*\*\*\*\*

-----  
Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	20.00
2	200.00	0.00
3	400.00	20.00

Manning's 'N' friction factor = 0.035

-----  
 Sub-Channel flow = 25.801 (CFS)  
 ' ' flow top width = 12.457 (Ft.)  
 ' ' velocity = 6.651 (Ft/s)  
 ' ' area = 3.879 (Sq.Ft)  
 ' ' Froude number = 2.100

Upstream point elevation = 1140.000 (Ft.)  
 Downstream point elevation = 1085.000 (Ft.)  
 Flow length = 470.000 (Ft.)  
 Travel time = 1.18 min.  
 Time of concentration = 10.90 min.  
 Depth of flow = 0.623 (Ft.)  
 Average velocity = 6.651 (Ft/s)  
 Total irregular channel flow = 25.801 (CFS)  
 Irregular channel normal depth above invert elev. = 0.623 (Ft.)  
 Average velocity of channel(s) = 6.651 (Ft/s)

Sub-Channel No. 1 Critical depth = 0.836 (Ft.)  
 ' ' ' Critical flow top width = 16.719 (Ft.)  
 ' ' ' Critical flow velocity = 3.692 (Ft/s)  
 ' ' ' Critical flow area = 6.988 (Sq.Ft)

Adding area flow to channel  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 78.00  
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)  
 Rainfall intensity = 3.053 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.781  
 Subarea runoff = 20.390 (CFS) for 9.000 (Ac.)  
 Total runoff = 34.581 (CFS)  
 Effective area this stream = 14.50 (Ac.)  
 Total Study Area (Main Stream No. 2) = 14.50 (Ac.)  
 Area averaged Fm value = 0.404 (In/Hr)

++++  
 Process from Point/Station 405.000 to Point/Station 75.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

-----  
 Upstream point/station elevation = 1078.000 (Ft.)  
 Downstream point/station elevation = 1077.000 (Ft.)  
 Pipe length = 150.00 (Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 34.581 (CFS)  
 Given pipe size = 36.00 (In.)  
 Calculated individual pipe flow = 34.581 (CFS)  
 Normal flow depth in pipe = 20.84 (In.)  
 Flow top width inside pipe = 35.55 (In.)  
 Critical Depth = 22.92 (In.)  
 Pipe flow velocity = 8.16 (Ft/s)  
 Travel time through pipe = 0.31 min.  
 Time of concentration (TC) = 11.20 min.

++++

Process from Point/Station 75.000 to Point/Station 75.000  
 \*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 2  
 Effective stream flow area = 14.500 (Ac.)  
 Total study area this main stream = 14.500 (Ac.)  
 Runoff from this stream = 34.581 (CFS)  
 Time of concentration = 11.20 min.  
 Rainfall intensity = 3.003 (In/Hr)  
 Area averaged loss rate (Fm) = 0.4035 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 1.0000  
 Program is now starting with Main Stream No. 3

+++++  
 Process from Point/Station 406.000 to Point/Station 408.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367 (In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000 (Ft.)  
 Top (of initial area) elevation = 1065.000 (Ft.)  
 Bottom (of initial area) elevation = 1055.000 (Ft.)  
 Difference in elevation = 10.000 (Ft.)  
 Slope = 0.01000 s(%) = 1.00  
 $TC = k(0.389) * [(length^3) / (elevation\ change)]^{0.2}$   
 Initial area time of concentration = 15.486 min.  
 Rainfall intensity = 2.473 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.766  
 Subarea runoff = 14.214 (CFS)  
 Total initial stream area = 7.500 (Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367 (In/Hr)

+++++  
 Process from Point/Station 408.000 to Point/Station 408.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 3 in normal stream number 1  
 Stream flow area = 7.500 (Ac.)  
 Runoff from this stream = 14.214 (CFS)  
 Time of concentration = 15.49 min.  
 Rainfall intensity = 2.473 (In/Hr)  
 Area averaged loss rate (Fm) = 0.3670 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000

+++++  
 Process from Point/Station 407.000 to Point/Station 408.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1065.000(Ft.)  
 Bottom (of initial area) elevation = 1055.000(Ft.)  
 Difference in elevation = 10.000(Ft.)  
 Slope = 0.01000 s(%)= 1.00  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 15.486 min.  
 Rainfall intensity = 2.473(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.766  
 Subarea runoff = 11.371(CFS)  
 Total initial stream area = 6.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

++++++  
 Process from Point/Station 408.000 to Point/Station 408.000  
 \*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*

Along Main Stream number: 3 in normal stream number 2  
 Stream flow area = 6.000(Ac.)  
 Runoff from this stream = 11.371(CFS)  
 Time of concentration = 15.49 min.  
 Rainfall intensity = 2.473(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	14.214	15.49	2.473
2	11.371	15.49	2.473
Qmax(1) =			
	1.000 *	1.000 *	14.214) +
	1.000 *	1.000 *	11.371) + = 25.585
Qmax(2) =			
	1.000 *	1.000 *	14.214) +
	1.000 *	1.000 *	11.371) + = 25.585

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 14.214      11.371  
 Maximum flow rates at confluence using above data:  
 25.585      25.585  
 Area of streams before confluence:  
 7.500      6.000  
 Effective area values after confluence:  
 13.500      13.500  
 Results of confluence:  
 Total flow rate = 25.585(CFS)  
 Time of concentration = 15.486 min.  
 Effective stream area after confluence = 13.500(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.500

Stream Area average soil loss rate(Fm) = 0.367(In/Hr)  
Study area (this main stream) = 13.50(Ac.)

++++  
Process from Point/Station 408.000 to Point/Station 408.000  
\*\*\*\* CONFLUENCE OF MAIN STREAMS \*\*\*\*

The following data inside Main Stream is listed:

In Main Stream number: 3  
Effective stream flow area = 13.500(Ac.)  
Total study area this main stream = 13.500(Ac.)  
Runoff from this stream = 25.585(CFS)  
Time of concentration = 15.49 min.  
Rainfall intensity = 2.473(In/Hr)  
Area averaged loss rate (Fm) = 0.3670(In/Hr)  
Area averaged Pervious ratio (Ap) = 0.5000  
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	36.980	12.09	2.869
2	34.581	11.20	3.003
3	25.585	15.49	2.473
Qmax(1) =			
	1.000 *	1.000 *	36.980) +
	0.948 *	1.000 *	34.581) +
	1.188 *	0.781 *	25.585) + = 93.508
Qmax(2) =			
	1.054 *	0.927 *	36.980) +
	1.000 *	1.000 *	34.581) +
	1.252 *	0.723 *	25.585) + = 93.883
Qmax(3) =			
	0.839 *	1.000 *	36.980) +
	0.796 *	1.000 *	34.581) +
	1.000 *	1.000 *	25.585) + = 84.149

Total of 3 main streams to confluence:  
Flow rates before confluence point:  
37.980 35.581 26.585  
Maximum flow rates at confluence using above data:  
93.508 93.883 84.149  
Effective Area of streams before confluence:  
15.500 14.500 13.500  
Effective area values after confluence:  
40.538 38.630 43.500

Results of confluence:  
Total flow rate = 93.883(CFS)  
Time of concentration = 11.203 min.  
Effective stream area after confluence = 38.630(Ac.)  
Stream Area average Pervious fraction(Ap) = 0.845  
Stream Area average soil loss rate(Fm) = 0.392(In/Hr)  
Stream effective area = 43.50(Ac.)

++++  
Process from Point/Station 75.000 to Point/Station 76.000

\*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1075.000(Ft.)  
 Downstream point/station elevation = 1047.000(Ft.)  
 Pipe length = 550.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 93.883(CFS)  
 Given pipe size = 42.00(In.)  
 Calculated individual pipe flow = 93.883(CFS)  
 Normal flow depth in pipe = 18.82(In.)  
 Flow top width inside pipe = 41.77(In.)  
 Critical Depth = 35.93(In.)  
 Pipe flow velocity = 22.47(Ft/s)  
 Travel time through pipe = 0.41 min.  
 Time of concentration (TC) = 11.61 min.

+++++  
 Process from Point/Station 76.000 to Point/Station 80.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1047.000(Ft.)  
 Downstream point/station elevation = 1041.300(Ft.)  
 Pipe length = 1000.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 93.883(CFS)  
 Given pipe size = 54.00(In.)  
 Calculated individual pipe flow = 93.883(CFS)  
 Normal flow depth in pipe = 31.17(In.)  
 Flow top width inside pipe = 53.35(In.)  
 Critical Depth = 34.13(In.)  
 Pipe flow velocity = 9.88(Ft/s)  
 Travel time through pipe = 1.69 min.  
 Time of concentration (TC) = 13.30 min.

+++++  
 Process from Point/Station 80.000 to Point/Station 80.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 38.630(Ac.)  
 Runoff from this stream = 93.883(CFS)  
 Time of concentration = 13.30 min.  
 Rainfall intensity = 2.709(In/Hr)  
 Area averaged loss rate (Fm) = 0.3922(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.8448

+++++  
 Process from Point/Station 80.000 to Point/Station 80.000  
 \*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

---

Soil classification AP and SCS values input by user  
 USER INPUT of soil data for subarea  
 SCS curve number for soil(AMC 2) = 74.46  
 Pervious ratio(Ap) = 0.8510 Max loss rate(Fm)= 0.393(In/Hr)  
 Rainfall intensity = 2.853(In/Hr) for a 25.0 year storm  
 User specified values are as follows:  
 TC = 12.20 min. Rain intensity = 2.85(In/Hr)  
 Total area this stream = 112.08(Ac.)  
 Total Study Area (Main Stream No. 1) = 125.58(Ac.)  
 Total runoff = 261.23(CFS)

+++++  
 Process from Point/Station 80.000 to Point/Station 80.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 112.080(Ac.)  
 Runoff from this stream = 261.230(CFS)  
 Time of concentration = 12.20 min.  
 Rainfall intensity = 2.853(In/Hr)  
 Area averaged loss rate (Fm) = 0.3930(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.8510  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	93.883	13.30	2.709
2	261.230	12.20	2.853
Qmax(1) =			
	1.000 *	1.000 *	93.883) +
	0.942 *	1.000 *	261.230) + = 339.845
Qmax(2) =			
	1.062 *	0.917 *	93.883) +
	1.000 *	1.000 *	261.230) + = 352.705

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 93.883 261.230  
 Maximum flow rates at confluence using above data:  
 339.845 352.705  
 Area of streams before confluence:  
 38.630 112.080  
 Effective area values after confluence:  
 150.710 147.521  
 Results of confluence:  
 Total flow rate = 352.705(CFS)  
 Time of concentration = 12.200 min.  
 Effective stream area after confluence = 147.521(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.849  
 Stream Area average soil loss rate(Fm) = 0.393(In/Hr)  
 Study area (this main stream) = 150.71(Ac.)

+++++  
 Process from Point/Station 80.000 to Point/Station 88.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1037.200(Ft.)  
 Downstream point/station elevation = 1031.600(Ft.)  
 Pipe length = 1450.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 352.705(CFS)  
 Given pipe size = 90.00(In.)  
 Calculated individual pipe flow = 352.705(CFS)  
 Normal flow depth in pipe = 57.56(In.)  
 Flow top width inside pipe = 86.42(In.)  
 Critical Depth = 58.29(In.)  
 Pipe flow velocity = 11.82(Ft/s)  
 Travel time through pipe = 2.04 min.

Time of concentration (TC) = 14.24 min.

\*\*\*\*\*  
Process from Point/Station 88.000 to Point/Station 88.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
Stream flow area = 147.521(Ac.)  
Runoff from this stream = 352.705(CFS)  
Time of concentration = 14.24 min.  
Rainfall intensity = 2.600(In/Hr)  
Area averaged loss rate (Fm) = 0.3928(In/Hr)  
Area averaged Pervious ratio (Ap) = 0.8494

\*\*\*\*\*  
Process from Point/Station 88.000 to Point/Station 88.000  
\*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

---

Soil classification AP and SCS values input by user  
USER INPUT of soil data for subarea  
SCS curve number for soil(AMC 2) = 73.85  
Pervious ratio(Ap) = 0.8290 Max loss rate(Fm)= 0.391(In/Hr)  
Rainfall intensity = 2.895(In/Hr) for a 25.0 year storm  
User specified values are as follows:  
TC = 11.91 min. Rain intensity = 2.89(In/Hr)  
Total area this stream = 161.66(Ac.)  
Total Study Area (Main Stream No. 1) = 287.24(Ac.)  
Total runoff = 389.29(CFS)

\*\*\*\*\*  
Process from Point/Station 88.000 to Point/Station 88.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2  
Stream flow area = 161.660(Ac.)  
Runoff from this stream = 389.290(CFS)  
Time of concentration = 11.91 min.  
Rainfall intensity = 2.895(In/Hr)  
Area averaged loss rate (Fm) = 0.3910(In/Hr)  
Area averaged Pervious ratio (Ap) = 0.8290  
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	352.705	14.24	2.600
2	389.290	11.91	2.895
Qmax(1) =	1.000 * 352.705) +	1.000 * 389.290) + =	696.160
Qmax(2) =	1.134 * 352.705) +	1.000 * 389.290) + =	723.574

Total of 2 streams to confluence:  
Flow rates before confluence point:  
352.705 389.290

Maximum flow rates at confluence using above data:  
 696.160            723.574  
 Area of streams before confluence:  
 147.521            161.660  
 Effective area values after confluence:  
 309.181            285.002  
 Results of confluence:  
 Total flow rate =    723.574(CFS)  
 Time of concentration =    11.910 min.  
 Effective stream area after confluence =    285.002(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.839  
 Stream Area average soil loss rate(Fm) =    0.392(In/Hr)  
 Study area (this main stream) =    309.18(Ac.)

\*\*\*\*\*  
 Process from Point/Station            88.000 to Point/Station            89.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1031.100(Ft.)  
 Downstream point/station elevation = 1028.800(Ft.)  
 Pipe length = 550.00(Ft.)    Manning's N = 0.013  
 No. of pipes = 1    Required pipe flow = 723.574(CFS)  
 Given pipe size = 96.00(In.)  
 NOTE: Normal flow is pressure flow in user selected pipe size.  
 The approximate hydraulic grade line above the pipe invert is  
 5.987(Ft.) at the headworks or inlet of the pipe(s)  
 Pipe friction loss = 3.460(Ft.)  
 Minor friction loss = 4.826(Ft.)    K-factor = 1.50  
 Pipe flow velocity = 14.40(Ft/s)  
 Travel time through pipe = 0.64 min.  
 Time of concentration (TC) = 12.55 min.

\*\*\*\*\*  
 Process from Point/Station            89.000 to Point/Station            89.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 285.002(Ac.)  
 Runoff from this stream = 723.574(CFS)  
 Time of concentration = 12.55 min.  
 Rainfall intensity = 2.806(In/Hr)  
 Area averaged loss rate (Fm) = 0.3919(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.8387

\*\*\*\*\*  
 Process from Point/Station            513.000 to Point/Station            530.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000    Max loss rate(Fm) = 0.404(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1770.000(Ft.)

Bottom (of initial area) elevation = 1380.000(Ft.)  
 Difference in elevation = 390.000(Ft.)  
 Slope = 0.39000 s(%) = 39.00  
 $TC = k(0.525) * [(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 10.045 min.  
 Rainfall intensity = 3.206(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.787  
 Subarea runoff = 15.134(CFS)  
 Total initial stream area = 6.000(Ac.)  
 Pervious area fraction = 1.000  
 Initial area Fm value = 0.404(In/Hr)

++++++  
 Process from Point/Station 530.000 to Point/Station 531.000  
 \*\*\*\* IRREGULAR CHANNEL FLOW TRAVEL TIME \*\*\*\*

-----  
 Estimated mean flow rate at midpoint of channel = 23.962(CFS)  
 Depth of flow = 0.429(Ft.), Average velocity = 8.665(Ft/s)  
 \*\*\*\*\* Irregular Channel Data \*\*\*\*\*

-----  
 Information entered for subchannel number 1 :  

Point number	'X' coordinate	'Y' coordinate
1	0.00	10.00
2	150.00	0.00
3	300.00	10.00

 Manning's 'N' friction factor = 0.035

-----  
 Sub-Channel flow = 23.962(CFS)  
 ' ' flow top width = 12.881(Ft.)  
 ' ' velocity = 8.665(Ft/s)  
 ' ' area = 2.765(Sq.Ft)  
 ' ' Froude number = 3.296

Upstream point elevation = 1380.000(Ft.)  
 Downstream point elevation = 1120.000(Ft.)  
 Flow length = 800.000(Ft.)  
 Travel time = 1.54 min.  
 Time of concentration = 11.58 min.  
 Depth of flow = 0.429(Ft.)  
 Average velocity = 8.665(Ft/s)  
 Total irregular channel flow = 23.962(CFS)  
 Irregular channel normal depth above invert elev. = 0.429(Ft.)  
 Average velocity of channel(s) = 8.665(Ft/s)

Sub-Channel No. 1 Critical depth = 0.691(Ft.)  
 ' ' ' Critical flow top width = 20.742(Ft.)  
 ' ' ' Critical flow velocity = 3.342(Ft/s)  
 ' ' ' Critical flow area = 7.171(Sq.Ft)

Adding area flow to channel  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404(In/Hr)  
 Rainfall intensity = 2.943(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.777

Subarea runoff = 14.582(CFS) for 7.000(Ac.)  
 Total runoff = 29.716(CFS)  
 Effective area this stream = 13.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 300.24(Ac.)  
 Area averaged Fm value = 0.404(In/Hr)

++++  
 Process from Point/Station 531.000 to Point/Station 532.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1120.000(Ft.)  
 End of street segment elevation = 1056.000(Ft.)  
 Length of street segment = 1800.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 48.003(CFS)  
 Depth of flow = 0.484(Ft.), Average velocity = 6.240(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 19.430(Ft.)  
 Flow velocity = 6.24(Ft/s)  
 Travel time = 4.81 min. TC = 16.39 min.  
 Adding area flow to street  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)  
 Rainfall intensity = 2.390(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.748  
 Subarea runoff = 22.129(CFS) for 16.000(Ac.)  
 Total runoff = 51.845(CFS)  
 Effective area this stream = 29.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 316.24(Ac.)  
 Area averaged Fm value = 0.404(In/Hr)  
 Street flow at end of street = 51.845(CFS)  
 Half street flow at end of street = 25.923(CFS)  
 Depth of flow = 0.495(Ft.), Average velocity = 6.362(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++  
 Process from Point/Station 532.000 to Point/Station 532.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 29.000 (Ac.)  
 Runoff from this stream = 51.845 (CFS)  
 Time of concentration = 16.39 min.  
 Rainfall intensity = 2.390 (In/Hr)  
 Area averaged loss rate (Fm) = 0.4035 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 1.0000

\*\*\*\*\*  
 Process from Point/Station 533.000 to Point/Station 534.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 56.00  
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.073 (In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000 (Ft.)  
 Top (of initial area) elevation = 1064.100 (Ft.)  
 Bottom (of initial area) elevation = 1059.100 (Ft.)  
 Difference in elevation = 5.000 (Ft.)  
 Slope = 0.00500 s(%) = 0.50  
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.902 min.  
 Rainfall intensity = 2.638 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875  
 Subarea runoff = 15.004 (CFS)  
 Total initial stream area = 6.500 (Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073 (In/Hr)

\*\*\*\*\*  
 Process from Point/Station 534.000 to Point/Station 535.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1059.300 (Ft.)  
 End of street segment elevation = 1056.200 (Ft.)  
 Length of street segment = 330.000 (Ft.)  
 Height of curb above gutter flowline = 8.0 (In.)  
 Width of half street (curb to crown) = 20.000 (Ft.)  
 Distance from crown to crossfall grade break = 18.500 (Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000 (Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500 (Ft.)  
 Gutter hike from flowline = 1.500 (In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 21.352 (CFS)  
 Depth of flow = 0.463 (Ft.), Average velocity = 3.095 (Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 18.380 (Ft.)  
 Flow velocity = 3.09 (Ft/s)  
 Travel time = 1.78 min. TC = 15.68 min.

Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.454(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.873  
 Subarea runoff = 10.712(CFS) for 5.500(Ac.)  
 Total runoff = 25.715(CFS)  
 Effective area this stream = 12.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 328.24(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 25.715(CFS)  
 Half street flow at end of street = 12.858(CFS)  
 Depth of flow = 0.490(Ft.), Average velocity = 3.240(Ft/s)  
 Flow width (from curb towards crown)= 19.740(Ft.)

+++++  
 Process from Point/Station 535.000 to Point/Station 535.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 12.000(Ac.)  
 Runoff from this stream = 25.715(CFS)  
 Time of concentration = 15.68 min.  
 Rainfall intensity = 2.454(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	723.574	12.55	2.806
2	51.845	16.39	2.390
3	25.715	15.68	2.454
Qmax(1) =			
	1.000 *	1.000 *	723.574) +
	1.209 *	0.765 *	51.845) +
	1.147 *	0.800 *	25.715) + = 795.178
Qmax(2) =			
	0.828 *	1.000 *	723.574) +
	1.000 *	1.000 *	51.845) +
	0.973 *	1.000 *	25.715) + = 675.821
Qmax(3) =			
	0.855 *	1.000 *	723.574) +
	1.032 *	0.957 *	51.845) +
	1.000 *	1.000 *	25.715) + = 695.223

Total of 3 streams to confluence:  
 Flow rates before confluence point:  
 723.574 51.845 25.715  
 Maximum flow rates at confluence using above data:  
 795.178 675.821 695.223  
 Area of streams before confluence:

285.002	29.000	12.000
Effective area values after confluence:		
316.803	326.002	324.742

Results of confluence:

Total flow rate = 795.178(CFS)

Time of concentration = 12.547 min.

Effective stream area after confluence = 316.803(Ac.)

Stream Area average Pervious fraction( $A_p$ ) = 0.826

Stream Area average soil loss rate( $F_m$ ) = 0.381(In/Hr)

Study area (this main stream) = 326.00(Ac.)

End of computations, Total Study Area = 358.24 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction( $A_p$ ) = 0.827

Area averaged SCS curve number = 73.5

LINE "SIERRA AVE

## San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
 Rational Hydrology Study Date: 01/13/05

FONTANA / LINE SIERRA AVENUE HYDROLOGY  
 25 YEAR STORM  
 JN 04339

Hall & Forman, Inc. - S/N 950

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

Rational hydrology study storm event year is 25.0  
 10 Year storm 1 hour rainfall = 0.930(In.)  
 100 Year storm 1 hour rainfall = 1.350(In.)  
 Computed rainfall intensity:  
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
 Slope used for rainfall intensity curve b = 0.6000  
 Soil antecedent moisture condition (AMC) = 2

\*\*\*\*\*  
 Process from Point/Station 200.000 to Point/Station 201.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

COMMERCIAL subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1103.000(Ft.)  
 Bottom (of initial area) elevation = 1098.000(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%) = 0.50  
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.902 min.  
 Rainfall intensity = 2.638(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.867  
 Subarea runoff = 12.575(CFS)  
 Total initial stream area = 5.500(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.098(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 201.000 to Point/Station 202.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1098.000(Ft.)  
 End of street segment elevation = 1091.600(Ft.)  
 Length of street segment = 670.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 23.435(CFS)  
 Depth of flow = 0.475(Ft.), Average velocity = 3.187(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 18.988(Ft.)  
 Flow velocity = 3.19(Ft/s)  
 Travel time = 3.50 min. TC = 17.41 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.305(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.868  
 Subarea runoff = 17.435(CFS) for 9.500(Ac.)  
 Total runoff = 30.010(CFS)  
 Effective area this stream = 15.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 15.00(Ac.)  
 Area averaged Fm value = 0.082(In/Hr)  
 Street flow at end of street = 30.010(CFS)  
 Half street flow at end of street = 15.005(CFS)  
 Depth of flow = 0.509(Ft.), Average velocity = 3.445(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 202.000 to Point/Station 60.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1084.600(Ft.)  
 Downstream point/station elevation = 1078.400(Ft.)  
 Pipe length = 555.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 30.010(CFS)  
 Given pipe size = 42.00(In.)  
 Calculated individual pipe flow = 30.010(CFS)  
 Normal flow depth in pipe = 15.26(In.)  
 Flow top width inside pipe = 40.40(In.)  
 Critical Depth = 20.31(In.)  
 Pipe flow velocity = 9.50(Ft/s)  
 Travel time through pipe = 0.97 min.  
 Time of concentration (TC) = 18.38 min.

+++++

Process from Point/Station 60.000 to Point/Station 60.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 15.000(Ac.)  
 Runoff from this stream = 30.010(CFS)  
 Time of concentration = 18.38 min.  
 Rainfall intensity = 2.231(In/Hr)  
 Area averaged loss rate (Fm) = 0.0823(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000

+++++  
 Process from Point/Station 203.000 to Point/Station 204.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

COMMERCIAL subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1103.000(Ft.)  
 Bottom (of initial area) elevation = 1096.000(Ft.)  
 Difference in elevation = 7.000(Ft.)  
 Slope = 0.00700 s(%)= 0.70  
 $TC = k(0.304) * [(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 12.997 min.  
 Rainfall intensity = 2.747(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.868  
 Subarea runoff = 15.497(CFS)  
 Total initial stream area = 6.500(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.098(In/Hr)

+++++  
 Process from Point/Station 204.000 to Point/Station 205.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1096.000(Ft.)  
 End of street segment elevation = 1090.500(Ft.)  
 Length of street segment = 675.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 25.630(CFS)  
 Depth of flow = 0.499(Ft.), Average velocity = 3.085(Ft/s)

Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 3.08(Ft/s)  
 Travel time = 3.65 min. TC = 16.64 min.

Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)  
 Rainfall intensity = 2.368(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.863  
 Subarea runoff = 15.151(CFS) for 8.500(Ac.)  
 Total runoff = 30.648(CFS)  
 Effective area this stream = 15.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 30.00(Ac.)  
 Area averaged Fm value = 0.098(In/Hr)  
 Street flow at end of street = 30.648(CFS)  
 Half street flow at end of street = 15.324(CFS)  
 Depth of flow = 0.523(Ft.), Average velocity = 3.312(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++  
 Process from Point/Station 205.000 to Point/Station 205.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 15.000(Ac.)  
 Runoff from this stream = 30.648(CFS)  
 Time of concentration = 16.64 min.  
 Rainfall intensity = 2.368(In/Hr)  
 Area averaged loss rate (Fm) = 0.0978(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	30.010	18.38	2.231
2	30.648	16.64	2.368
Qmax(1) =			
	1.000 *	1.000 *	30.010) +
	0.940 *	1.000 *	30.648) + = 58.812
Qmax(2) =			
	1.064 *	0.906 *	30.010) +
	1.000 *	1.000 *	30.648) + = 59.555

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 30.010 30.648  
 Maximum flow rates at confluence using above data:  
 58.812 59.555  
 Area of streams before confluence:  
 15.000 15.000

Effective area values after confluence:

30.000            28.584

Results of confluence:

Total flow rate = 59.555(CFS)

Time of concentration = 16.645 min.

Effective stream area after confluence = 28.584(Ac.)

Stream Area average Pervious fraction(Ap) = 0.100

Stream Area average soil loss rate(Fm) = 0.090(In/Hr)

Study area (this main stream) = 30.00(Ac.)

+++++  
Process from Point/Station            60.000 to Point/Station            61.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1078.400(Ft.)  
Downstream point/station elevation = 1076.700(Ft.)  
Pipe length = 500.00(Ft.)    Manning's N = 0.013  
No. of pipes = 1    Required pipe flow = 59.555(CFS)  
Given pipe size = 42.00(In.)  
Calculated individual pipe flow = 59.555(CFS)  
Normal flow depth in pipe = 35.06(In.)  
Flow top width inside pipe = 31.19(In.)  
Critical Depth = 29.01(In.)  
Pipe flow velocity = 6.95(Ft/s)  
Travel time through pipe = 1.20 min.  
Time of concentration (TC) = 17.84 min.

+++++  
Process from Point/Station            61.000 to Point/Station            61.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
Stream flow area = 28.584(Ac.)  
Runoff from this stream = 59.555(CFS)  
Time of concentration = 17.84 min.  
Rainfall intensity = 2.271(In/Hr)  
Area averaged loss rate (Fm) = 0.0901(In/Hr)  
Area averaged Pervious ratio (Ap) = 0.1000

+++++  
Process from Point/Station            206.000 to Point/Station            207.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

COMMERCIAL subarea type

Decimal fraction soil group A = 1.000

Decimal fraction soil group B = 0.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 32.00

Pervious ratio(Ap) = 0.1000            Max loss rate(Fm) = 0.098(In/Hr)

Initial subarea data:

Initial area flow distance = 1000.000(Ft.)

Top (of initial area) elevation = 1103.000(Ft.)

Bottom (of initial area) elevation = 1097.000(Ft.)

Difference in elevation = 6.000(Ft.)

Slope = 0.00600 s(%) = 0.60

TC = k(0.304)\*[(length^3)/(elevation change)]^0.2

Initial area time of concentration = 13.404 min.

Rainfall intensity = 2.697(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.867  
 Subarea runoff = 14.033(CFS)  
 Total initial stream area = 6.000(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.098(In/Hr)

++++  
 Process from Point/Station 207.000 to Point/Station 208.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1097.000(Ft.)  
 End of street segment elevation = 1089.300(Ft.)  
 Length of street segment = 775.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 25.728(CFS)  
 Depth of flow = 0.486(Ft.), Average velocity = 3.310(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 19.533(Ft.)  
 Flow velocity = 3.31(Ft/s)  
 Travel time = 3.90 min. TC = 17.31 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)  
 Rainfall intensity = 2.313(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.862  
 Subarea runoff = 17.869(CFS) for 10.000(Ac.)  
 Total runoff = 31.903(CFS)  
 Effective area this stream = 16.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 46.00(Ac.)  
 Area averaged Fm value = 0.098(In/Hr)  
 Street flow at end of street = 31.903(CFS)  
 Half street flow at end of street = 15.951(CFS)  
 Depth of flow = 0.515(Ft.), Average velocity = 3.572(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++  
 Process from Point/Station 208.000 to Point/Station 208.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 16.000(Ac.)  
 Runoff from this stream = 31.903(CFS)  
 Time of concentration = 17.31 min.  
 Rainfall intensity = 2.313(In/Hr)  
 Area averaged loss rate (Fm) = 0.0978(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	59.555	17.84	2.271
2	31.903	17.31	2.313
Qmax(1) =			
	1.000 *	1.000 *	59.555) +
	0.981 *	1.000 *	31.903) + = 90.852
Qmax(2) =			
	1.019 *	0.970 *	59.555) +
	1.000 *	1.000 *	31.903) + = 90.778

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 59.555      31.903  
 Maximum flow rates at confluence using above data:  
 90.852      90.778

Area of streams before confluence:  
 28.584      16.000  
 Effective area values after confluence:  
 44.584      43.723

Results of confluence:  
 Total flow rate = 90.852(CFS)  
 Time of concentration = 17.844 min.  
 Effective stream area after confluence = 44.584(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.100  
 Stream Area average soil loss rate(Fm) = 0.093(In/Hr)  
 Study area (this main stream) = 44.58(Ac.)

+++++  
 Process from Point/Station      61.000 to Point/Station      62.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1076.700(Ft.)  
 Downstream point/station elevation = 1065.000(Ft.)  
 Pipe length = 1320.00(Ft.)      Manning's N = 0.013  
 No. of pipes = 1      Required pipe flow = 90.852(CFS)  
 Given pipe size = 48.00(In.)  
 Calculated individual pipe flow = 90.852(CFS)  
 Normal flow depth in pipe = 28.78(In.)  
 Flow top width inside pipe = 47.04(In.)  
 Critical Depth = 34.69(In.)  
 Pipe flow velocity = 11.54(Ft/s)  
 Travel time through pipe = 1.91 min.  
 Time of concentration (TC) = 19.75 min.

+++++  
 Process from Point/Station      62.000 to Point/Station      62.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 44.584 (Ac.)  
 Runoff from this stream = 90.852 (CFS)  
 Time of concentration = 19.75 min.  
 Rainfall intensity = 2.137 (In/Hr)  
 Area averaged loss rate (Fm) = 0.0928 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000

\*\*\*\*\*  
 Process from Point/Station 209.000 to Point/Station 210.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

COMMERCIAL subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 32.00  
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.098 (In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000 (Ft.)  
 Top (of initial area) elevation = 1090.500 (Ft.)  
 Bottom (of initial area) elevation = 1084.500 (Ft.)  
 Difference in elevation = 6.000 (Ft.)  
 Slope = 0.00600 s (%) = 0.60  
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.404 min.  
 Rainfall intensity = 2.697 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.867  
 Subarea runoff = 12.864 (CFS)  
 Total initial stream area = 5.500 (Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.098 (In/Hr)

\*\*\*\*\*  
 Process from Point/Station 210.000 to Point/Station 211.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1084.500 (Ft.)  
 End of street segment elevation = 1076.500 (Ft.)  
 Length of street segment = 875.000 (Ft.)  
 Height of curb above gutter flowline = 8.0 (In.)  
 Width of half street (curb to crown) = 20.000 (Ft.)  
 Distance from crown to crossfall grade break = 18.500 (Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000 (Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500 (Ft.)  
 Gutter hike from flowline = 1.500 (In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 25.728 (CFS)  
 Depth of flow = 0.492 (Ft.), Average velocity = 3.208 (Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 19.846 (Ft.)

Flow velocity = 3.21(Ft/s)  
 Travel time = 4.55 min. TC = 17.95 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.263(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.868  
 Subarea runoff = 19.533(CFS) for 11.000(Ac.)  
 Total runoff = 32.397(CFS)  
 Effective area this stream = 16.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 62.50(Ac.)  
 Area averaged Fm value = 0.082(In/Hr)  
 Street flow at end of street = 32.397(CFS)  
 Half street flow at end of street = 16.198(CFS)  
 Depth of flow = 0.523(Ft.), Average velocity = 3.505(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 211.000 to Point/Station 211.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

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Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 16.500(Ac.)  
 Runoff from this stream = 32.397(CFS)  
 Time of concentration = 17.95 min.  
 Rainfall intensity = 2.263(In/Hr)  
 Area averaged loss rate (Fm) = 0.0815(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000

++++++  
 Process from Point/Station 212.000 to Point/Station 213.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

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COMMERCIAL subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1092.600(Ft.)  
 Bottom (of initial area) elevation = 1086.000(Ft.)  
 Difference in elevation = 6.600(Ft.)  
 Slope = 0.00660 s(%)= 0.66  
 $TC = k(0.304) * [(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.151 min.  
 Rainfall intensity = 2.728(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.868  
 Subarea runoff = 11.834(CFS)  
 Total initial stream area = 5.000(Ac.)

Pervious area fraction = 0.100  
Initial area Fm value = 0.098(In/Hr)

+++++  
Process from Point/Station 213.000 to Point/Station 214.000  
\*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1086.000(Ft.)  
End of street segment elevation = 1076.500(Ft.)  
Length of street segment = 1000.000(Ft.)  
Height of curb above gutter flowline = 8.0(In.)  
Width of half street (curb to crown) = 20.000(Ft.)  
Distance from crown to crossfall grade break = 18.500(Ft.)  
Slope from gutter to grade break (v/hz) = 0.020  
Slope from grade break to crown (v/hz) = 0.020  
Street flow is on [2] side(s) of the street  
Distance from curb to property line = 10.000(Ft.)  
Slope from curb to property line (v/hz) = 0.020  
Gutter width = 1.500(Ft.)  
Gutter hike from flowline = 1.500(In.)  
Manning's N in gutter = 0.0150  
Manning's N from gutter to grade break = 0.0150  
Manning's N from grade break to crown = 0.0150  
Estimated mean flow rate at midpoint of street = 23.668(CFS)  
Depth of flow = 0.477(Ft.), Average velocity = 3.188(Ft/s)  
Streetflow hydraulics at midpoint of street travel:  
Halfstreet flow width = 19.081(Ft.)  
Flow velocity = 3.19(Ft/s)  
Travel time = 5.23 min. TC = 18.38 min.

Adding area flow to street  
COMMERCIAL subarea type  
Decimal fraction soil group A = 1.000  
Decimal fraction soil group B = 0.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
SCS curve number for soil(AMC 2) = 32.00  
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)  
Rainfall intensity = 2.231(In/Hr) for a 25.0 year storm  
Effective runoff coefficient used for area, (total area with modified  
rational method) (Q=KCIA) is C = 0.861  
Subarea runoff = 16.968(CFS) for 10.000(Ac.)  
Total runoff = 28.802(CFS)  
Effective area this stream = 15.00(Ac.)  
Total Study Area (Main Stream No. 1) = 77.50(Ac.)  
Area averaged Fm value = 0.098(In/Hr)  
Street flow at end of street = 28.802(CFS)  
Half street flow at end of street = 14.401(CFS)  
Depth of flow = 0.504(Ft.), Average velocity = 3.384(Ft/s)  
Note: depth of flow exceeds top of street crown.  
Flow width (from curb towards crown)= 20.000(Ft.)

+++++  
Process from Point/Station 214.000 to Point/Station 214.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 3  
Stream flow area = 15.000(Ac.)  
Runoff from this stream = 28.802(CFS)  
Time of concentration = 18.38 min.

Rainfall intensity = 2.231(In/Hr)  
 Area averaged loss rate (Fm) = 0.0978(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	90.852	19.75	2.137
2	32.397	17.95	2.263
3	28.802	18.38	2.231
Qmax(1) =			
	1.000 *	1.000 *	90.852) +
	0.942 *	1.000 *	32.397) +
	0.956 *	1.000 *	28.802) + = 148.904
Qmax(2) =			
	1.062 *	0.909 *	90.852) +
	1.000 *	1.000 *	32.397) +
	1.015 *	0.977 *	28.802) + = 148.612
Qmax(3) =			
	1.046 *	0.931 *	90.852) +
	0.985 *	1.000 *	32.397) +
	1.000 *	1.000 *	28.802) + = 149.169

Total of 3 streams to confluence:

Flow rates before confluence point:

90.852      32.397      28.802

Maximum flow rates at confluence using above data:

148.904      148.612      149.169

Area of streams before confluence:

44.584      16.500      15.000

Effective area values after confluence:

76.084      71.669      72.987

Results of confluence:

Total flow rate = 149.169(CFS)

Time of concentration = 18.379 min.

Effective stream area after confluence = 72.987(Ac.)

Stream Area average Pervious fraction(Ap) = 0.100

Stream Area average soil loss rate(Fm) = 0.091(In/Hr)

Study area (this main stream) = 76.08(Ac.)

+++++  
 Process from Point/Station 62.000 to Point/Station 63.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1065.000(Ft.)  
 Downstream point/station elevation = 1042.200(Ft.)  
 Pipe length = 1320.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 149.169(CFS)  
 Given pipe size = 54.00(In.)  
 Calculated individual pipe flow = 149.169(CFS)  
 Normal flow depth in pipe = 29.44(In.)  
 Flow top width inside pipe = 53.78(In.)  
 Critical Depth = 42.99(In.)  
 Pipe flow velocity = 16.83(Ft/s)  
 Travel time through pipe = 1.31 min.  
 Time of concentration (TC) = 19.69 min.

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Process from Point/Station      63.000 to Point/Station      63.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 1
Stream flow area =      72.987(Ac.)
Runoff from this stream =   149.169(CFS)
Time of concentration =   19.69 min.
Rainfall intensity =     2.141(In/Hr)
Area averaged loss rate (Fm) =  0.0914(In/Hr)
Area averaged Pervious ratio (Ap) = 0.1000

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Process from Point/Station      215.000 to Point/Station      216.000
**** INITIAL AREA EVALUATION ****

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COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 56.00
Pervious ratio(Ap) = 0.1000      Max loss rate(Fm)=      0.073(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1074.600(Ft.)
Bottom (of initial area) elevation = 1071.000(Ft.)
Difference in elevation =      3.600(Ft.)
Slope =      0.00360  s(%)=      0.36
TC = k(0.304)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 14.846 min.
Rainfall intensity =      2.536(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.874
Subarea runoff =      12.191(CFS)
Total initial stream area =      5.500(Ac.)
Pervious area fraction = 0.100
Initial area Fm value =      0.073(In/Hr)

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Process from Point/Station      216.000 to Point/Station      217.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

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Top of street segment elevation = 1071.000(Ft.)
End of street segment elevation = 1063.700(Ft.)
Length of street segment = 875.000(Ft.)
Height of curb above gutter flowline = 8.0(In.)
Width of half street (curb to crown) = 20.000(Ft.)
Distance from crown to crossfall grade break = 18.500(Ft.)
Slope from gutter to grade break (v/hz) = 0.020
Slope from grade break to crown (v/hz) = 0.020
Street flow is on [2] side(s) of the street
Distance from curb to property line = 10.000(Ft.)
Slope from curb to property line (v/hz) = 0.020
Gutter width = 1.500(Ft.)
Gutter hike from flowline = 1.500(In.)
Manning's N in gutter = 0.0150
Manning's N from gutter to grade break = 0.0150
Manning's N from grade break to crown = 0.0150
Estimated mean flow rate at midpoint of street = 24.382(CFS)

```

Depth of flow = 0.491(Ft.), Average velocity = 3.058(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 19.786(Ft.)  
 Flow velocity = 3.06(Ft/s)  
 Travel time = 4.77 min. TC = 19.61 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.146(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.869  
 Subarea runoff = 18.586(CFS) for 11.000(Ac.)  
 Total runoff = 30.776(CFS)  
 Effective area this stream = 16.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 94.00(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 30.776(CFS)  
 Half street flow at end of street = 15.388(CFS)  
 Depth of flow = 0.522(Ft.), Average velocity = 3.341(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

\*\*\*\*\*  
 Process from Point/Station 217.000 to Point/Station 217.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 16.500(Ac.)  
 Runoff from this stream = 30.776(CFS)  
 Time of concentration = 19.61 min.  
 Rainfall intensity = 2.146(In/Hr)  
 Area averaged loss rate (Fm) = 0.0734(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000

\*\*\*\*\*  
 Process from Point/Station 63.000 to Point/Station 63.000  
 \*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

---

Soil classification AP and SCS values input by user  
 USER INPUT of soil data for subarea  
 SCS curve number for soil(AMC 2) = 54.95  
 Pervious ratio(Ap) = 0.1110 Max loss rate(Fm)= 0.083(In/Hr)  
 Rainfall intensity = 2.049(In/Hr) for a 25.0 year storm  
 User specified values are as follows:  
 TC = 21.19 min. Rain intensity = 2.05(In/Hr)  
 Total area this stream = 203.15(Ac.)  
 Total Study Area (Main Stream No. 1) = 297.15(Ac.)  
 Total runoff = 403.88(CFS)

\*\*\*\*\*  
 Process from Point/Station 63.000 to Point/Station 63.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 203.150(Ac.)  
 Runoff from this stream = 403.880(CFS)  
 Time of concentration = 21.19 min.  
 Rainfall intensity = 2.049(In/Hr)  
 Area averaged loss rate (Fm) = 0.0830(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1110  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	149.169	19.69	2.141
2	30.776	19.61	2.146
3	403.880	21.19	2.049
Qmax(1) =			
	1.000 *	1.000 *	149.169) +
	0.998 *	1.000 *	30.776) +
	1.047 *	0.929 *	403.880) + = 572.752
Qmax(2) =			
	1.002 *	0.996 *	149.169) +
	1.000 *	1.000 *	30.776) +
	1.049 *	0.926 *	403.880) + = 572.081
Qmax(3) =			
	0.955 *	1.000 *	149.169) +
	0.953 *	1.000 *	30.776) +
	1.000 *	1.000 *	403.880) + = 575.650

Total of 3 streams to confluence:  
 Flow rates before confluence point:  
 149.169      30.776      403.880  
 Maximum flow rates at confluence using above data:  
 572.752      572.081      575.650  
 Area of streams before confluence:  
 72.987      16.500      203.150  
 Effective area values after confluence:  
 278.220      277.266      292.637  
 Results of confluence:  
 Total flow rate = 575.650(CFS)  
 Time of concentration = 21.190 min.  
 Effective stream area after confluence = 292.637(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.108  
 Stream Area average soil loss rate(Fm) = 0.085(In/Hr)  
 Study area (this main stream) = 292.64(Ac.)

++++  
 Process from Point/Station 63.000 to Point/Station 64.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1039.100(Ft.)  
 Downstream point/station elevation = 1033.800(Ft.)  
 Pipe length = 1320.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 575.650(CFS)  
 Given pipe size = 90.00(In.)  
 NOTE: Normal flow is pressure flow in user selected pipe size.  
 The approximate hydraulic grade line above the pipe invert is  
 6.071(Ft.) at the headworks or inlet of the pipe(s)  
 Pipe friction loss = 7.416(Ft.)  
 Minor friction loss = 3.955(Ft.) K-factor = 1.50

Pipe flow velocity = 13.03(Ft/s)  
 Travel time through pipe = 1.69 min.  
 Time of concentration (TC) = 22.88 min.

++++  
 Process from Point/Station 64.000 to Point/Station 64.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 292.637(Ac.)  
 Runoff from this stream = 575.650(CFS)  
 Time of concentration = 22.88 min.  
 Rainfall intensity = 1.957(In/Hr)  
 Area averaged loss rate (Fm) = 0.0845(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1076

++++  
 Process from Point/Station 218.000 to Point/Station 219.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1065.500(Ft.)  
 Bottom (of initial area) elevation = 1059.000(Ft.)  
 Difference in elevation = 6.500(Ft.)  
 Slope = 0.00650 s(%) = 0.65  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 16.880 min.  
 Rainfall intensity = 2.348(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.759  
 Subarea runoff = 8.915(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

++++  
 Process from Point/Station 219.000 to Point/Station 220.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1059.000(Ft.)  
 End of street segment elevation = 1056.500(Ft.)  
 Length of street segment = 500.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)

Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 16.048(CFS)  
 Depth of flow = 0.467(Ft.), Average velocity = 2.274(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 18.592(Ft.)  
 Flow velocity = 2.27(Ft/s)  
 Travel time = 3.66 min. TC = 20.54 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 2.087(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.742  
 Subarea runoff = 11.210(CFS) for 8.000(Ac.)  
 Total runoff = 20.126(CFS)  
 Effective area this stream = 13.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 310.15(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 20.126(CFS)  
 Half street flow at end of street = 10.063(CFS)  
 Depth of flow = 0.499(Ft.), Average velocity = 2.419(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 220.000 to Point/Station 221.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1056.500(Ft.)  
 End of street segment elevation = 1051.200(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 30.188(CFS)  
 Depth of flow = 0.658(Ft.), Average velocity = 3.776(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 28.148(Ft.)  
 Flow velocity = 3.78(Ft/s)  
 Travel time = 2.91 min. TC = 23.46 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 1.927(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.729  
 Subarea runoff = 16.391(CFS) for 13.000(Ac.)  
 Total runoff = 36.516(CFS)  
 Effective area this stream = 26.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 323.15(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 36.516(CFS)  
 Half street flow at end of street = 36.516(CFS)  
 Depth of flow = 0.708(Ft.), Average velocity = 3.842(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 2.06(Ft.)  
 Flow width (from curb towards crown)= 30.644(Ft.)

++++++  
 Process from Point/Station 221.000 to Point/Station 221.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 26.000(Ac.)  
 Runoff from this stream = 36.516(CFS)  
 Time of concentration = 23.46 min.  
 Rainfall intensity = 1.927(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	575.650	22.88	1.957
2	36.516	23.46	1.927
Qmax(1) =	1.000 *	1.000 *	575.650) +
	1.019 *	0.975 *	36.516) + = 611.929
Qmax(2) =	0.984 *	1.000 *	575.650) +
	1.000 *	1.000 *	36.516) + = 603.223

Total of 2 streams to confluence:

Flow rates before confluence point:

575.650      36.516

Maximum flow rates at confluence using above data:

611.929      603.223

Area of streams before confluence:

292.637      26.000

Effective area values after confluence:

317.996      318.637

Results of confluence:

Total flow rate = 611.929(CFS)

Time of concentration = 22.878 min.

Effective stream area after confluence = 317.996(Ac.)

Stream Area average Pervious fraction(Ap) = 0.140  
 Stream Area average soil loss rate(Fm) = 0.108(In/Hr)  
 Study area (this main stream) = 318.64(Ac.)

+++++  
 Process from Point/Station 64.000 to Point/Station 71.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1033.800(Ft.)  
 Downstream point/station elevation = 1030.000(Ft.)  
 Pipe length = 660.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 611.929(CFS)  
 Given pipe size = 90.00(In.)  
 Calculated individual pipe flow = 611.929(CFS)  
 Normal flow depth in pipe = 78.75(In.)  
 Flow top width inside pipe = 59.53(In.)  
 Critical Depth = 76.01(In.)  
 Pipe flow velocity = 14.94(Ft/s)  
 Travel time through pipe = 0.74 min.  
 Time of concentration (TC) = 23.61 min.

+++++  
 Process from Point/Station 71.000 to Point/Station 71.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 317.996(Ac.)  
 Runoff from this stream = 611.929(CFS)  
 Time of concentration = 23.61 min.  
 Rainfall intensity = 1.920(In/Hr)  
 Area averaged loss rate (Fm) = 0.1076(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1397

+++++  
 Process from Point/Station 71.000 to Point/Station 71.000  
 \*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

---

Soil classification AP and SCS values input by user  
 USER INPUT of soil data for subarea  
 SCS curve number for soil(AMC 2) = 56.12  
 Pervious ratio(Ap) = 0.4520 Max loss rate(Fm)= 0.331(In/Hr)  
 Rainfall intensity = 1.822(In/Hr) for a 25.0 year storm  
 User specified values are as follows:  
 TC = 25.76 min. Rain intensity = 1.82(In/Hr)  
 Total area this stream = 202.68(Ac.)  
 Total Study Area (Main Stream No. 1) = 525.83(Ac.)  
 Total runoff = 307.34(CFS)

+++++  
 Process from Point/Station 71.000 to Point/Station 71.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 202.680(Ac.)  
 Runoff from this stream = 307.340(CFS)  
 Time of concentration = 25.76 min.  
 Rainfall intensity = 1.822(In/Hr)

Area averaged loss rate (Fm) = 0.3310(In/Hr)  
Area averaged Pervious ratio (Ap) = 0.4520  
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	611.929	23.61	1.920
2	307.340	25.76	1.822
Qmax(1) =			
	1.000 *	1.000 *	611.929) +
	1.065 *	0.917 *	307.340) + = 912.114
Qmax(2) =			
	0.946 *	1.000 *	611.929) +
	1.000 *	1.000 *	307.340) + = 886.319

Total of 2 streams to confluence:  
Flow rates before confluence point:  
611.929 307.340  
Maximum flow rates at confluence using above data:  
912.114 886.319  
Area of streams before confluence:  
317.996 202.680  
Effective area values after confluence:  
503.799 520.676  
Results of confluence:  
Total flow rate = 912.114(CFS)  
Time of concentration = 23.615 min.  
Effective stream area after confluence = 503.799(Ac.)  
Stream Area average Pervious fraction(Ap) = 0.261  
Stream Area average soil loss rate(Fm) = 0.195(In/Hr)  
Study area (this main stream) = 520.68(Ac.)

\*\*\*\*\*  
Process from Point/Station 71.000 to Point/Station 89.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1030.000(Ft.)  
Downstream point/station elevation = 1025.000(Ft.)  
Pipe length = 680.00(Ft.) Manning's N = 0.013  
No. of pipes = 1 Required pipe flow = 912.114(CFS)  
Given pipe size = 108.00(In.)  
Calculated individual pipe flow = 912.114(CFS)  
Normal flow depth in pipe = 76.59(In.)  
Flow top width inside pipe = 98.09(In.)  
Critical Depth = 89.02(In.)  
Pipe flow velocity = 18.90(Ft/s)  
Travel time through pipe = 0.60 min.  
Time of concentration (TC) = 24.21 min.

\*\*\*\*\*  
Process from Point/Station 89.000 to Point/Station 89.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
Stream flow area = 503.799(Ac.)  
Runoff from this stream = 912.114(CFS)  
Time of concentration = 24.21 min.

Rainfall intensity = 1.891(In/Hr)  
 Area averaged loss rate (Fm) = 0.1946(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.2612

+++++  
 Process from Point/Station 89.000 to Point/Station 89.000  
 \*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

Soil classification AP and SCS values input by user  
 USER INPUT of soil data for subarea  
 SCS curve number for soil(AMC 2) = 74.49  
 Pervious ratio(Ap) = 0.8260 Max loss rate(Fm)= 0.381(In/Hr)  
 Rainfall intensity = 2.805(In/Hr) for a 25.0 year storm  
 User specified values are as follows:  
 TC = 12.55 min. Rain intensity = 2.81(In/Hr)  
 Total area this stream = 316.80(Ac.)  
 Total Study Area (Main Stream No. 1) = 842.63(Ac.)  
 Total runoff = 795.18(CFS)

+++++  
 Process from Point/Station 89.000 to Point/Station 89.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 316.800(Ac.)  
 Runoff from this stream = 795.180(CFS)  
 Time of concentration = 12.55 min.  
 Rainfall intensity = 2.805(In/Hr)  
 Area averaged loss rate (Fm) = 0.3810(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.8260  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	912.114	24.21	1.891
2	795.180	12.55	2.805
Qmax(1) =			
	1.000 *	1.000 *	912.114) +
	0.623 *	1.000 *	795.180) + = 1407.437
Qmax(2) =			
	1.539 *	0.518 *	912.114) +
	1.000 *	1.000 *	795.180) + = 1522.641

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 912.114 795.180  
 Maximum flow rates at confluence using above data:  
 1407.437 1522.641  
 Area of streams before confluence:  
 503.799 316.800  
 Effective area values after confluence:  
 820.599 577.909  
 Results of confluence:  
 Total flow rate = 1522.641(CFS)  
 Time of concentration = 12.550 min.  
 Effective stream area after confluence = 577.909(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.479

Stream Area average soil loss rate(Fm) = 0.267(In/Hr)  
Study area (this main stream) = 820.60(Ac.)  
End of computations, Total Study Area = 842.63 (Ac.)  
The following figures may  
be used for a unit hydrograph study of the same area.  
Note: These figures do not consider reduced effective area  
effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.473  
Area averaged SCS curve number = 61.1

LINE "DZ-4"

## San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
 Rational Hydrology Study Date: 08/03/04

-----  
 FONTANA / LINE DZ-4 HYDROLOGY  
 25 YEAR STORM  
 JN 04339  
 -----

Hall & Forman, Inc. - S/N 950  
 -----

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*  
 -----

Rational hydrology study storm event year is 25.0  
 10 Year storm 1 hour rainfall = 0.930 (In.)  
 100 Year storm 1 hour rainfall = 1.350 (In.)  
 Computed rainfall intensity:  
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
 Slope used for rainfall intensity curve b = 0.6000  
 Soil antecedent moisture condition (AMC) = 2

\*\*\*\*\*  
 Process from Point/Station 600.000 to Point/Station 601.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*  
 -----

COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 56.00  
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.073 (In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000 (Ft.)  
 Top (of initial area) elevation = 1065.000 (Ft.)  
 Bottom (of initial area) elevation = 1060.000 (Ft.)  
 Difference in elevation = 5.000 (Ft.)  
 Slope = 0.00500 s(%) = 0.50  
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.902 min.  
 Rainfall intensity = 2.638 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875  
 Subarea runoff = 11.541 (CFS)  
 Total initial stream area = 5.000 (Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073 (In/Hr)

\*\*\*\*\*  
 Process from Point/Station 601.000 to Point/Station 602.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*  
 -----

Top of street segment elevation = 1060.000 (Ft.)  
 End of street segment elevation = 1058.300 (Ft.)

Length of street segment = 330.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 17.312(CFS)  
 Depth of flow = 0.476(Ft.), Average velocity = 2.344(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 19.032(Ft.)  
 Flow velocity = 2.34(Ft/s)  
 Travel time = 2.35 min. TC = 16.25 min.

Adding area flow to street

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.073(In/Hr)  
 Rainfall intensity = 2.402(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.873  
 Subarea runoff = 9.420(CFS) for 5.000(Ac.)  
 Total runoff = 20.962(CFS)  
 Effective area this stream = 10.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 10.00(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 20.962(CFS)  
 Half street flow at end of street = 10.481(CFS)  
 Depth of flow = 0.503(Ft.), Average velocity = 2.480(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 602.000 to Point/Station 603.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1058.300(Ft.)  
 End of street segment elevation = 1055.000(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)

Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 31.443 (CFS)  
 Depth of flow = 0.564 (Ft.), Average velocity = 2.888 (Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000 (Ft.)  
 Flow velocity = 2.89 (Ft/s)  
 Travel time = 3.81 min. TC = 20.06 min.

Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 56.00  
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.073 (In/Hr)  
 Rainfall intensity = 2.117 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.869  
 Subarea runoff = 15.828 (CFS) for 10.000 (Ac.)  
 Total runoff = 36.790 (CFS)  
 Effective area this stream = 20.00 (Ac.)  
 Total Study Area (Main Stream No. 1) = 20.00 (Ac.)  
 Area averaged Fm value = 0.073 (In/Hr)  
 Street flow at end of street = 36.790 (CFS)  
 Half street flow at end of street = 18.395 (CFS)  
 Depth of flow = 0.591 (Ft.), Average velocity = 3.073 (Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown) = 20.000 (Ft.)

\*\*\*\*\*  
 Process from Point/Station 603.000 to Point/Station 607.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1055.000 (Ft.)  
 End of street segment elevation = 1052.000 (Ft.)  
 Length of street segment = 660.000 (Ft.)  
 Height of curb above gutter flowline = 8.0 (In.)  
 Width of half street (curb to crown) = 42.000 (Ft.)  
 Distance from crown to crossfall grade break = 40.500 (Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000 (Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500 (Ft.)  
 Gutter hike from flowline = 1.500 (In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 36.790 (CFS)  
 Depth of flow = 0.784 (Ft.), Average velocity = 2.991 (Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 5.89 (Ft.)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 34.469 (Ft.)  
 Flow velocity = 2.99 (Ft/s)

Travel time = 3.68 min. TC = 23.74 min.

Adding area flow to street

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 56.00

Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073 (In/Hr)

Rainfall intensity = 1.914 (In/Hr) for a 25.0 year storm

Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.865

Subarea runoff = 0.000 (CFS) for 0.000 (Ac.)

Total runoff = 36.790 (CFS)

Effective area this stream = 20.00 (Ac.)

Total Study Area (Main Stream No. 1) = 20.00 (Ac.)

Area averaged Fm value = 0.073 (In/Hr)

Street flow at end of street = 36.790 (CFS)

Half street flow at end of street = 36.790 (CFS)

Depth of flow = 0.784 (Ft.), Average velocity = 2.991 (Ft/s)

Warning: depth of flow exceeds top of curb

Distance that curb overflow reaches into property = 5.89 (Ft.)

Flow width (from curb towards crown) = 34.469 (Ft.)

\*\*\*\*\*  
 Process from Point/Station 607.000 to Point/Station 607.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 20.000 (Ac.)

Runoff from this stream = 36.790 (CFS)

Time of concentration = 23.74 min.

Rainfall intensity = 1.914 (In/Hr)

Area averaged loss rate (Fm) = 0.0734 (In/Hr)

Area averaged Pervious ratio (Ap) = 0.1000

\*\*\*\*\*  
 Process from Point/Station 604.000 to Point/Station 605.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 56.00

Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073 (In/Hr)

Initial subarea data:

Initial area flow distance = 1000.000 (Ft.)

Top (of initial area) elevation = 1062.900 (Ft.)

Bottom (of initial area) elevation = 1057.900 (Ft.)

Difference in elevation = 5.000 (Ft.)

Slope = 0.00500 s(%) = 0.50

TC = k(0.304)\*[(length^3)/(elevation change)]^0.2

Initial area time of concentration = 13.902 min.

Rainfall intensity = 2.638 (In/Hr) for a 25.0 year storm

Effective runoff coefficient used for area (Q=KCIA) is C = 0.875

Subarea runoff = 11.541 (CFS)

Total initial stream area = 5.000 (Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073 (In/Hr)

\*\*\*\*\*  
 Process from Point/Station 605.000 to Point/Station 606.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1057.900 (Ft.)  
 End of street segment elevation = 1055.900 (Ft.)  
 Length of street segment = 330.000 (Ft.)  
 Height of curb above gutter flowline = 8.0 (In.)  
 Width of half street (curb to crown) = 20.000 (Ft.)  
 Distance from crown to crossfall grade break = 18.500 (Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000 (Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500 (Ft.)  
 Gutter hike from flowline = 1.500 (In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 17.312 (CFS)  
 Depth of flow = 0.464 (Ft.), Average velocity = 2.492 (Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 18.447 (Ft.)  
 Flow velocity = 2.49 (Ft/s)  
 Travel time = 2.21 min. TC = 16.11 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 56.00  
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.073 (In/Hr)  
 Rainfall intensity = 2.415 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.873  
 Subarea runoff = 9.532 (CFS) for 5.000 (Ac.)  
 Total runoff = 21.074 (CFS)  
 Effective area this stream = 10.00 (Ac.)  
 Total Study Area (Main Stream No. 1) = 30.00 (Ac.)  
 Area averaged Fm value = 0.073 (In/Hr)  
 Street flow at end of street = 21.074 (CFS)  
 Half street flow at end of street = 10.537 (CFS)  
 Depth of flow = 0.493 (Ft.), Average velocity = 2.616 (Ft/s)  
 Flow width (from curb towards crown) = 19.892 (Ft.)

\*\*\*\*\*  
 Process from Point/Station 606.000 to Point/Station 607.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1055.900 (Ft.)  
 End of street segment elevation = 1052.000 (Ft.)  
 Length of street segment = 660.000 (Ft.)

Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 31.611(CFS)  
 Depth of flow = 0.551(Ft.), Average velocity = 3.043(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 3.04(Ft/s)  
 Travel time = 3.61 min. TC = 19.72 min.  
 Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm) = 0.257(In/Hr)  
 Rainfall intensity = 2.139(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.831  
 Subarea runoff = 14.451(CFS) for 10.000(Ac.)  
 Total runoff = 35.524(CFS)  
 Effective area this stream = 20.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 40.00(Ac.)  
 Area averaged Fm value = 0.165(In/Hr)  
 Street flow at end of street = 35.524(CFS)  
 Half street flow at end of street = 17.762(CFS)  
 Depth of flow = 0.570(Ft.), Average velocity = 3.187(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown) = 20.000(Ft.)

++++++  
 Process from Point/Station 607.000 to Point/Station 607.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 20.000(Ac.)  
 Runoff from this stream = 35.524(CFS)  
 Time of concentration = 19.72 min.  
 Rainfall intensity = 2.139(In/Hr)  
 Area averaged loss rate (Fm) = 0.1651(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.2250  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
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1	36.790	23.74	1.914
2	35.524	19.72	2.139
Qmax(1) =			
	1.000 *	1.000 *	36.790) +
	0.886 *	1.000 *	35.524) + = 68.267
Qmax(2) =			
	1.122 *	0.831 *	36.790) +
	1.000 *	1.000 *	35.524) + = 69.831

Total of 2 streams to confluence:

Flow rates before confluence point:

36.790          35.524

Maximum flow rates at confluence using above data:

68.267          69.831

Area of streams before confluence:

20.000          20.000

Effective area values after confluence:

40.000          36.620

Results of confluence:

Total flow rate = 69.831(CFS)

Time of concentration = 19.724 min.

Effective stream area after confluence = 36.620(Ac.)

Stream Area average Pervious fraction(Ap) = 0.163

Stream Area average soil loss rate(Fm) = 0.119(In/Hr)

Study area (this main stream) = 40.00(Ac.)

\*\*\*\*\*  
 Process from Point/Station          607.000 to Point/Station          45.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1047.000(Ft.)  
 Downstream point/station elevation = 1041.000(Ft.)  
 Pipe length = 660.00(Ft.)      Manning's N = 0.013  
 No. of pipes = 1      Required pipe flow = 69.831(CFS)  
 Given pipe size = 42.00(In.)  
 Calculated individual pipe flow = 69.831(CFS)  
 Normal flow depth in pipe = 26.58(In.)  
 Flow top width inside pipe = 40.49(In.)  
 Critical Depth = 31.40(In.)  
 Pipe flow velocity = 10.88(Ft/s)  
 Travel time through pipe = 1.01 min.  
 Time of concentration (TC) = 20.74 min.

\*\*\*\*\*  
 Process from Point/Station          45.000 to Point/Station          45.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 36.620(Ac.)  
 Runoff from this stream = 69.831(CFS)  
 Time of concentration = 20.74 min.  
 Rainfall intensity = 2.075(In/Hr)  
 Area averaged loss rate (Fm) = 0.1193(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1625

\*\*\*\*\*  
 Process from Point/Station          608.000 to Point/Station          609.000

\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000      Max loss rate(Fm) =      0.073 (In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000 (Ft.)  
 Top (of initial area) elevation = 1060.800 (Ft.)  
 Bottom (of initial area) elevation = 1055.800 (Ft.)  
 Difference in elevation = 5.000 (Ft.)  
 Slope = 0.00500 s(%) = 0.50  
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.902 min.  
 Rainfall intensity = 2.638 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875  
 Subarea runoff = 11.541 (CFS)  
 Total initial stream area = 5.000 (Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073 (In/Hr)

+++++  
 Process from Point/Station 609.000 to Point/Station 610.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1055.800 (Ft.)  
 End of street segment elevation = 1053.500 (Ft.)  
 Length of street segment = 330.000 (Ft.)  
 Height of curb above gutter flowline = 8.0 (In.)  
 Width of half street (curb to crown) = 20.000 (Ft.)  
 Distance from crown to crossfall grade break = 18.500 (Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000 (Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500 (Ft.)  
 Gutter hike from flowline = 1.500 (In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 17.312 (CFS)  
 Depth of flow = 0.454 (Ft.), Average velocity = 2.626 (Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 17.958 (Ft.)  
 Flow velocity = 2.63 (Ft/s)  
 Travel time = 2.09 min.      TC = 16.00 min.

Adding area flow to street

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000      Max loss rate(Fm) =      0.073 (In/Hr)  
 Rainfall intensity = 2.425 (In/Hr) for a 25.0 year storm

Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.873  
 Subarea runoff = 9.624 (CFS) for 5.000 (Ac.)  
 Total runoff = 21.166 (CFS)  
 Effective area this stream = 10.00 (Ac.)  
 Total Study Area (Main Stream No. 1) = 50.00 (Ac.)  
 Area averaged Fm value = 0.073 (In/Hr)  
 Street flow at end of street = 21.166 (CFS)  
 Half street flow at end of street = 10.583 (CFS)  
 Depth of flow = 0.483 (Ft.), Average velocity = 2.760 (Ft/s)  
 Flow width (from curb towards crown) = 19.399 (Ft.)

\*\*\*\*\*  
 Process from Point/Station 610.000 to Point/Station 611.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1053.500 (Ft.)  
 End of street segment elevation = 1049.000 (Ft.)  
 Length of street segment = 660.000 (Ft.)  
 Height of curb above gutter flowline = 8.0 (In.)  
 Width of half street (curb to crown) = 20.000 (Ft.)  
 Distance from crown to crossfall grade break = 18.500 (Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000 (Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500 (Ft.)  
 Gutter hike from flowline = 1.500 (In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 31.749 (CFS)  
 Depth of flow = 0.541 (Ft.), Average velocity = 3.183 (Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000 (Ft.)  
 Flow velocity = 3.18 (Ft/s)  
 Travel time = 3.46 min. TC = 19.45 min.  
 Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 56.00  
 Pervious ratio (Ap) = 0.3500 Max loss rate (Fm) = 0.257 (In/Hr)  
 Rainfall intensity = 2.157 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.831  
 Subarea runoff = 14.680 (CFS) for 10.000 (Ac.)  
 Total runoff = 35.846 (CFS)  
 Effective area this stream = 20.00 (Ac.)  
 Total Study Area (Main Stream No. 1) = 60.00 (Ac.)  
 Area averaged Fm value = 0.165 (In/Hr)  
 Street flow at end of street = 35.846 (CFS)  
 Half street flow at end of street = 17.923 (CFS)  
 Depth of flow = 0.560 (Ft.), Average velocity = 3.340 (Ft/s)  
 Note: depth of flow exceeds top of street crown.

Flow width (from curb towards crown) = 20.000 (Ft.)

\*\*\*\*\*  
 Process from Point/Station 611.000 to Point/Station 611.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 20.000 (Ac.)  
 Runoff from this stream = 35.846 (CFS)  
 Time of concentration = 19.45 min.  
 Rainfall intensity = 2.157 (In/Hr)  
 Area averaged loss rate (Fm) = 0.1651 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.2250  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	69.831	20.74	2.075
2	35.846	19.45	2.157
Qmax(1) =			
	1.000 *	1.000 *	69.831) +
	0.959 *	1.000 *	35.846) + = 104.218
Qmax(2) =			
	1.041 *	0.938 *	69.831) +
	1.000 *	1.000 *	35.846) + = 104.072

Total of 2 streams to confluence:  
 Flow rates before confluence point:

69.831 35.846

Maximum flow rates at confluence using above data:

104.218 104.072

Area of streams before confluence:

36.620 20.000

Effective area values after confluence:

56.620 54.354

Results of confluence:

Total flow rate = 104.218 (CFS)

Time of concentration = 20.736 min.

Effective stream area after confluence = 56.620 (Ac.)

Stream Area average Pervious fraction (Ap) = 0.185

Stream Area average soil loss rate (Fm) = 0.135 (In/Hr)

Study area (this main stream) = 56.62 (Ac.)

\*\*\*\*\*  
 Process from Point/Station 45.000 to Point/Station 90.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1040.000 (Ft.)  
 Downstream point/station elevation = 1025.000 (Ft.)  
 Pipe length = 750.00 (Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 104.218 (CFS)  
 Given pipe size = 54.00 (In.)  
 Calculated individual pipe flow = 104.218 (CFS)  
 Normal flow depth in pipe = 22.90 (In.)  
 Flow top width inside pipe = 53.37 (In.)  
 Critical Depth = 35.99 (In.)

Pipe flow velocity = 16.23 (Ft/s)  
 Travel time through pipe = 0.77 min.  
 Time of concentration (TC) = 21.51 min.

\*\*\*\*\*  
 Process from Point/Station 90.000 to Point/Station 90.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 56.620 (Ac.)  
 Runoff from this stream = 104.218 (CFS)  
 Time of concentration = 21.51 min.  
 Rainfall intensity = 2.031 (In/Hr)  
 Area averaged loss rate (Fm) = 0.1355 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1846

\*\*\*\*\*  
 Process from Point/Station 612.000 to Point/Station 613.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 56.00  
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.073 (In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000 (Ft.)  
 Top (of initial area) elevation = 1058.700 (Ft.)  
 Bottom (of initial area) elevation = 1053.700 (Ft.)  
 Difference in elevation = 5.000 (Ft.)  
 Slope = 0.00500 s(%) = 0.50  
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$   
 Initial area time of concentration = 13.902 min.  
 Rainfall intensity = 2.638 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.875  
 Subarea runoff = 11.541 (CFS)  
 Total initial stream area = 5.000 (Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.073 (In/Hr)

\*\*\*\*\*  
 Process from Point/Station 613.000 to Point/Station 614.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1053.700 (Ft.)  
 End of street segment elevation = 1051.100 (Ft.)  
 Length of street segment = 330.000 (Ft.)  
 Height of curb above gutter flowline = 8.0 (In.)  
 Width of half street (curb to crown) = 20.000 (Ft.)  
 Distance from crown to crossfall grade break = 18.500 (Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000 (Ft.)  
 Slope from curb to property line (v/hz) = 0.020

Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 17.312(CFS)  
 Depth of flow = 0.446(Ft.), Average velocity = 2.750(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 17.539(Ft.)  
 Flow velocity = 2.75(Ft/s)  
 Travel time = 2.00 min. TC = 15.90 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm) = 0.073(In/Hr)  
 Rainfall intensity = 2.434(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.873  
 Subarea runoff = 9.702(CFS) for 5.000(Ac.)  
 Total runoff = 21.244(CFS)  
 Effective area this stream = 10.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 70.00(Ac.)  
 Area averaged Fm value = 0.073(In/Hr)  
 Street flow at end of street = 21.244(CFS)  
 Half street flow at end of street = 10.622(CFS)  
 Depth of flow = 0.474(Ft.), Average velocity = 2.893(Ft/s)  
 Flow width (from curb towards crown) = 18.975(Ft.)

++++++  
 Process from Point/Station 614.000 to Point/Station 615.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1051.100(Ft.)  
 End of street segment elevation = 1046.000(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 31.865(CFS)  
 Depth of flow = 0.532(Ft.), Average velocity = 3.310(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 3.31(Ft/s)  
 Travel time = 3.32 min. TC = 19.23 min.

Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.257(In/Hr)  
 Rainfall intensity = 2.172(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.832  
 Subarea runoff = 14.877(CFS) for 10.000(Ac.)  
 Total runoff = 36.121(CFS)  
 Effective area this stream = 20.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 80.00(Ac.)  
 Area averaged Fm value = 0.165(In/Hr)  
 Street flow at end of street = 36.121(CFS)  
 Half street flow at end of street = 18.060(CFS)  
 Depth of flow = 0.551(Ft.), Average velocity = 3.479(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

\*\*\*\*\*  
 Process from Point/Station 615.000 to Point/Station 615.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2

Stream flow area = 20.000(Ac.)  
 Runoff from this stream = 36.121(CFS)  
 Time of concentration = 19.23 min.  
 Rainfall intensity = 2.172(In/Hr)  
 Area averaged loss rate (Fm) = 0.1651(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.2250  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	104.218	21.51	2.031
2	36.121	19.23	2.172
Qmax(1) =			
	1.000 *	1.000 *	104.218) +
	0.930 *	1.000 *	36.121) + = 137.795
Qmax(2) =			
	1.075 *	0.894 *	104.218) +
	1.000 *	1.000 *	36.121) + = 136.232

Total of 2 streams to confluence:

Flow rates before confluence point:

104.218      36.121

Maximum flow rates at confluence using above data:

137.795      136.232

Area of streams before confluence:

56.620      20.000

Effective area values after confluence:

76.620      70.615

Results of confluence:

Total flow rate = 137.795(CFS)

Time of concentration = 21.506 min.  
Effective stream area after confluence = 76.620 (Ac.)  
Stream Area average Pervious fraction( $A_p$ ) = 0.195  
Stream Area average soil loss rate( $F_m$ ) = 0.143 (In/Hr)  
Study area (this main stream) = 76.62 (Ac.)  
End of computations, Total Study Area = 80.00 (Ac.)

The following figures may  
be used for a unit hydrograph study of the same area.  
Note: These figures do not consider reduced effective area  
effects caused by confluences in the rational equation.

Area averaged pervious area fraction( $A_p$ ) = 0.194  
Area averaged SCS curve number = 56.0

LINE "DZ-4A"

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
Rational Hydrology Study Date: 08/03/04

-----  
FONTANA / LINE DZ-4A HYDROLOGY  
25 YEAR STORM  
JN 04339  
-----

Hall & Forman, Inc. - S/N 950  
-----

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

-----  
Rational hydrology study storm event year is 25.0  
10 Year storm 1 hour rainfall = 0.930(In.)  
100 Year storm 1 hour rainfall = 1.350(In.)  
Computed rainfall intensity:  
Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
Slope used for rainfall intensity curve b = 0.6000  
Soil antecedent moisture condition (AMC) = 2

-----  
\*\*\*\*\*  
Process from Point/Station 625.000 to Point/Station 626.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*  
-----

RESIDENTIAL(5 - 7 dwl/acre)  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
SCS curve number for soil(AMC 2) = 56.00  
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367(In/Hr)  
Initial subarea data:  
Initial area flow distance = 1000.000(Ft.)  
Top (of initial area) elevation = 1058.000(Ft.)  
Bottom (of initial area) elevation = 1051.300(Ft.)  
Difference in elevation = 6.700(Ft.)  
Slope = 0.00670 s(%) = 0.67  
TC = k(0.389)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 16.778 min.  
Rainfall intensity = 2.357(In/Hr) for a 25.0 year storm  
Effective runoff coefficient used for area (Q=KCIA) is C = 0.760  
Subarea runoff = 8.954(CFS)  
Total initial stream area = 5.000(Ac.)  
Pervious area fraction = 0.500  
Initial area Fm value = 0.367(In/Hr)

-----  
\*\*\*\*\*  
Process from Point/Station 626.000 to Point/Station 627.000  
\*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*  
-----

Top of street segment elevation = 1051.300(Ft.)  
End of street segment elevation = 1049.000(Ft.)

Length of street segment = 330.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 13.431(CFS)  
 Depth of flow = 0.421(Ft.), Average velocity = 2.467(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 16.282(Ft.)  
 Flow velocity = 2.47(Ft/s)  
 Travel time = 2.23 min. TC = 19.01 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367(In/Hr)  
 Rainfall intensity = 2.187(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.749  
 Subarea runoff = 7.424(CFS) for 5.000(Ac.)  
 Total runoff = 16.378(CFS)  
 Effective area this stream = 10.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 10.00(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 16.378(CFS)  
 Half street flow at end of street = 8.189(CFS)  
 Depth of flow = 0.447(Ft.), Average velocity = 2.591(Ft/s)  
 Flow width (from curb towards crown) = 17.578(Ft.)

++++++  
 Process from Point/Station 627.000 to Point/Station 628.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1049.000(Ft.)  
 End of street segment elevation = 1044.600(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150

Manning's N from gutter to grade break = 0.0150  
Manning's N from grade break to crown = 0.0150  
Estimated mean flow rate at midpoint of street = 24.567(CFS)  
Depth of flow = 0.507(Ft.), Average velocity = 2.855(Ft/s)  
Note: depth of flow exceeds top of street crown.  
Streetflow hydraulics at midpoint of street travel:  
Halfstreet flow width = 20.000(Ft.)  
Flow velocity = 2.86(Ft/s)  
Travel time = 3.85 min. TC = 22.86 min.  
Adding area flow to street  
RESIDENTIAL(5 - 7 dwl/acre)  
Decimal fraction soil group A = 0.000  
Decimal fraction soil group B = 1.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
SCS curve number for soil(AMC 2) = 56.00  
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
Rainfall intensity = 1.958(In/Hr) for a 25.0 year storm  
Effective runoff coefficient used for area, (total area with modified  
rational method) (Q=KCIA) is C = 0.731  
Subarea runoff = 12.252(CFS) for 10.000(Ac.)  
Total runoff = 28.630(CFS)  
Effective area this stream = 20.00(Ac.)  
Total Study Area (Main Stream No. 1) = 20.00(Ac.)  
Area averaged Fm value = 0.367(In/Hr)  
Street flow at end of street = 28.630(CFS)  
Half street flow at end of street = 14.315(CFS)  
Depth of flow = 0.527(Ft.), Average velocity = 3.034(Ft/s)  
Note: depth of flow exceeds top of street crown.  
Flow width (from curb towards crown)= 20.000(Ft.)

\*\*\*\*\*  
Process from Point/Station 628.000 to Point/Station 629.000  
\*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1044.600(Ft.)  
End of street segment elevation = 1040.300(Ft.)  
Length of street segment = 660.000(Ft.)  
Height of curb above gutter flowline = 8.0(In.)  
Width of half street (curb to crown) = 42.000(Ft.)  
Distance from crown to crossfall grade break = 40.500(Ft.)  
Slope from gutter to grade break (v/hz) = 0.020  
Slope from grade break to crown (v/hz) = 0.020  
Street flow is on [1] side(s) of the street  
Distance from curb to property line = 13.000(Ft.)  
Slope from curb to property line (v/hz) = 0.020  
Gutter width = 1.500(Ft.)  
Gutter hike from flowline = 1.500(In.)  
Manning's N in gutter = 0.0150  
Manning's N from gutter to grade break = 0.0150  
Manning's N from grade break to crown = 0.0150  
Estimated mean flow rate at midpoint of street = 42.945(CFS)  
Depth of flow = 0.778(Ft.), Average velocity = 3.568(Ft/s)  
Warning: depth of flow exceeds top of curb  
Distance that curb overflow reaches into property = 5.56(Ft.)  
Streetflow hydraulics at midpoint of street travel:  
Halfstreet flow width = 34.140(Ft.)  
Flow velocity = 3.57(Ft/s)  
Travel time = 3.08 min. TC = 25.94 min.

Adding area flow to street

RESIDENTIAL(5 - 7 dwl/acre)

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 56.00

Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)

Rainfall intensity = 1.814(In/Hr) for a 25.0 year storm

Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.718

Subarea runoff = 23.479(CFS) for 20.000(Ac.)

Total runoff = 52.109(CFS)

Effective area this stream = 40.00(Ac.)

Total Study Area (Main Stream No. 1) = 40.00(Ac.)

Area averaged Fm value = 0.367(In/Hr)

Street flow at end of street = 52.109(CFS)

Half street flow at end of street = 52.109(CFS)

Depth of flow = 0.828(Ft.), Average velocity = 3.678(Ft/s)

Warning: depth of flow exceeds top of curb

Distance that curb overflow reaches into property = 8.08(Ft.)

Flow width (from curb towards crown)= 36.667(Ft.)

\*\*\*\*\*  
 Process from Point/Station 629.000 to Point/Station 46.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1033.300(Ft.)  
 Downstream point/station elevation = 1026.000(Ft.)  
 Pipe length = 660.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 52.109(CFS)  
 Given pipe size = 36.00(In.)  
 Calculated individual pipe flow = 52.109(CFS)  
 Normal flow depth in pipe = 23.11(In.)  
 Flow top width inside pipe = 34.52(In.)  
 Critical Depth = 28.15(In.)  
 Pipe flow velocity = 10.87(Ft/s)  
 Travel time through pipe = 1.01 min.  
 Time of concentration (TC) = 26.95 min.

\*\*\*\*\*  
 Process from Point/Station 629.000 to Point/Station 46.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 40.000(Ac.)  
 Runoff from this stream = 52.109(CFS)  
 Time of concentration = 26.95 min.  
 Rainfall intensity = 1.773(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000

\*\*\*\*\*  
 Process from Point/Station 630.000 to Point/Station 631.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)

Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1052.200(Ft.)  
 Bottom (of initial area) elevation = 1044.000(Ft.)  
 Difference in elevation = 8.200(Ft.)  
 Slope = 0.00820    s(%)= 0.82  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 16.113 min.  
 Rainfall intensity = 2.415(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.763  
 Subarea runoff = 9.214(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

++++++  
 Process from Point/Station      631.000 to Point/Station      632.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1044.000(Ft.)  
 End of street segment elevation = 1041.300(Ft.)  
 Length of street segment = 330.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 13.821(CFS)  
 Depth of flow = 0.414(Ft.), Average velocity = 2.639(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 15.960(Ft.)  
 Flow velocity = 2.64(Ft/s)  
 Travel time = 2.08 min.      TC = 18.20 min.

Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)  
 Rainfall intensity = 2.245(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.753  
 Subarea runoff = 7.685(CFS) for 5.000(Ac.)

Total runoff = 16.899 (CFS)  
 Effective area this stream = 10.00 (Ac.)  
 Total Study Area (Main Stream No. 1) = 50.00 (Ac.)  
 Area averaged Fm value = 0.367 (In/Hr)  
 Street flow at end of street = 16.899 (CFS)  
 Half street flow at end of street = 8.449 (CFS)  
 Depth of flow = 0.440 (Ft.), Average velocity = 2.773 (Ft/s)  
 Flow width (from curb towards crown) = 17.250 (Ft.)

++++++  
 Process from Point/Station 632.000 to Point/Station 633.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1041.300 (Ft.)  
 End of street segment elevation = 1035.900 (Ft.)  
 Length of street segment = 660.000 (Ft.)  
 Height of curb above gutter flowline = 8.0 (In.)  
 Width of half street (curb to crown) = 20.000 (Ft.)  
 Distance from crown to crossfall grade break = 18.500 (Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000 (Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500 (Ft.)  
 Gutter hike from flowline = 1.500 (In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 25.348 (CFS)  
 Depth of flow = 0.498 (Ft.), Average velocity = 3.075 (Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000 (Ft.)  
 Flow velocity = 3.07 (Ft/s)  
 Travel time = 3.58 min. TC = 21.77 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367 (In/Hr)  
 Rainfall intensity = 2.015 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.736  
 Subarea runoff = 12.774 (CFS) for 10.000 (Ac.)  
 Total runoff = 29.673 (CFS)  
 Effective area this stream = 20.00 (Ac.)  
 Total Study Area (Main Stream No. 1) = 60.00 (Ac.)  
 Area averaged Fm value = 0.367 (In/Hr)  
 Street flow at end of street = 29.673 (CFS)  
 Half street flow at end of street = 14.837 (CFS)  
 Depth of flow = 0.518 (Ft.), Average velocity = 3.273 (Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown) = 20.000 (Ft.)

\*\*\*\*\*  
 Process from Point/Station 633.000 to Point/Station 633.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 20.000 (Ac.)  
 Runoff from this stream = 29.673 (CFS)  
 Time of concentration = 21.77 min.  
 Rainfall intensity = 2.015 (In/Hr)  
 Area averaged loss rate (Fm) = 0.3670 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	52.109	26.95	1.773
2	29.673	21.77	2.015
Qmax(1) =			
	1.000 *	1.000 *	52.109) +
	0.853 *	1.000 *	29.673) + = 77.421
Qmax(2) =			
	1.172 *	0.808 *	52.109) +
	1.000 *	1.000 *	29.673) + = 79.019

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 52.109      29.673  
 Maximum flow rates at confluence using above data:  
 77.421      79.019  
 Area of streams before confluence:  
 40.000      20.000  
 Effective area values after confluence:  
 60.000      52.313  
 Results of confluence:  
 Total flow rate = 79.019 (CFS)  
 Time of concentration = 21.775 min.  
 Effective stream area after confluence = 52.313 (Ac.)  
 Stream Area average Pervious fraction (Ap) = 0.500  
 Stream Area average soil loss rate (Fm) = 0.367 (In/Hr)  
 Study area (this main stream) = 60.00 (Ac.)

\*\*\*\*\*  
 Process from Point/Station 46.000 to Point/Station 91.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1026.000 (Ft.)  
 Downstream point/station elevation = 1014.500 (Ft.)  
 Pipe length = 750.00 (Ft.)      Manning's N = 0.013  
 No. of pipes = 1      Required pipe flow = 79.019 (CFS)  
 Given pipe size = 60.00 (In.)  
 Calculated individual pipe flow = 79.019 (CFS)  
 Normal flow depth in pipe = 20.23 (In.)  
 Flow top width inside pipe = 56.73 (In.)  
 Critical Depth = 30.19 (In.)  
 Pipe flow velocity = 13.58 (Ft/s)  
 Travel time through pipe = 0.92 min.  
 Time of concentration (TC) = 22.70 min.

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+++++
Process from Point/Station      91.000 to Point/Station      91.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 1
Stream flow area =      52.313(Ac.)
Runoff from this stream =      79.019(CFS)
Time of concentration =      22.70 min.
Rainfall intensity =      1.966(In/Hr)
Area averaged loss rate (Fm) =      0.3670(In/Hr)
Area averaged Pervious ratio (Ap) = 0.5000

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+++++
Process from Point/Station      634.000 to Point/Station      635.000
**** INITIAL AREA EVALUATION ****

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RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 56.00
Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1046.800(Ft.)
Bottom (of initial area) elevation = 1041.800(Ft.)
Difference in elevation =      5.000(Ft.)
Slope =      0.00500 s(%)=      0.50
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 17.789 min.
Rainfall intensity =      2.275(In/Hr) for a      25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
Subarea runoff =      10.306(CFS)
Total initial stream area =      6.000(Ac.)
Pervious area fraction = 0.500
Initial area Fm value =      0.367(In/Hr)

```

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+++++
Process from Point/Station      635.000 to Point/Station      636.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

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```

Top of street segment elevation = 1041.800(Ft.)
End of street segment elevation = 1037.800(Ft.)
Length of street segment = 330.000(Ft.)
Height of curb above gutter flowline = 8.0(In.)
Width of half street (curb to crown) = 20.000(Ft.)
Distance from crown to crossfall grade break = 18.500(Ft.)
Slope from gutter to grade break (v/hz) = 0.020
Slope from grade break to crown (v/hz) = 0.020
Street flow is on [2] side(s) of the street
Distance from curb to property line = 10.000(Ft.)
Slope from curb to property line (v/hz) = 0.020
Gutter width = 1.500(Ft.)
Gutter hike from flowline = 1.500(In.)
Manning's N in gutter = 0.0150

```

Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 15.458 (CFS)  
 Depth of flow = 0.404 (Ft.), Average velocity = 3.146 (Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 15.445 (Ft.)  
 Flow velocity = 3.15 (Ft/s)  
 Travel time = 1.75 min. TC = 19.54 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367 (In/Hr)  
 Rainfall intensity = 2.151 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rationally method) (Q=KCIA) is C = 0.746  
 Subarea runoff = 8.962 (CFS) for 6.000 (Ac.)  
 Total runoff = 19.267 (CFS)  
 Effective area this stream = 12.00 (Ac.)  
 Total Study Area (Main Stream No. 1) = 72.00 (Ac.)  
 Area averaged Fm value = 0.367 (In/Hr)  
 Street flow at end of street = 19.267 (CFS)  
 Half street flow at end of street = 9.634 (CFS)  
 Depth of flow = 0.431 (Ft.), Average velocity = 3.321 (Ft/s)  
 Flow width (from curb towards crown) = 16.820 (Ft.)

++++++  
 Process from Point/Station 636.000 to Point/Station 637.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1037.800 (Ft.)  
 End of street segment elevation = 1031.000 (Ft.)  
 Length of street segment = 660.000 (Ft.)  
 Height of curb above gutter flowline = 8.0 (In.)  
 Width of half street (curb to crown) = 20.000 (Ft.)  
 Distance from crown to crossfall grade break = 18.500 (Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000 (Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500 (Ft.)  
 Gutter hike from flowline = 1.500 (In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 28.098 (CFS)  
 Depth of flow = 0.496 (Ft.), Average velocity = 3.434 (Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000 (Ft.)  
 Flow velocity = 3.43 (Ft/s)  
 Travel time = 3.20 min. TC = 22.74 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000

Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.489(In/Hr)  
 Rainfall intensity =      1.964(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.705  
 Subarea runoff =      12.577(CFS) for      11.000(Ac.)  
 Total runoff =      31.844(CFS)  
 Effective area this stream =      23.00(Ac.)  
 Total Study Area (Main Stream No. 1) =      83.00(Ac.)  
 Area averaged Fm value =      0.425(In/Hr)  
 Street flow at end of street =      31.844(CFS)  
 Half street flow at end of street =      15.922(CFS)  
 Depth of flow =      0.512(Ft.), Average velocity =      3.609(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)=      20.000(Ft.)

++++++  
 Process from Point/Station      637.000 to Point/Station      637.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2

Stream flow area =      23.000(Ac.)  
 Runoff from this stream =      31.844(CFS)  
 Time of concentration =      22.74 min.  
 Rainfall intensity =      1.964(In/Hr)  
 Area averaged loss rate (Fm) =      0.4253(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000

Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	79.019	22.70	1.966
2	31.844	22.74	1.964
Qmax(1) =			
	1.000 *	1.000 *	79.019) +
	1.002 *	0.998 *	31.844) + =      110.848
Qmax(2) =			
	0.999 *	1.000 *	79.019) +
	1.000 *	1.000 *	31.844) + =      110.747

Total of 2 streams to confluence:

Flow rates before confluence point:

79.019      31.844

Maximum flow rates at confluence using above data:

110.848      110.747

Area of streams before confluence:

52.313      23.000

Effective area values after confluence:

75.267      75.313

Results of confluence:

Total flow rate =      110.848(CFS)

Time of concentration =      22.696 min.

Effective stream area after confluence =      75.267(Ac.)

Stream Area average Pervious fraction(Ap) =      0.500

Stream Area average soil loss rate(Fm) = 0.385(In/Hr)  
Study area (this main stream) = 75.31(Ac.)  
End of computations, Total Study Area = 83.00 (Ac.)

The following figures may  
be used for a unit hydrograph study of the same area.  
Note: These figures do not consider reduced effective area  
effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.500  
Area averaged SCS curve number = 52.8

LINE "14' x 9' RCB"

## San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
 Rational Hydrology Study Date: 01/13/05

-----  
 FONTANA / LINE JURUPA AVE. 14'X 9' RCB HYDROLOGY  
 25 YEAR STORM  
 JN 04339  
 -----

Hall & Forman, Inc. - S/N 950  
 -----

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*  
 -----

Rational hydrology study storm event year is 25.0  
 10 Year storm 1 hour rainfall = 0.930(In.)  
 100 Year storm 1 hour rainfall = 1.350(In.)  
 Computed rainfall intensity:  
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
 Slope used for rainfall intensity curve b = 0.6000  
 Soil antecedent moisture condition (AMC) = 2

+++++  
 Process from Point/Station 89.000 to Point/Station 89.000  
 \*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*  
 -----

Soil classification AP and SCS values input by user  
 USER INPUT of soil data for subarea  
 SCS curve number for soil(AMC 2) = 68.38  
 Pervious ratio(Ap) = 0.4790 Max loss rate(Fm)= 0.267(In/Hr)  
 Rainfall intensity = 2.805(In/Hr) for a 25.0 year storm  
 User specified values are as follows:  
 TC = 12.55 min. Rain intensity = 2.81(In/Hr)  
 Total area this stream = 577.91(Ac.)  
 Total Study Area (Main Stream No. 1) = 577.91(Ac.)  
 Total runoff = 1522.64(CFS)

+++++  
 Process from Point/Station 89.000 to Point/Station 90.000  
 \*\*\*\* IMPROVED CHANNEL TRAVEL TIME \*\*\*\*  
 -----

Covered channel  
 Upstream point elevation = 1028.200(Ft.)  
 Downstream point elevation = 1022.300(Ft.)  
 Channel length thru subarea = 1320.000(Ft.)  
 Channel base width = 14.000(Ft.)  
 Slope or 'Z' of left channel bank = 0.000  
 Slope or 'Z' of right channel bank = 0.000  
 Manning's 'N' = 0.015  
 Maximum depth of channel = 9.000(Ft.)  
 Flow(q) thru subarea = 1522.640(CFS)  
 Depth of flow = 7.092(Ft.), Average velocity = 15.335(Ft/s)  
 Channel flow top width = 14.000(Ft.)  
 Flow Velocity = 15.33(Ft/s)  
 Travel time = 1.43 min.

Time of concentration = 13.98 min.  
 Critical depth = 7.125(Ft.)

+++++  
 Process from Point/Station 90.000 to Point/Station 90.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 577.910(Ac.)  
 Runoff from this stream = 1522.640(CFS)  
 Time of concentration = 13.98 min.  
 Rainfall intensity = 2.629(In/Hr)  
 Area averaged loss rate (Fm) = 0.2670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.4790

+++++  
 Process from Point/Station 90.000 to Point/Station 90.000  
 \*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

---

Soil classification AP and SCS values input by user  
 USER INPUT of soil data for subarea  
 SCS curve number for soil(AMC 2) = 56.05  
 Pervious ratio(Ap) = 0.1950 Max loss rate(Fm)= 0.143(In/Hr)  
 Rainfall intensity = 2.030(In/Hr) for a 25.0 year storm  
 User specified values are as follows:  
 TC = 21.51 min. Rain intensity = 2.03(In/Hr)  
 Total area this stream = 76.62(Ac.)  
 Total Study Area (Main Stream No. 1) = 654.53(Ac.)  
 Total runoff = 137.80(CFS)

+++++  
 Process from Point/Station 90.000 to Point/Station 90.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 76.620(Ac.)  
 Runoff from this stream = 137.800(CFS)  
 Time of concentration = 21.51 min.  
 Rainfall intensity = 2.030(In/Hr)  
 Area averaged loss rate (Fm) = 0.1430(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1950

+++++  
 Process from Point/Station 616.000 to Point/Station 617.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1540.000(Ft.)  
 Bottom (of initial area) elevation = 1160.000(Ft.)

Difference in elevation = 380.000(Ft.)  
 Slope = 0.38000 s(%) = 38.00  
 $TC = k(0.525) * [(length^3) / (elevation\ change)]^{0.2}$   
 Initial area time of concentration = 10.097 min.  
 Rainfall intensity = 3.196(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.786  
 Subarea runoff = 17.594(CFS)  
 Total initial stream area = 7.000(Ac.)  
 Pervious area fraction = 1.000  
 Initial area Fm value = 0.404(In/Hr)

+++++  
 Process from Point/Station 617.000 to Point/Station 618.000  
 \*\*\*\* IRREGULAR CHANNEL FLOW TRAVEL TIME \*\*\*\*

-----  
 Estimated mean flow rate at midpoint of channel = 40.214(CFS)  
 Depth of flow = 0.512(Ft.), Average velocity = 5.105(Ft/s)  
 \*\*\*\*\* Irregular Channel Data \*\*\*\*\*

-----  
 Information entered for subchannel number 1 :  
 Point number 'X' coordinate 'Y' coordinate  
 1 0.00 5.00  
 2 150.00 0.00  
 3 300.00 5.00  
 Manning's 'N' friction factor = 0.035  
 -----

Sub-Channel flow = 40.214(CFS)  
 ' ' flow top width = 30.747(Ft.)  
 ' ' velocity = 5.105(Ft/s)  
 ' ' area = 7.878(Sq.Ft)  
 ' ' Froude number = 1.777

Upstream point elevation = 1160.000(Ft.)  
 Downstream point elevation = 1080.000(Ft.)  
 Flow length = 900.000(Ft.)  
 Travel time = 2.94 min.  
 Time of concentration = 13.04 min.  
 Depth of flow = 0.512(Ft.)  
 Average velocity = 5.105(Ft/s)  
 Total irregular channel flow = 40.214(CFS)  
 Irregular channel normal depth above invert elev. = 0.512(Ft.)  
 Average velocity of channel(s) = 5.105(Ft/s)

Sub-Channel No. 1 Critical depth = 0.645(Ft.)  
 ' ' ' Critical flow top width = 38.672(Ft.)  
 ' ' ' Critical flow velocity = 3.227(Ft/s)  
 ' ' ' Critical flow area = 12.463(Sq.Ft)

Adding area flow to channel  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404(In/Hr)  
 Rainfall intensity = 2.742(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.768  
 Subarea runoff = 35.022(CFS) for 18.000(Ac.)

Total runoff = 52.616(CFS)  
 Effective area this stream = 25.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 679.53(Ac.)  
 Area averaged Fm value = 0.404(In/Hr)

++++  
 Process from Point/Station 618.000 to Point/Station 90.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1033.000(Ft.)  
 Downstream point/station elevation = 1025.000(Ft.)  
 Pipe length = 420.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 52.616(CFS)  
 Given pipe size = 48.00(In.)  
 Calculated individual pipe flow = 52.616(CFS)  
 Normal flow depth in pipe = 16.88(In.)  
 Flow top width inside pipe = 45.84(In.)  
 Critical Depth = 26.14(In.)  
 Pipe flow velocity = 13.33(Ft/s)  
 Travel time through pipe = 0.53 min.  
 Time of concentration (TC) = 13.56 min.

++++  
 Process from Point/Station 90.000 to Point/Station 90.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 25.000(Ac.)  
 Runoff from this stream = 52.616(CFS)  
 Time of concentration = 13.56 min.  
 Rainfall intensity = 2.678(In/Hr)  
 Area averaged loss rate (Fm) = 0.4035(In/Hr)  
 Area averaged Pervious ratio (Ap) = 1.0000

++++  
 Process from Point/Station 619.000 to Point/Station 620.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1056.400(Ft.)  
 Bottom (of initial area) elevation = 1051.400(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%)= 0.50  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 17.789 min.  
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755  
 Subarea runoff = 10.306(CFS)  
 Total initial stream area = 6.000(Ac.)  
 Pervious area fraction = 0.500

Initial area Fm value = 0.367(In/Hr)

+++++  
 Process from Point/Station 620.000 to Point/Station 621.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1051.400(Ft.)  
 End of street segment elevation = 1046.000(Ft.)  
 Length of street segment = 1070.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.083  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 15.458(CFS)  
 Depth of flow = 0.461(Ft.), Average velocity = 2.261(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 18.293(Ft.)  
 Flow velocity = 2.26(Ft/s)  
 Travel time = 7.89 min. TC = 25.67 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 1.826(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.719  
 Subarea runoff = 5.450(CFS) for 6.000(Ac.)  
 Total runoff = 15.755(CFS)  
 Effective area this stream = 12.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 691.53(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 15.755(CFS)  
 Half street flow at end of street = 7.878(CFS)  
 Depth of flow = 0.464(Ft.), Average velocity = 2.272(Ft/s)  
 Flow width (from curb towards crown)= 18.428(Ft.)

+++++  
 Process from Point/Station 621.000 to Point/Station 621.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 4  
 Stream flow area = 12.000(Ac.)  
 Runoff from this stream = 15.755(CFS)  
 Time of concentration = 25.67 min.  
 Rainfall intensity = 1.826(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)

Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1522.640	13.98	2.629
2	137.800	21.51	2.030
3	52.616	13.56	2.678
4	15.755	25.67	1.826

Qmax(1) =  
 1.000 \* 1.000 \* 1522.640) +  
 1.317 \* 0.650 \* 137.800) +  
 0.978 \* 1.000 \* 52.616) +  
 1.550 \* 0.545 \* 15.755) + = 1705.428

Qmax(2) =  
 0.747 \* 1.000 \* 1522.640) +  
 1.000 \* 1.000 \* 137.800) +  
 0.715 \* 1.000 \* 52.616) +  
 1.140 \* 0.838 \* 15.755) + = 1327.290

Qmax(3) =  
 1.021 \* 0.970 \* 1522.640) +  
 1.343 \* 0.630 \* 137.800) +  
 1.000 \* 1.000 \* 52.616) +  
 1.584 \* 0.528 \* 15.755) + = 1689.602

Qmax(4) =  
 0.660 \* 1.000 \* 1522.640) +  
 0.892 \* 1.000 \* 137.800) +  
 0.625 \* 1.000 \* 52.616) +  
 1.000 \* 1.000 \* 15.755) + = 1176.449

Total of 4 streams to confluence:

Flow rates before confluence point:

1522.640      137.800      52.616      15.755

Maximum flow rates at confluence using above data:

1705.428      1327.290      1689.602      1176.449

Area of streams before confluence:

577.910      76.620      25.000      12.000

Effective area values after confluence:

659.260      689.583      640.042      691.530

Results of confluence:

Total flow rate = 1705.428(CFS)

Time of concentration = 13.985 min.

Effective stream area after confluence = 659.260(Ac.)

Stream Area average Pervious fraction(Ap) = 0.467

Stream Area average soil loss rate(Fm) = 0.260(In/Hr)

Study area (this main stream) = 691.53(Ac.)

\*\*\*\*\*  
 Process from Point/Station      90.000 to Point/Station      91.000  
 \*\*\*\* IMPROVED CHANNEL TRAVEL TIME \*\*\*\*

Covered channel

Upstream point elevation = 1022.300(Ft.)

Downstream point elevation = 1013.100(Ft.)

Channel length thru subarea = 1320.000(Ft.)

Channel base width = 14.000(Ft.)

Slope or 'Z' of left channel bank = 0.000

Slope or 'Z' of right channel bank = 0.000

Manning's 'N' = 0.015  
 Maximum depth of channel = 9.000(Ft.)  
 Flow(q) thru subarea = 1705.428(CFS)  
 Depth of flow = 6.539(Ft.), Average velocity = 18.630(Ft/s)  
 Channel flow top width = 14.000(Ft.)  
 Flow Velocity = 18.63(Ft/s)  
 Travel time = 1.18 min.  
 Time of concentration = 15.17 min.  
 Critical depth = 7.750(Ft.)

++++++  
 Process from Point/Station 91.000 to Point/Station 91.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 659.260(Ac.)  
 Runoff from this stream = 1705.428(CFS)  
 Time of concentration = 15.17 min.  
 Rainfall intensity = 2.504(In/Hr)  
 Area averaged loss rate (Fm) = 0.2599(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.4667

++++++  
 Process from Point/Station 91.000 to Point/Station 91.000  
 \*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

Soil classification AP and SCS values input by user  
 USER INPUT of soil data for subarea  
 SCS curve number for soil(AMC 2) = 53.21  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.385(In/Hr)  
 Rainfall intensity = 1.966(In/Hr) for a 25.0 year storm  
 User specified values are as follows:  
 TC = 22.70 min. Rain intensity = 1.97(In/Hr)  
 Total area this stream = 75.27(Ac.)  
 Total Study Area (Main Stream No. 1) = 766.80(Ac.)  
 Total runoff = 110.85(CFS)

++++++  
 Process from Point/Station 91.000 to Point/Station 91.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 75.270(Ac.)  
 Runoff from this stream = 110.850(CFS)  
 Time of concentration = 22.70 min.  
 Rainfall intensity = 1.966(In/Hr)  
 Area averaged loss rate (Fm) = 0.3850(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000

++++++  
 Process from Point/Station 638.000 to Point/Station 639.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000      Max loss rate(Fm)=      0.404(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1900.000(Ft.)  
 Bottom (of initial area) elevation = 1540.000(Ft.)  
 Difference in elevation = 360.000(Ft.)  
 Slope = 0.36000 s(%)= 36.00  
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 10.207 min.  
 Rainfall intensity = 3.175(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.786  
 Subarea runoff = 24.948(CFS)  
 Total initial stream area = 10.000(Ac.)  
 Pervious area fraction = 1.000  
 Initial area Fm value = 0.404(In/Hr)

++++++  
 Process from Point/Station      639.000 to Point/Station      640.000  
 \*\*\*\* IRREGULAR CHANNEL FLOW TRAVEL TIME \*\*\*\*

-----  
 Estimated mean flow rate at midpoint of channel = 49.896(CFS)  
 Depth of flow = 0.772(Ft.), Average velocity = 16.729(Ft/s)  
 \*\*\*\*\* Irregular Channel Data \*\*\*\*\*

-----  
 Information entered for subchannel number 1 :  

Point number	'X' coordinate	'Y' coordinate
1	0.00	20.00
2	100.00	0.00
3	200.00	20.00

 Manning's 'N' friction factor = 0.035  
 -----

Sub-Channel flow = 49.896(CFS)  
 ' ' flow top width = 7.724(Ft.)  
 ' ' velocity= 16.729(Ft/s)  
 ' ' area = 2.983(Sq.Ft)  
 ' ' Froude number = 4.744

Upstream point elevation = 1540.000(Ft.)  
 Downstream point elevation = 1200.000(Ft.)  
 Flow length = 600.000(Ft.)  
 Travel time = 0.60 min.  
 Time of concentration = 10.80 min.  
 Depth of flow = 0.772(Ft.)  
 Average velocity = 16.729(Ft/s)  
 Total irregular channel flow = 49.896(CFS)  
 Irregular channel normal depth above invert elev. = 0.772(Ft.)  
 Average velocity of channel(s) = 16.729(Ft/s)

Sub-Channel No. 1 Critical depth = 1.438(Ft.)  
 ' ' ' Critical flow top width = 14.375(Ft.)  
 ' ' ' Critical flow velocity= 4.829(Ft/s)  
 ' ' ' Critical flow area = 10.332(Sq.Ft)

Adding area flow to channel  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)  
 Rainfall intensity = 3.069(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.782  
 Subarea runoff = 47.017(CFS) for 20.000(Ac.)  
 Total runoff = 71.965(CFS)  
 Effective area this stream = 30.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 796.80(Ac.)  
 Area averaged Fm value = 0.404(In/Hr)

++++++  
 Process from Point/Station 640.000 to Point/Station 641.000  
 \*\*\*\* IRREGULAR CHANNEL FLOW TRAVEL TIME \*\*\*\*

-----  
 Estimated mean flow rate at midpoint of channel = 122.341(CFS)  
 Depth of flow = 0.624(Ft.), Average velocity = 6.279(Ft/s)  
 \*\*\*\*\* Irregular Channel Data \*\*\*\*\*

-----  
 Information entered for subchannel number 1 :  

Point number	'X' coordinate	'Y' coordinate
1	0.00	4.00
2	200.00	0.00
3	400.00	4.00

 Manning's 'N' friction factor = 0.035  
 -----

Sub-Channel flow = 122.341(CFS)  
 ' ' flow top width = 62.424(Ft.)  
 ' ' velocity= 6.279(Ft/s)  
 ' ' area = 19.484(Sq.Ft)  
 ' ' Froude number = 1.981

Upstream point elevation = 1200.000(Ft.)  
 Downstream point elevation = 1045.000(Ft.)  
 Flow length = 1500.000(Ft.)  
 Travel time = 3.98 min.  
 Time of concentration = 14.79 min.  
 Depth of flow = 0.624(Ft.)  
 Average velocity = 6.279(Ft/s)  
 Total irregular channel flow = 122.341(CFS)  
 Irregular channel normal depth above invert elev. = 0.624(Ft.)  
 Average velocity of channel(s) = 6.279(Ft/s)

Sub-Channel No. 1 Critical depth = 0.820(Ft.)  
 ' ' ' Critical flow top width = 82.031(Ft.)  
 ' ' ' Critical flow velocity= 3.636(Ft/s)  
 ' ' ' Critical flow area = 33.646(Sq.Ft)

Adding area flow to channel  
 UNDEVELOPED (poor cover) subarea  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 78.00  
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)  
 Rainfall intensity = 2.542(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.757

Subarea runoff = 66.631(CFS) for 42.000(Ac.)  
 Total runoff = 138.596(CFS)  
 Effective area this stream = 72.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 838.80(Ac.)  
 Area averaged Fm value = 0.404(In/Hr)

++++  
 Process from Point/Station 641.000 to Point/Station 91.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1035.000(Ft.)  
 Downstream point/station elevation = 1015.400(Ft.)  
 Pipe length = 450.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 138.596(CFS)  
 Given pipe size = 42.00(In.)  
 Calculated individual pipe flow = 138.596(CFS)  
 Normal flow depth in pipe = 24.91(In.)  
 Flow top width inside pipe = 41.26(In.)  
 Critical depth could not be calculated.  
 Pipe flow velocity = 23.31(Ft/s)  
 Travel time through pipe = 0.32 min.  
 Time of concentration (TC) = 15.11 min.

++++  
 Process from Point/Station 91.000 to Point/Station 91.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 72.000(Ac.)  
 Runoff from this stream = 138.596(CFS)  
 Time of concentration = 15.11 min.  
 Rainfall intensity = 2.510(In/Hr)  
 Area averaged loss rate (Fm) = 0.4035(In/Hr)  
 Area averaged Pervious ratio (Ap) = 1.0000

++++  
 Process from Point/Station 642.000 to Point/Station 643.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1042.000(Ft.)  
 Bottom (of initial area) elevation = 1037.000(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%) = 0.50  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 17.789 min.  
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755  
 Subarea runoff = 10.306(CFS)  
 Total initial stream area = 6.000(Ac.)

Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

+++++  
 Process from Point/Station 643.000 to Point/Station 644.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1037.000(Ft.)  
 End of street segment elevation = 1031.000(Ft.)  
 Length of street segment = 1200.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.083  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 17.176(CFS)  
 Depth of flow = 0.477(Ft.), Average velocity = 2.313(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 19.083(Ft.)  
 Flow velocity = 2.31(Ft/s)  
 Travel time = 8.65 min. TC = 26.44 min.

Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)  
 Rainfall intensity = 1.794(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.681  
 Subarea runoff = 6.798(CFS) for 8.000(Ac.)  
 Total runoff = 17.103(CFS)  
 Effective area this stream = 14.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 852.80(Ac.)  
 Area averaged Fm value = 0.437(In/Hr)  
 Street flow at end of street = 17.103(CFS)  
 Half street flow at end of street = 8.552(CFS)  
 Depth of flow = 0.476(Ft.), Average velocity = 2.311(Ft/s)  
 Flow width (from curb towards crown)= 19.052(Ft.)

+++++  
 Process from Point/Station 644.000 to Point/Station 644.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 4  
 Stream flow area = 14.000(Ac.)  
 Runoff from this stream = 17.103(CFS)  
 Time of concentration = 26.44 min.  
 Rainfall intensity = 1.794(In/Hr)

Area averaged loss rate (Fm) = 0.4366(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000

+++++  
 Process from Point/Station 645.000 to Point/Station 646.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1042.000(Ft.)  
 Bottom (of initial area) elevation = 1037.000(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%)= 0.50  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 17.789 min.  
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.707  
 Subarea runoff = 9.647(CFS)  
 Total initial stream area = 6.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.489(In/Hr)

+++++  
 Process from Point/Station 646.000 to Point/Station 647.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1037.000(Ft.)  
 End of street segment elevation = 1031.000(Ft.)  
 Length of street segment = 1200.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.083  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 15.275(CFS)  
 Depth of flow = 0.460(Ft.), Average velocity = 2.247(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 18.242(Ft.)  
 Flow velocity = 2.25(Ft/s)  
 Travel time = 8.90 min. TC = 26.69 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000

Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)  
 Rainfall intensity = 1.784(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.653  
 Subarea runoff = 5.503(CFS) for 7.000(Ac.)  
 Total runoff = 15.150(CFS)  
 Effective area this stream = 13.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 865.80(Ac.)  
 Area averaged Fm value = 0.489(In/Hr)  
 Street flow at end of street = 15.150(CFS)  
 Half street flow at end of street = 7.575(CFS)  
 Depth of flow = 0.459(Ft.), Average velocity = 2.242(Ft/s)  
 Flow width (from curb towards crown)= 18.185(Ft.)

+++++  
 Process from Point/Station 647.000 to Point/Station 647.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
 Along Main Stream number: 1 in normal stream number 5  
 Stream flow area = 13.000(Ac.)  
 Runoff from this stream = 15.150(CFS)  
 Time of concentration = 26.69 min.  
 Rainfall intensity = 1.784(In/Hr)  
 Area averaged loss rate (Fm) = 0.4889(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1705.428	15.17	2.504
2	110.850	22.70	1.966
3	138.596	15.11	2.510
4	17.103	26.44	1.794
5	15.150	26.69	1.784
Qmax(1) =			
	1.000 *	1.000 *	1705.428) +
	1.340 *	0.668 *	110.850) +
	0.997 *	1.000 *	138.596) +
	1.523 *	0.574 *	17.103) +
	1.556 *	0.568 *	15.150) + = 1971.261
Qmax(2) =			
	0.760 *	1.000 *	1705.428) +
	1.000 *	1.000 *	110.850) +
	0.742 *	1.000 *	138.596) +
	1.127 *	0.859 *	17.103) +
	1.141 *	0.850 *	15.150) + = 1541.286
Qmax(3) =			
	1.003 *	0.996 *	1705.428) +
	1.344 *	0.666 *	110.850) +
	1.000 *	1.000 *	138.596) +
	1.527 *	0.571 *	17.103) +
	1.561 *	0.566 *	15.150) + = 1969.356
Qmax(4) =			
	0.684 *	1.000 *	1705.428) +
	0.891 *	1.000 *	110.850) +

	0.660 *	1.000 *	138.596)	+	
	1.000 *	1.000 *	17.103)	+	
	1.008 *	0.990 *	15.150)	+	1388.419
Qmax(5) =					
	0.679 *	1.000 *	1705.428)	+	
	0.885 *	1.000 *	110.850)	+	
	0.655 *	1.000 *	138.596)	+	
	0.992 *	1.000 *	17.103)	+	
	1.000 *	1.000 *	15.150)	+	1379.108

Total of 5 streams to confluence:

Flow rates before confluence point:

1705.428	110.850	138.596	17.103	15.150
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Maximum flow rates at confluence using above data:

1971.261	1541.286	1969.356	1388.419	1379.108
----------	----------	----------	----------	----------

Area of streams before confluence:

659.260	75.270	72.000	14.000	13.000
---------	--------	--------	--------	--------

Effective area values after confluence:

796.965	829.608	794.213	833.407	833.530
---------	---------	---------	---------	---------

Results of confluence:

Total flow rate = 1971.261(CFS)

Time of concentration = 15.166 min.

Effective stream area after confluence = 796.965(Ac.)

Stream Area average Pervious fraction(Ap) = 0.517

Stream Area average soil loss rate(Fm) = 0.290(In/Hr)

Study area (this main stream) = 833.53(Ac.)

\*\*\*\*\*  
 Process from Point/Station 91.000 to Point/Station 92.000  
 \*\*\*\* IMPROVED CHANNEL TRAVEL TIME \*\*\*\*

Covered channel

Upstream point elevation = 1013.100(Ft.)

Downstream point elevation = 1006.400(Ft.)

Channel length thru subarea = 1340.000(Ft.)

Channel base width = 14.000(Ft.)

Slope or 'Z' of left channel bank = 0.000

Slope or 'Z' of right channel bank = 0.000

Manning's 'N' = 0.013

Maximum depth of channel = 9.000(Ft.)

Flow(q) thru subarea = 1971.261(CFS)

Depth of flow = 7.415(Ft.), Average velocity = 18.989(Ft/s)

Channel flow top width = 14.000(Ft.)

Flow Velocity = 18.99(Ft/s)

Travel time = 1.18 min.

Time of concentration = 16.34 min.

Critical depth = 8.500(Ft.)

\*\*\*\*\*  
 Process from Point/Station 92.000 to Point/Station 92.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 796.965(Ac.)

Runoff from this stream = 1971.261(CFS)

Time of concentration = 16.34 min.

Rainfall intensity = 2.394(In/Hr)

Area averaged loss rate (Fm) = 0.2902(In/Hr)

Area averaged Pervious ratio (Ap) = 0.5169

\*\*\*\*\*  
 Process from Point/Station 650.000 to Point/Station 651.000  
 \*\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*\*

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.489(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1040.300(Ft.)  
 Bottom (of initial area) elevation = 1033.600(Ft.)  
 Difference in elevation = 6.700(Ft.)  
 Slope = 0.00670 s(%) = 0.67  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 16.778 min.  
 Rainfall intensity = 2.357(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.713  
 Subarea runoff = 8.405(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.489(In/Hr)

\*\*\*\*\*  
 Process from Point/Station 651.000 to Point/Station 652.000  
 \*\*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*\*

Top of street segment elevation = 1033.600(Ft.)  
 End of street segment elevation = 1031.400(Ft.)  
 Length of street segment = 330.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.083  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 12.608(CFS)  
 Depth of flow = 0.416(Ft.), Average velocity = 2.388(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 16.025(Ft.)  
 Flow velocity = 2.39(Ft/s)  
 Travel time = 2.30 min. TC = 19.08 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)  
 Rainfall intensity = 2.182(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.698  
 Subarea runoff = 6.830(CFS) for 5.000(Ac.)  
 Total runoff = 15.235(CFS)  
 Effective area this stream = 10.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 875.80(Ac.)  
 Area averaged Fm value = 0.489(In/Hr)  
 Street flow at end of street = 15.235(CFS)  
 Half street flow at end of street = 7.618(CFS)  
 Depth of flow = 0.440(Ft.), Average velocity = 2.502(Ft/s)  
 Flow width (from curb towards crown)= 17.242(Ft.)

+++++  
 Process from Point/Station 652.000 to Point/Station 653.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

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Top of street segment elevation = 1031.400(Ft.)  
 End of street segment elevation = 1026.000(Ft.)  
 Length of street segment = 750.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.083  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 23.615(CFS)  
 Depth of flow = 0.497(Ft.), Average velocity = 2.877(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 2.88(Ft/s)  
 Travel time = 4.35 min. TC = 23.43 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)  
 Rainfall intensity = 1.929(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.672  
 Subarea runoff = 11.982(CFS) for 11.000(Ac.)  
 Total runoff = 27.218(CFS)  
 Effective area this stream = 21.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 886.80(Ac.)  
 Area averaged Fm value = 0.489(In/Hr)  
 Street flow at end of street = 27.218(CFS)  
 Half street flow at end of street = 13.609(CFS)

Warning: depth of flow exceeds top of curb  
 Note: depth of flow exceeds top of street crown.  
 Distance that curb overflow reaches into property = 10.00(Ft.)  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++  
 Process from Point/Station 653.000 to Point/Station 654.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1026.000(Ft.)  
 End of street segment elevation = 1023.000(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.083  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 34.346(CFS)  
 Depth of flow = 0.767(Ft.), Average velocity = 2.963(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 4.99(Ft.)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 33.576(Ft.)  
 Flow velocity = 2.96(Ft/s)  
 Travel time = 3.71 min. TC = 27.14 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)  
 Rainfall intensity = 1.766(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.651  
 Subarea runoff = 9.563(CFS) for 11.000(Ac.)  
 Total runoff = 36.781(CFS)  
 Effective area this stream = 32.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 897.80(Ac.)  
 Area averaged Fm value = 0.489(In/Hr)  
 Street flow at end of street = 36.781(CFS)  
 Half street flow at end of street = 36.781(CFS)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 13.42(Ft.)  
 Flow width (from curb towards crown)= 42.000(Ft.)

++++  
 Process from Point/Station 654.000 to Point/Station 654.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 32.000(Ac.)  
 Runoff from this stream = 36.781(CFS)  
 Time of concentration = 27.14 min.  
 Rainfall intensity = 1.766(In/Hr)  
 Area averaged loss rate (Fm) = 0.4889(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	1971.261	16.34	2.394
2	36.781	27.14	1.766
Qmax(1) =			
	1.000 *	1.000 *	1971.261) +
	1.492 *	0.602 *	36.781) + = 2004.303
Qmax(2) =			
	0.701 *	1.000 *	1971.261) +
	1.000 *	1.000 *	36.781) + = 1419.449

Total of 2 streams to confluence:

Flow rates before confluence point:

1971.261      36.781

Maximum flow rates at confluence using above data:

2004.303      1419.449

Area of streams before confluence:

796.965      32.000

Effective area values after confluence:

816.234      828.965

Results of confluence:

Total flow rate = 2004.303(CFS)

Time of concentration = 16.342 min.

Effective stream area after confluence = 816.234(Ac.)

Stream Area average Pervious fraction(Ap) = 0.516

Stream Area average soil loss rate(Fm) = 0.298(In/Hr)

Study area (this main stream) = 828.97(Ac.)

\*\*\*\*\*  
 Process from Point/Station      92.000 to Point/Station      93.000  
 \*\*\*\* IMPROVED CHANNEL TRAVEL TIME \*\*\*\*

Covered channel

Upstream point elevation = 1006.400(Ft.)

Downstream point elevation = 1005.500(Ft.)

Channel length thru subarea = 450.000(Ft.)

Channel base width = 14.000(Ft.)

Slope or 'Z' of left channel bank = 0.000

Slope or 'Z' of right channel bank = 0.000

Manning's 'N' = 0.015

Maximum depth of channel = 9.000(Ft.)

Flow(q) thru subarea = 2004.303(CFS)

Pressure flow condition in covered channel:

Wetted perimeter = 46.00(Ft.)      Flow area = 126.00(Sq.Ft)

Hydraulic grade line required at box inlet = 4.505(Ft.)

Friction loss = 5.405(Ft.)

Minor Friction loss = 0.000(Ft.)      K-Factor = 0.000

Flow Velocity = 15.91(Ft/s)

Travel time = 0.47 min.

Time of concentration = 23.17 min.  
End of computations, Total Study Area = 897.80 (Ac.)  
The following figures may  
be used for a unit hydrograph study of the same area.  
Note: These figures do not consider reduced effective area  
effects caused by confluences in the rational equation.

Area averaged pervious area fraction( $A_p$ ) = 0.514  
Area averaged SCS curve number = 64.7

LINE "DZ-6"

## San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
 Rational Hydrology Study Date: 01/13/05

-----  
 FONTANA / LINE DZ-6 HYDROLOGY  
 25 YEAR STORM  
 JN 04339  
 -----

-----  
 Hall & Forman, Inc. - S/N 950  
 -----

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

-----  
 Rational hydrology study storm event year is 25.0  
 10 Year storm 1 hour rainfall = 0.930(In.)  
 100 Year storm 1 hour rainfall = 1.350(In.)  
 Computed rainfall intensity:  
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
 Slope used for rainfall intensity curve b = 0.6000  
 Soil antecedent moisture condition (AMC) = 2

+++++  
 Process from Point/Station 714.000 to Point/Station 715.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

-----  
 COMMERCIAL subarea type

Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1104.000(Ft.)  
 Bottom (of initial area) elevation = 1092.000(Ft.)  
 Difference in elevation = 12.000(Ft.)  
 Slope = 0.01200 s(%)= 1.20  
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 11.669 min.  
 Rainfall intensity = 2.930(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.870  
 Subarea runoff = 17.846(CFS)  
 Total initial stream area = 7.000(Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.098(In/Hr)

+++++  
 Process from Point/Station 715.000 to Point/Station 716.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

-----  
 Top of street segment elevation = 1092.000(Ft.)  
 End of street segment elevation = 1089.000(Ft.)  
 Length of street segment = 800.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 31.867(CFS)  
 Depth of flow = 0.591(Ft.), Average velocity = 2.662(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 2.66(Ft/s)  
 Travel time = 5.01 min. TC = 16.68 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)  
 Rainfall intensity = 2.365(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.863  
 Subarea runoff = 18.885(CFS) for 11.000(Ac.)  
 Total runoff = 36.731(CFS)  
 Effective area this stream = 18.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 18.00(Ac.)  
 Area averaged Fm value = 0.098(In/Hr)  
 Street flow at end of street = 36.731(CFS)  
 Half street flow at end of street = 18.366(CFS)  
 Depth of flow = 0.618(Ft.), Average velocity = 2.816(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 716.000 to Point/Station 717.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1089.000(Ft.)  
 End of street segment elevation = 1081.500(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150

Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 57.137(CFS)  
 Depth of flow = 0.780(Ft.), Average velocity = 4.717(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 5.65(Ft.)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 34.236(Ft.)  
 Flow velocity = 4.72(Ft/s)  
 Travel time = 2.33 min. TC = 19.01 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)  
 Rainfall intensity = 2.187(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.860  
 Subarea runoff = 34.704(CFS) for 20.000(Ac.)  
 Total runoff = 71.435(CFS)  
 Effective area this stream = 38.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 38.00(Ac.)  
 Area averaged Fm value = 0.098(In/Hr)  
 Street flow at end of street = 71.435(CFS)  
 Half street flow at end of street = 71.435(CFS)  
 Depth of flow = 0.838(Ft.), Average velocity = 4.888(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 8.58(Ft.)  
 Flow width (from curb towards crown)= 37.160(Ft.)

++++++  
 Process from Point/Station 717.000 to Point/Station 33.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1075.000(Ft.)  
 Downstream point/station elevation = 1061.000(Ft.)  
 Pipe length = 990.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 71.435(CFS)  
 Given pipe size = 36.00(In.)  
 Calculated individual pipe flow = 71.435(CFS)  
 Normal flow depth in pipe = 26.72(In.)  
 Flow top width inside pipe = 31.49(In.)  
 Critical Depth = 32.12(In.)  
 Pipe flow velocity = 12.70(Ft/s)  
 Travel time through pipe = 1.30 min.  
 Time of concentration (TC) = 20.31 min.

++++++  
 Process from Point/Station 33.000 to Point/Station 33.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 38.000(Ac.)  
 Runoff from this stream = 71.435(CFS)  
 Time of concentration = 20.31 min.  
 Rainfall intensity = 2.102(In/Hr)

Area averaged loss rate (Fm) = 0.0978 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1000

++++  
 Process from Point/Station 718.000 to Point/Station 719.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

COMMERCIAL subarea type

Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 32.00  
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.098 (In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000 (Ft.)  
 Top (of initial area) elevation = 1082.000 (Ft.)  
 Bottom (of initial area) elevation = 1075.000 (Ft.)  
 Difference in elevation = 7.000 (Ft.)  
 Slope = 0.00700 s(%) = 0.70  
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$   
 Initial area time of concentration = 12.997 min.  
 Rainfall intensity = 2.747 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.868  
 Subarea runoff = 11.921 (CFS)  
 Total initial stream area = 5.000 (Ac.)  
 Pervious area fraction = 0.100  
 Initial area Fm value = 0.098 (In/Hr)

++++  
 Process from Point/Station 719.000 to Point/Station 720.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1075.000 (Ft.)  
 End of street segment elevation = 1073.300 (Ft.)  
 Length of street segment = 330.000 (Ft.)  
 Height of curb above gutter flowline = 8.0 (In.)  
 Width of half street (curb to crown) = 20.000 (Ft.)  
 Distance from crown to crossfall grade break = 18.500 (Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000 (Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500 (Ft.)  
 Gutter hike from flowline = 1.500 (In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 17.881 (CFS)  
 Depth of flow = 0.480 (Ft.), Average velocity = 2.363 (Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 19.269 (Ft.)  
 Flow velocity = 2.36 (Ft/s)  
 Travel time = 2.33 min. TC = 15.33 min.  
 Adding area flow to street

COMMERCIAL subarea type

Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000

Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000      Max loss rate(Fm)= 0.098(In/Hr)  
 Rainfall intensity = 2.488(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.865  
 Subarea runoff = 9.594(CFS) for 5.000(Ac.)  
 Total runoff = 21.515(CFS)  
 Effective area this stream = 10.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 48.00(Ac.)  
 Area averaged Fm value = 0.098(In/Hr)  
 Street flow at end of street = 21.515(CFS)  
 Half street flow at end of street = 10.757(CFS)  
 Depth of flow = 0.506(Ft.), Average velocity = 2.506(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 720.000 to Point/Station 721.000  
 \*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*

Top of street segment elevation = 1073.300(Ft.)  
 End of street segment elevation = 1070.000(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 32.272(CFS)  
 Depth of flow = 0.568(Ft.), Average velocity = 2.918(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 2.92(Ft/s)  
 Travel time = 3.77 min.      TC = 19.10 min.

Adding area flow to street  
 COMMERCIAL subarea type

Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000      Max loss rate(Fm)= 0.098(In/Hr)  
 Rainfall intensity = 2.181(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.860  
 Subarea runoff = 15.977(CFS) for 10.000(Ac.)  
 Total runoff = 37.492(CFS)  
 Effective area this stream = 20.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 58.00(Ac.)

Area averaged Fm value = 0.098(In/Hr)  
 Street flow at end of street = 37.492(CFS)  
 Half street flow at end of street = 18.746(CFS)  
 Depth of flow = 0.594(Ft.), Average velocity = 3.096(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++  
 Process from Point/Station 721.000 to Point/Station 722.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1070.000(Ft.)  
 End of street segment elevation = 1068.000(Ft.)  
 Length of street segment = 330.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 46.865(CFS)  
 Depth of flow = 0.810(Ft.), Average velocity = 3.506(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 7.17(Ft.)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 35.750(Ft.)  
 Flow velocity = 3.51(Ft/s)  
 Travel time = 1.57 min. TC = 20.66 min.  
 Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)  
 Rainfall intensity = 2.080(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.822  
 Subarea runoff = 13.822(CFS) for 10.000(Ac.)  
 Total runoff = 51.314(CFS)  
 Effective area this stream = 30.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 68.00(Ac.)  
 Area averaged Fm value = 0.179(In/Hr)  
 Street flow at end of street = 51.314(CFS)  
 Half street flow at end of street = 51.314(CFS)  
 Depth of flow = 0.834(Ft.), Average velocity = 3.559(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 8.36(Ft.)  
 Flow width (from curb towards crown)= 36.941(Ft.)

++++

Process from Point/Station 722.000 to Point/Station 722.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 30.000(Ac.)  
 Runoff from this stream = 51.314(CFS)  
 Time of concentration = 20.66 min.  
 Rainfall intensity = 2.080(In/Hr)  
 Area averaged loss rate (Fm) = 0.1793(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1833  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	71.435	20.31	2.102
2	51.314	20.66	2.080
Qmax(1) =			
	1.000 *	1.000 *	71.435) +
	1.011 *	0.983 *	51.314) + = 122.445
Qmax(2) =			
	0.989 *	1.000 *	71.435) +
	1.000 *	1.000 *	51.314) + = 121.976

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
     71.435      51.314  
 Maximum flow rates at confluence using above data:  
     122.445      121.976  
 Area of streams before confluence:  
     38.000      30.000  
 Effective area values after confluence:  
     67.485      68.000  
 Results of confluence:  
 Total flow rate = 122.445(CFS)  
 Time of concentration = 20.310 min.  
 Effective stream area after confluence = 67.485(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.137  
 Stream Area average soil loss rate(Fm) = 0.134(In/Hr)  
 Study area (this main stream) = 68.00(Ac.)

+++++  
 Process from Point/Station 33.000 to Point/Station 34.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1061.000(Ft.)  
 Downstream point/station elevation = 1048.200(Ft.)  
 Pipe length = 990.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 122.445(CFS)  
 Given pipe size = 39.00(In.)  
 NOTE: Normal flow is pressure flow in user selected pipe size.  
 The approximate hydraulic grade line above the pipe invert is  
     14.039(Ft.) at the headworks or inlet of the pipe(s)  
 Pipe friction loss = 21.764(Ft.)  
 Minor friction loss = 5.074(Ft.) K-factor = 1.50  
 Pipe flow velocity = 14.76(Ft/s)  
 Travel time through pipe = 1.12 min.  
 Time of concentration (TC) = 21.43 min.

+++++  
 Process from Point/Station 34.000 to Point/Station 34.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 67.485(Ac.)  
 Runoff from this stream = 122.445(CFS)  
 Time of concentration = 21.43 min.  
 Rainfall intensity = 2.035(In/Hr)  
 Area averaged loss rate (Fm) = 0.1337(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.1368

+++++  
 Process from Point/Station 723.000 to Point/Station 724.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1072.000(Ft.)  
 Bottom (of initial area) elevation = 1066.600(Ft.)  
 Difference in elevation = 5.400(Ft.)  
 Slope = 0.00540 s(%)= 0.54  
 $TC = k(0.360)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 16.212 min.  
 Rainfall intensity = 2.406(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.772  
 Subarea runoff = 9.286(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.350  
 Initial area Fm value = 0.342(In/Hr)

+++++  
 Process from Point/Station 724.000 to Point/Station 725.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1066.600(Ft.)  
 End of street segment elevation = 1063.000(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150

Estimated mean flow rate at midpoint of street = 13.929(CFS)  
 Depth of flow = 0.441(Ft.), Average velocity = 2.270(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 17.313(Ft.)  
 Flow velocity = 2.27(Ft/s)  
 Travel time = 4.85 min. TC = 21.06 min.  
 Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)  
 Rainfall intensity = 2.056(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.750  
 Subarea runoff = 6.141(CFS) for 5.000(Ac.)  
 Total runoff = 15.427(CFS)  
 Effective area this stream = 10.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 78.00(Ac.)  
 Area averaged Fm value = 0.342(In/Hr)  
 Street flow at end of street = 15.427(CFS)  
 Half street flow at end of street = 7.713(CFS)  
 Depth of flow = 0.455(Ft.), Average velocity = 2.327(Ft/s)  
 Flow width (from curb towards crown)= 18.008(Ft.)

++++++  
 Process from Point/Station 725.000 to Point/Station 729.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1063.000(Ft.)  
 End of street segment elevation = 1056.600(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 15.427(CFS)  
 Depth of flow = 0.516(Ft.), Average velocity = 3.431(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 21.037(Ft.)  
 Flow velocity = 3.43(Ft/s)  
 Travel time = 3.21 min. TC = 24.26 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00

Pervious ratio(Ap) = 0.1000      Max loss rate(Fm)=      0.098 (In/Hr)  
 Rainfall intensity =      1.889(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.737  
 Subarea runoff =      0.000 (CFS) for      0.000 (Ac.)  
 Total runoff =      15.427 (CFS)  
 Effective area this stream =      10.00 (Ac.)  
 Total Study Area (Main Stream No. 1) =      78.00 (Ac.)  
 Area averaged Fm value =      0.342 (In/Hr)  
 Street flow at end of street =      15.427 (CFS)  
 Half street flow at end of street =      15.427 (CFS)  
 Depth of flow =      0.516 (Ft.), Average velocity =      3.431 (Ft/s)  
 Flow width (from curb towards crown)=      21.037 (Ft.)

++++++  
 Process from Point/Station      729.000 to Point/Station      729.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

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Along Main Stream number: 1 in normal stream number 2  
 Stream flow area =      10.000 (Ac.)  
 Runoff from this stream =      15.427 (CFS)  
 Time of concentration =      24.26 min.  
 Rainfall intensity =      1.889 (In/Hr)  
 Area averaged loss rate (Fm) =      0.3422 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.3500

++++++  
 Process from Point/Station      726.000 to Point/Station      727.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

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CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500      Max loss rate(Fm)=      0.342 (In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000 (Ft.)  
 Top (of initial area) elevation = 1069.200 (Ft.)  
 Bottom (of initial area) elevation = 1062.000 (Ft.)  
 Difference in elevation =      7.200 (Ft.)  
 Slope =      0.00720      s(%)=      0.72  
 TC = k(0.360)\*[(length^3)/(elevation change)]^0.2  
 Initial area time of concentration = 15.305 min.  
 Rainfall intensity =      2.490 (In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.776  
 Subarea runoff =      9.666 (CFS)  
 Total initial stream area =      5.000 (Ac.)  
 Pervious area fraction = 0.350  
 Initial area Fm value =      0.342 (In/Hr)

++++++  
 Process from Point/Station      727.000 to Point/Station      728.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1062.000 (Ft.)  
 End of street segment elevation = 1060.000 (Ft.)

Length of street segment = 330.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 14.499(CFS)  
 Depth of flow = 0.440(Ft.), Average velocity = 2.385(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 17.230(Ft.)  
 Flow velocity = 2.38(Ft/s)  
 Travel time = 2.31 min. TC = 17.61 min.  
 Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)  
 Rainfall intensity = 2.289(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.765  
 Subarea runoff = 7.856(CFS) for 5.000(Ac.)  
 Total runoff = 17.522(CFS)  
 Effective area this stream = 10.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 88.00(Ac.)  
 Area averaged Fm value = 0.342(In/Hr)  
 Street flow at end of street = 17.522(CFS)  
 Half street flow at end of street = 8.761(CFS)  
 Depth of flow = 0.466(Ft.), Average velocity = 2.499(Ft/s)  
 Flow width (from curb towards crown)= 18.533(Ft.)

++++++  
 Process from Point/Station 728.000 to Point/Station 729.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1060.000(Ft.)  
 End of street segment elevation = 1056.600(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150

Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 26.284 (CFS)  
 Depth of flow = 0.534 (Ft.), Average velocity = 2.714 (Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000 (Ft.)  
 Flow velocity = 2.71 (Ft/s)  
 Travel time = 4.05 min. TC = 21.67 min.  
 Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 32.00  
 Pervious ratio (Ap) = 0.3500 Max loss rate (Fm) = 0.342 (In/Hr)  
 Rainfall intensity = 2.022 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.748  
 Subarea runoff = 12.706 (CFS) for 10.000 (Ac.)  
 Total runoff = 30.229 (CFS)  
 Effective area this stream = 20.00 (Ac.)  
 Total Study Area (Main Stream No. 1) = 98.00 (Ac.)  
 Area averaged Fm value = 0.342 (In/Hr)  
 Street flow at end of street = 30.229 (CFS)  
 Half street flow at end of street = 15.114 (CFS)  
 Depth of flow = 0.555 (Ft.), Average velocity = 2.868 (Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown) = 20.000 (Ft.)

+++++  
 Process from Point/Station 729.000 to Point/Station 729.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 3  
 Stream flow area = 20.000 (Ac.)  
 Runoff from this stream = 30.229 (CFS)  
 Time of concentration = 21.67 min.  
 Rainfall intensity = 2.022 (In/Hr)  
 Area averaged loss rate (Fm) = 0.3422 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.3500  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	122.445	21.43	2.035
2	15.427	24.26	1.889
3	30.229	21.67	2.022
Qmax (1) =			
	1.000 *	1.000 *	122.445) +
	1.095 *	0.883 *	15.427) +
	1.008 *	0.989 *	30.229) + = 167.493
Qmax (2) =			
	0.923 *	1.000 *	122.445) +
	1.000 *	1.000 *	15.427) +
	0.921 *	1.000 *	30.229) + = 156.287
Qmax (3) =			
	0.993 *	1.000 *	122.445) +

1.086 \* 0.893 \* 15.427) +  
 1.000 \* 1.000 \* 30.229) + = 166.768

Total of 3 streams to confluence:

Flow rates before confluence point:

122.445 15.427 30.229

Maximum flow rates at confluence using above data:

167.493 156.287 166.768

Area of streams before confluence:

67.485 10.000 20.000

Effective area values after confluence:

96.097 97.485 96.414

Results of confluence:

Total flow rate = 167.493(CFS)

Time of concentration = 21.428 min.

Effective stream area after confluence = 96.097(Ac.)

Stream Area average Pervious fraction(Ap) = 0.202

Stream Area average soil loss rate(Fm) = 0.198(In/Hr)

Study area (this main stream) = 97.49(Ac.)

+++++  
 Process from Point/Station 34.000 to Point/Station 35.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1048.200(Ft.)

Downstream point/station elevation = 1042.000(Ft.)

Pipe length = 660.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 167.493(CFS)

Given pipe size = 39.00(In.)

NOTE: Normal flow is pressure flow in user selected pipe size.

The approximate hydraulic grade line above the pipe invert is

30.445(Ft.) at the headworks or inlet of the pipe(s)

Pipe friction loss = 27.150(Ft.)

Minor friction loss = 9.495(Ft.) K-factor = 1.50

Pipe flow velocity = 20.19(Ft/s)

Travel time through pipe = 0.54 min.

Time of concentration (TC) = 21.97 min.

+++++  
 Process from Point/Station 35.000 to Point/Station 35.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 96.097(Ac.)

Runoff from this stream = 167.493(CFS)

Time of concentration = 21.97 min.

Rainfall intensity = 2.005(In/Hr)

Area averaged loss rate (Fm) = 0.1979(In/Hr)

Area averaged Pervious ratio (Ap) = 0.2024

+++++  
 Process from Point/Station 730.000 to Point/Station 731.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

CONDOMINIUM subarea type

Decimal fraction soil group A = 0.000

Decimal fraction soil group B = 1.000

Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.3500      Max loss rate(Fm)=      0.257(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1063.700(Ft.)  
 Bottom (of initial area) elevation = 1055.800(Ft.)  
 Difference in elevation =      7.900(Ft.)  
 Slope =      0.00790    s(%)=      0.79  
 $TC = k(0.360)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 15.024 min.  
 Rainfall intensity =      2.518(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.808  
 Subarea runoff =      10.176(CFS)  
 Total initial stream area =      5.000(Ac.)  
 Pervious area fraction = 0.350  
 Initial area Fm value =      0.257(In/Hr)

++++++  
 Process from Point/Station      731.000 to Point/Station      732.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1055.800(Ft.)  
 End of street segment elevation = 1053.600(Ft.)  
 Length of street segment = 330.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
   Manning's N in gutter = 0.0150  
   Manning's N from gutter to grade break = 0.0150  
   Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 15.264(CFS)  
 Depth of flow = 0.440(Ft.), Average velocity = 2.504(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 17.254(Ft.)  
 Flow velocity = 2.50(Ft/s)  
 Travel time = 2.20 min.      TC = 17.22 min.  
 Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.3500      Max loss rate(Fm)=      0.257(In/Hr)  
 Rainfall intensity =      2.320(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.800  
 Subarea runoff =      8.394(CFS) for      5.000(Ac.)  
 Total runoff =      18.570(CFS)  
 Effective area this stream =      10.00(Ac.)  
 Total Study Area (Main Stream No. 1) =      108.00(Ac.)  
 Area averaged Fm value =      0.257(In/Hr)

Street flow at end of street = 18.570(CFS)  
 Half street flow at end of street = 9.285(CFS)  
 Depth of flow = 0.467(Ft.), Average velocity = 2.628(Ft/s)  
 Flow width (from curb towards crown)= 18.607(Ft.)

+++++  
 Process from Point/Station 732.000 to Point/Station 733.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1053.600(Ft.)  
 End of street segment elevation = 1049.000(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 27.855(CFS)  
 Depth of flow = 0.656(Ft.), Average velocity = 3.510(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 28.045(Ft.)  
 Flow velocity = 3.51(Ft/s)  
 Travel time = 3.13 min. TC = 20.35 min.  
 Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)  
 Rainfall intensity = 2.099(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.772  
 Subarea runoff = 13.815(CFS) for 10.000(Ac.)  
 Total runoff = 32.385(CFS)  
 Effective area this stream = 20.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 118.00(Ac.)  
 Area averaged Fm value = 0.300(In/Hr)  
 Street flow at end of street = 32.385(CFS)  
 Half street flow at end of street = 32.385(CFS)  
 Depth of flow = 0.695(Ft.), Average velocity = 3.567(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 1.40(Ft.)  
 Flow width (from curb towards crown)= 29.981(Ft.)

+++++  
 Process from Point/Station 733.000 to Point/Station 733.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

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Along Main Stream number: 1 in normal stream number 2

Stream flow area = 20.000 (Ac.)  
 Runoff from this stream = 32.385 (CFS)  
 Time of concentration = 20.35 min.  
 Rainfall intensity = 2.099 (In/Hr)  
 Area averaged loss rate (Fm) = 0.2996 (In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.3500  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	167.493	21.97	2.005
2	32.385	20.35	2.099
Qmax(1) =			
	1.000 *	1.000 *	167.493) +
	0.948 *	1.000 *	32.385) + = 198.184
Qmax(2) =			
	1.052 *	0.926 *	167.493) +
	1.000 *	1.000 *	32.385) + = 195.630

Total of 2 streams to confluence:

Flow rates before confluence point:  
 167.493      32.385

Maximum flow rates at confluence using above data:  
 198.184      195.630

Area of streams before confluence:  
 96.097      20.000

Effective area values after confluence:  
 116.097      109.023

Results of confluence:

Total flow rate = 198.184 (CFS)

Time of concentration = 21.972 min.

Effective stream area after confluence = 116.097 (Ac.)

Stream Area average Pervious fraction (Ap) = 0.228

Stream Area average soil loss rate (Fm) = 0.215 (In/Hr)

Study area (this main stream) = 116.10 (Ac.)

End of computations, Total Study Area = 118.00 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction (Ap) = 0.227

Area averaged SCS curve number = 34.0

LINE "DZ-7"

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
Rational Hydrology Study Date: 01/13/05

FONTANA / LINE DZ-7 HYDROLOGY  
25 YEAR STORM  
JN 04339

Hall & Forman, Inc. - S/N 950

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

Rational hydrology study storm event year is 25.0  
10 Year storm 1 hour rainfall = 0.930(In.)  
100 Year storm 1 hour rainfall = 1.350(In.)  
Computed rainfall intensity:  
Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
Slope used for rainfall intensity curve b = 0.6000  
Soil antecedent moisture condition (AMC) = 2

++++  
Process from Point/Station 800.000 to Point/Station 801.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

COMMERCIAL subarea type  
Decimal fraction soil group A = 1.000  
Decimal fraction soil group B = 0.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
SCS curve number for soil(AMC 2) = 32.00  
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)  
Initial subarea data:  
Initial area flow distance = 1000.000(Ft.)  
Top (of initial area) elevation = 1098.000(Ft.)  
Bottom (of initial area) elevation = 1088.000(Ft.)  
Difference in elevation = 10.000(Ft.)  
Slope = 0.01000 s(%)= 1.00  
TC = k(0.304)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 12.102 min.  
Rainfall intensity = 2.867(In/Hr) for a 25.0 year storm  
Effective runoff coefficient used for area (Q=KCIA) is C = 0.869  
Subarea runoff = 14.954(CFS)  
Total initial stream area = 6.000(Ac.)  
Pervious area fraction = 0.100  
Initial area Fm value = 0.098(In/Hr)

++++  
Process from Point/Station 801.000 to Point/Station 802.000  
\*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1088.000(Ft.)  
End of street segment elevation = 1081.000(Ft.)  
Length of street segment = 820.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 27.415(CFS)  
 Depth of flow = 0.505(Ft.), Average velocity = 3.213(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 3.21(Ft/s)  
 Travel time = 4.25 min. TC = 16.36 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098(In/Hr)  
 Rainfall intensity = 2.393(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.863  
 Subarea runoff = 18.097(CFS) for 10.000(Ac.)  
 Total runoff = 33.051(CFS)  
 Effective area this stream = 16.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 16.00(Ac.)  
 Area averaged Fm value = 0.098(In/Hr)  
 Street flow at end of street = 33.051(CFS)  
 Half street flow at end of street = 16.526(CFS)  
 Depth of flow = 0.530(Ft.), Average velocity = 3.461(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 802.000 to Point/Station 803.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1081.000(Ft.)  
 End of street segment elevation = 1075.000(Ft.)  
 Length of street segment = 620.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150

Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 53.708 (CFS)  
 Depth of flow = 0.785 (Ft.), Average velocity = 4.365 (Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 5.89 (Ft.)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 34.476 (Ft.)  
 Flow velocity = 4.37 (Ft/s)  
 Travel time = 2.37 min. TC = 18.72 min.  
 Adding area flow to street  
 COMMERCIAL subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil (AMC 2) = 32.00  
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.098 (In/Hr)  
 Rainfall intensity = 2.207 (In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.860  
 Subarea runoff = 35.274 (CFS) for 20.000 (Ac.)  
 Total runoff = 68.325 (CFS)  
 Effective area this stream = 36.00 (Ac.)  
 Total Study Area (Main Stream No. 1) = 36.00 (Ac.)  
 Area averaged Fm value = 0.098 (In/Hr)  
 Street flow at end of street = 68.325 (CFS)  
 Half street flow at end of street = 68.325 (CFS)  
 Depth of flow = 0.848 (Ft.), Average velocity = 4.539 (Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 9.05 (Ft.)  
 Flow width (from curb towards crown) = 37.634 (Ft.)

++++++  
 Process from Point/Station 803.000 to Point/Station 36.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1069.000 (Ft.)  
 Downstream point/station elevation = 1054.000 (Ft.)  
 Pipe length = 990.00 (Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 68.325 (CFS)  
 Given pipe size = 36.00 (In.)  
 Calculated individual pipe flow = 68.325 (CFS)  
 Normal flow depth in pipe = 25.08 (In.)  
 Flow top width inside pipe = 33.10 (In.)  
 Critical Depth = 31.61 (In.)  
 Pipe flow velocity = 12.99 (Ft/s)  
 Travel time through pipe = 1.27 min.  
 Time of concentration (TC) = 19.99 min.

++++++  
 Process from Point/Station 36.000 to Point/Station 36.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 36.000 (Ac.)  
 Runoff from this stream = 68.325 (CFS)  
 Time of concentration = 19.99 min.  
 Rainfall intensity = 2.121 (In/Hr)

Area averaged loss rate (Fm) = 0.0978 (In/Hr)  
Area averaged Pervious ratio (Ap) = 0.1000

+++++  
Process from Point/Station 804.000 to Point/Station 805.000  
\*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

COMMERCIAL subarea type  
Decimal fraction soil group A = 1.000  
Decimal fraction soil group B = 0.000  
Decimal fraction soil group C = 0.000  
Decimal fraction soil group D = 0.000  
SCS curve number for soil(AMC 2) = 32.00  
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.098 (In/Hr)  
Initial subarea data:  
Initial area flow distance = 1000.000(Ft.)  
Top (of initial area) elevation = 1081.500(Ft.)  
Bottom (of initial area) elevation = 1071.000(Ft.)  
Difference in elevation = 10.500(Ft.)  
Slope = 0.01050 s(%)= 1.05  
TC = k(0.304)\*[(length^3)/(elevation change)]^0.2  
Initial area time of concentration = 11.985 min.  
Rainfall intensity = 2.884(In/Hr) for a 25.0 year storm  
Effective runoff coefficient used for area (Q=KCIA) is C = 0.869  
Subarea runoff = 12.537(CFS)  
Total initial stream area = 5.000(Ac.)  
Pervious area fraction = 0.100  
Initial area Fm value = 0.098 (In/Hr)

+++++  
Process from Point/Station 805.000 to Point/Station 806.000  
\*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1071.000(Ft.)  
End of street segment elevation = 1069.000(Ft.)  
Length of street segment = 660.000(Ft.)  
Height of curb above gutter flowline = 8.0(In.)  
Width of half street (curb to crown) = 20.000(Ft.)  
Distance from crown to crossfall grade break = 18.500(Ft.)  
Slope from gutter to grade break (v/hz) = 0.020  
Slope from grade break to crown (v/hz) = 0.020  
Street flow is on [2] side(s) of the street  
Distance from curb to property line = 10.000(Ft.)  
Slope from curb to property line (v/hz) = 0.020  
Gutter width = 1.500(Ft.)  
Gutter hike from flowline = 1.500(In.)  
Manning's N in gutter = 0.0150  
Manning's N from gutter to grade break = 0.0150  
Manning's N from grade break to crown = 0.0150  
Estimated mean flow rate at midpoint of street = 25.074(CFS)  
Depth of flow = 0.568(Ft.), Average velocity = 2.270(Ft/s)  
Note: depth of flow exceeds top of street crown.  
Streetflow hydraulics at midpoint of street travel:  
Halfstreet flow width = 20.000(Ft.)  
Flow velocity = 2.27(Ft/s)  
Travel time = 4.85 min. TC = 16.83 min.  
Adding area flow to street  
COMMERCIAL subarea type  
Decimal fraction soil group A = 1.000

Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.1000      Max loss rate(Fm)=      0.098(In/Hr)  
 Rainfall intensity =      2.352(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.863  
 Subarea runoff =      17.897(CFS) for      10.000(Ac.)  
 Total runoff =      30.435(CFS)  
 Effective area this stream =      15.00(Ac.)  
 Total Study Area (Main Stream No. 1) =      51.00(Ac.)  
 Area averaged Fm value =      0.098(In/Hr)  
 Street flow at end of street =      30.435(CFS)  
 Half street flow at end of street =      15.217(CFS)  
 Depth of flow =      0.602(Ft.), Average velocity =      2.451(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)=      20.000(Ft.)

++++++  
 Process from Point/Station      806.000 to Point/Station      807.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1069.000(Ft.)  
 End of street segment elevation = 1065.000(Ft.)  
 Length of street segment = 330.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street =      35.507(CFS)  
 Depth of flow =      0.516(Ft.), Average velocity =      3.958(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 3.96(Ft/s)  
 Travel time = 1.39 min.      TC = 18.22 min.

Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.489(In/Hr)  
 Rainfall intensity =      2.243(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.822  
 Subarea runoff =      6.417(CFS) for      5.000(Ac.)  
 Total runoff =      36.851(CFS)  
 Effective area this stream =      20.00(Ac.)

Total Study Area (Main Stream No. 1) = 56.00(Ac.)  
 Area averaged Fm value = 0.196(In/Hr)  
 Street flow at end of street = 36.851(CFS)  
 Half street flow at end of street = 18.426(CFS)  
 Depth of flow = 0.521(Ft.), Average velocity = 4.016(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

+++++  
 Process from Point/Station 807.000 to Point/Station 808.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1065.000(Ft.)  
 End of street segment elevation = 1060.000(Ft.)  
 Length of street segment = 330.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 46.064(CFS)  
 Depth of flow = 0.685(Ft.), Average velocity = 5.249(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 0.91(Ft.)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 29.489(Ft.)  
 Flow velocity = 5.25(Ft/s)  
 Travel time = 1.05 min. TC = 19.27 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)  
 Rainfall intensity = 2.169(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.778  
 Subarea runoff = 13.788(CFS) for 10.000(Ac.)  
 Total runoff = 50.639(CFS)  
 Effective area this stream = 30.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 66.00(Ac.)  
 Area averaged Fm value = 0.293(In/Hr)  
 Street flow at end of street = 50.639(CFS)  
 Half street flow at end of street = 50.639(CFS)  
 Depth of flow = 0.710(Ft.), Average velocity = 5.281(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 2.19(Ft.)  
 Flow width (from curb towards crown)= 30.772(Ft.)

\*\*\*\*\*  
 Process from Point/Station 808.000 to Point/Station 808.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
 Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 30.000(Ac.)  
 Runoff from this stream = 50.639(CFS)  
 Time of concentration = 19.27 min.  
 Rainfall intensity = 2.169(In/Hr)  
 Area averaged loss rate (Fm) = 0.2933(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.3000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	68.325	19.99	2.121
2	50.639	19.27	2.169
Qmax(1) =			
	1.000 *	1.000 *	68.325) +
	0.975 *	1.000 *	50.639) + = 117.682
Qmax(2) =			
	1.023 *	0.964 *	68.325) +
	1.000 *	1.000 *	50.639) + = 118.035

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 68.325 50.639  
 Maximum flow rates at confluence using above data:  
 117.682 118.035  
 Area of streams before confluence:  
 36.000 30.000  
 Effective area values after confluence:  
 66.000 64.696  
 Results of confluence:  
 Total flow rate = 118.035(CFS)  
 Time of concentration = 19.269 min.  
 Effective stream area after confluence = 64.696(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.191  
 Stream Area average soil loss rate(Fm) = 0.187(In/Hr)  
 Study area (this main stream) = 66.00(Ac.)

\*\*\*\*\*  
 Process from Point/Station 36.000 to Point/Station 37.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

-----  
 Upstream point/station elevation = 1054.000(Ft.)  
 Downstream point/station elevation = 1043.500(Ft.)  
 Pipe length = 990.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 118.035(CFS)  
 Given pipe size = 42.00(In.)  
 NOTE: Normal flow is pressure flow in user selected pipe size.  
 The approximate hydraulic grade line above the pipe invert is  
 6.627(Ft.) at the headworks or inlet of the pipe(s)  
 Pipe friction loss = 13.622(Ft.)  
 Minor friction loss = 3.506(Ft.) K-factor = 1.50  
 Pipe flow velocity = 12.27(Ft/s)  
 Travel time through pipe = 1.34 min.  
 Time of concentration (TC) = 20.61 min.

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Process from Point/Station      37.000 to Point/Station      37.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 1
Stream flow area =      64.696(Ac.)
Runoff from this stream =    118.035(CFS)
Time of concentration =    20.61 min.
Rainfall intensity =      2.083(In/Hr)
Area averaged loss rate (Fm) =    0.1867(In/Hr)
Area averaged Pervious ratio (Ap) = 0.1909

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Process from Point/Station      809.000 to Point/Station      810.000
**** INITIAL AREA EVALUATION ****

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RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 32.00
Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.489(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1068.000(Ft.)
Bottom (of initial area) elevation = 1061.000(Ft.)
Difference in elevation =      7.000(Ft.)
Slope =      0.00700 s(%)=      0.70
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 16.631 min.
Rainfall intensity =      2.369(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.714
Subarea runoff =      8.461(CFS)
Total initial stream area =      5.000(Ac.)
Pervious area fraction = 0.500
Initial area Fm value =      0.489(In/Hr)

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Process from Point/Station      810.000 to Point/Station      811.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

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Top of street segment elevation = 1061.000(Ft.)
End of street segment elevation = 1057.000(Ft.)
Length of street segment = 660.000(Ft.)
Height of curb above gutter flowline = 8.0(In.)
Width of half street (curb to crown) = 20.000(Ft.)
Distance from crown to crossfall grade break = 18.500(Ft.)
Slope from gutter to grade break (v/hz) = 0.020
Slope from grade break to crown (v/hz) = 0.020
Street flow is on [2] side(s) of the street
Distance from curb to property line = 10.000(Ft.)
Slope from curb to property line (v/hz) = 0.020
Gutter width = 1.500(Ft.)
Gutter hike from flowline = 1.500(In.)
Manning's N in gutter = 0.0150
Manning's N from gutter to grade break = 0.0150

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Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 12.692 (CFS)  
 Depth of flow = 0.422(Ft.), Average velocity = 2.308(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 16.366(Ft.)  
 Flow velocity = 2.31(Ft/s)  
 Travel time = 4.77 min. TC = 21.40 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)  
 Rainfall intensity = 2.037(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.684  
 Subarea runoff = 5.469(CFS) for 5.000(Ac.)  
 Total runoff = 13.930(CFS)  
 Effective area this stream = 10.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 76.00(Ac.)  
 Area averaged Fm value = 0.489(In/Hr)  
 Street flow at end of street = 13.930(CFS)  
 Half street flow at end of street = 6.965(CFS)  
 Depth of flow = 0.434(Ft.), Average velocity = 2.361(Ft/s)  
 Flow width (from curb towards crown)= 16.965(Ft.)

+++++  
 Process from Point/Station 811.000 to Point/Station 812.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

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Top of street segment elevation = 1057.000(Ft.)  
 End of street segment elevation = 1051.000(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 27.861(CFS)  
 Depth of flow = 0.628(Ft.), Average velocity = 3.878(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 26.670(Ft.)  
 Flow velocity = 3.88(Ft/s)  
 Travel time = 2.84 min. TC = 24.23 min.  
 Adding area flow to street  
 SCHOOL subarea  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.6000 Max loss rate(Fm)= 0.587(In/Hr)  
 Rainfall intensity = 1.890(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified rational method)(Q=KCIA) is C = 0.636  
 Subarea runoff = 22.143(CFS) for 20.000(Ac.)  
 Total runoff = 36.073(CFS)  
 Effective area this stream = 30.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 96.00(Ac.)  
 Area averaged Fm value = 0.554(In/Hr)  
 Street flow at end of street = 36.073(CFS)  
 Half street flow at end of street = 36.073(CFS)  
 Depth of flow = 0.688(Ft.), Average velocity = 4.068(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 1.06(Ft.)  
 Flow width (from curb towards crown)= 29.640(Ft.)

\*\*\*\*\*  
 Process from Point/Station 812.000 to Point/Station 812.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 30.000(Ac.)  
 Runoff from this stream = 36.073(CFS)  
 Time of concentration = 24.23 min.  
 Rainfall intensity = 1.890(In/Hr)  
 Area averaged loss rate (Fm) = 0.5541(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5667  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	118.035	20.61	2.083
2	36.073	24.23	1.890
Qmax(1) =			
	1.000 *	1.000 *	118.035) +
	1.144 *	0.851 *	36.073) + = 153.145
Qmax(2) =			
	0.898 *	1.000 *	118.035) +
	1.000 *	1.000 *	36.073) + = 142.114

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 118.035 36.073  
 Maximum flow rates at confluence using above data:  
 153.145 142.114  
 Area of streams before confluence:  
 64.696 30.000  
 Effective area values after confluence:  
 90.215 94.696  
 Results of confluence:  
 Total flow rate = 153.145(CFS)  
 Time of concentration = 20.614 min.  
 Effective stream area after confluence = 90.215(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.310  
 Stream Area average soil loss rate(Fm) = 0.303(In/Hr)  
 Study area (this main stream) = 94.70(Ac.)

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+++++
Process from Point/Station      37.000 to Point/Station      38.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****

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Upstream point/station elevation = 1043.500(Ft.)
Downstream point/station elevation = 1038.000(Ft.)
Pipe length = 660.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 153.145(CFS)
Given pipe size = 42.00(In.)
NOTE: Normal flow is pressure flow in user selected pipe size.
The approximate hydraulic grade line above the pipe invert is
      15.689(Ft.) at the headworks or inlet of the pipe(s)
Pipe friction loss = 15.287(Ft.)
Minor friction loss = 5.901(Ft.) K-factor = 1.50
Pipe flow velocity = 15.92(Ft/s)
Travel time through pipe = 0.69 min.
Time of concentration (TC) = 21.31 min.

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+++++
Process from Point/Station      38.000 to Point/Station      38.000
**** CONFLUENCE OF MINOR STREAMS ****

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Along Main Stream number: 1 in normal stream number 1
Stream flow area = 90.215(Ac.)
Runoff from this stream = 153.145(CFS)
Time of concentration = 21.31 min.
Rainfall intensity = 2.042(In/Hr)
Area averaged loss rate (Fm) = 0.3031(In/Hr)
Area averaged Pervious ratio (Ap) = 0.3099

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+++++
Process from Point/Station      813.000 to Point/Station      814.000
**** INITIAL AREA EVALUATION ****

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CONDOMINIUM subarea type
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 32.00
Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1056.600(Ft.)
Bottom (of initial area) elevation = 1048.500(Ft.)
Difference in elevation = 8.100(Ft.)
Slope = 0.00810 s(%)= 0.81
TC = k(0.360)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 14.949 min.
Rainfall intensity = 2.526(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.778
Subarea runoff = 9.826(CFS)
Total initial stream area = 5.000(Ac.)
Pervious area fraction = 0.350
Initial area Fm value = 0.342(In/Hr)

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Process from Point/Station 814.000 to Point/Station 815.000  
\*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1048.500(Ft.)  
 End of street segment elevation = 1047.300(Ft.)  
 Length of street segment = 330.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 14.739(CFS)  
 Depth of flow = 0.478(Ft.), Average velocity = 1.976(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 19.128(Ft.)  
 Flow velocity = 1.98(Ft/s)  
 Travel time = 2.78 min. TC = 17.73 min.  
 Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)  
 Rainfall intensity = 2.280(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.765  
 Subarea runoff = 7.612(CFS) for 5.000(Ac.)  
 Total runoff = 17.438(CFS)  
 Effective area this stream = 10.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 106.00(Ac.)  
 Area averaged Fm value = 0.342(In/Hr)  
 Street flow at end of street = 17.438(CFS)  
 Half street flow at end of street = 8.719(CFS)  
 Depth of flow = 0.501(Ft.), Average velocity = 2.076(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 815.000 to Point/Station 816.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1047.300(Ft.)  
 End of street segment elevation = 1045.000(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street

Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 26.156(CFS)  
 Depth of flow = 0.563(Ft.), Average velocity = 2.407(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 2.41(Ft/s)  
 Travel time = 4.57 min. TC = 22.30 min.

Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)  
 Rainfall intensity = 1.987(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.745  
 Subarea runoff = 12.164(CFS) for 10.000(Ac.)  
 Total runoff = 29.601(CFS)  
 Effective area this stream = 20.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 116.00(Ac.)  
 Area averaged Fm value = 0.342(In/Hr)  
 Street flow at end of street = 29.601(CFS)  
 Half street flow at end of street = 14.801(CFS)  
 Depth of flow = 0.584(Ft.), Average velocity = 2.528(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

\*\*\*\*\*  
 Process from Point/Station 816.000 to Point/Station 816.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 20.000(Ac.)  
 Runoff from this stream = 29.601(CFS)  
 Time of concentration = 22.30 min.  
 Rainfall intensity = 1.987(In/Hr)  
 Area averaged loss rate (Fm) = 0.3422(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.3500  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	153.145	21.31	2.042
2	29.601	22.30	1.987
Qmax(1) =	1.000 *	1.000 *	153.145) +
	1.034 *	0.955 *	29.601) + = 182.373
Qmax(2) =	0.968 *	1.000 *	153.145) +

$$1.000 * 1.000 * 29.601) + = 177.878$$

Total of 2 streams to confluence:

Flow rates before confluence point:

153.145      29.601

Maximum flow rates at confluence using above data:

182.373      177.878

Area of streams before confluence:

90.215      20.000

Effective area values after confluence:

109.321      110.215

Results of confluence:

Total flow rate = 182.373(CFS)

Time of concentration = 21.305 min.

Effective stream area after confluence = 109.321(Ac.)

Stream Area average Pervious fraction( $A_p$ ) = 0.317

Stream Area average soil loss rate( $F_m$ ) = 0.310(In/Hr)

Study area (this main stream) = 110.22(Ac.)

End of computations, Total Study Area = 116.00 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction( $A_p$ ) = 0.316

Area averaged SCS curve number = 32.0

LINE "DZ-5"

## San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
 Rational Hydrology Study Date: 01/13/05

-----  
 FONTANA / LINE DZ-5 HYDROLOGY  
 25 YEAR STORM  
 JN 04339

-----  
 Hall & Forman, Inc. - S/N 950

-----  
 \*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*

-----  
 Rational hydrology study storm event year is 25.0  
 10 Year storm 1 hour rainfall = 0.930(In.)  
 100 Year storm 1 hour rainfall = 1.350(In.)  
 Computed rainfall intensity:  
 Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
 Slope used for rainfall intensity curve b = 0.6000  
 Soil antecedent moisture condition (AMC) = 2

+++++  
 Process from Point/Station 700.000 to Point/Station 701.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

-----  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm) = 0.342(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1104.000(Ft.)  
 Bottom (of initial area) elevation = 1096.700(Ft.)  
 Difference in elevation = 7.300(Ft.)  
 Slope = 0.00730 s(%) = 0.73  
 $TC = k(0.360) * [(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 15.263 min.  
 Rainfall intensity = 2.494(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.777  
 Subarea runoff = 9.685(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.350  
 Initial area Fm value = 0.342(In/Hr)

+++++  
 Process from Point/Station 701.000 to Point/Station 702.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

-----  
 Top of street segment elevation = 1096.700(Ft.)  
 End of street segment elevation = 1095.000(Ft.)  
 Length of street segment = 330.000(Ft.)

Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 14.527 (CFS)  
 Depth of flow = 0.451(Ft.), Average velocity = 2.244(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 17.791(Ft.)  
 Flow velocity = 2.24(Ft/s)  
 Travel time = 2.45 min. TC = 17.71 min.  
 Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)  
 Rainfall intensity = 2.281(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.765  
 Subarea runoff = 7.766(CFS) for 5.000(Ac.)  
 Total runoff = 17.451(CFS)  
 Effective area this stream = 10.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 10.00(Ac.)  
 Area averaged Fm value = 0.342(In/Hr)  
 Street flow at end of street = 17.451(CFS)  
 Half street flow at end of street = 8.725(CFS)  
 Depth of flow = 0.477(Ft.), Average velocity = 2.348(Ft/s)  
 Flow width (from curb towards crown)= 19.090(Ft.)

++++++  
 Process from Point/Station 702.000 to Point/Station 703.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1095.000(Ft.)  
 End of street segment elevation = 1092.000(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150

Estimated mean flow rate at midpoint of street = 26.176(CFS)  
 Depth of flow = 0.542(Ft.), Average velocity = 2.609(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 2.61(Ft/s)  
 Travel time = 4.22 min. TC = 21.93 min.

Adding area flow to street

CONDOMINIUM subarea type

Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)  
 Rainfall intensity = 2.007(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.747  
 Subarea runoff = 12.513(CFS) for 10.000(Ac.)  
 Total runoff = 29.964(CFS)  
 Effective area this stream = 20.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 20.00(Ac.)  
 Area averaged Fm value = 0.342(In/Hr)  
 Street flow at end of street = 29.964(CFS)  
 Half street flow at end of street = 14.982(CFS)  
 Depth of flow = 0.564(Ft.), Average velocity = 2.753(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

\*\*\*\*\*  
 Process from Point/Station 703.000 to Point/Station 704.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1092.000(Ft.)  
 End of street segment elevation = 1082.000(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 44.946(CFS)  
 Depth of flow = 0.678(Ft.), Average velocity = 5.244(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 0.56(Ft.)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 29.148(Ft.)  
 Flow velocity = 5.24(Ft/s)  
 Travel time = 2.10 min. TC = 24.03 min.  
 Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000

Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500      Max loss rate(Fm)=      0.342(In/Hr)  
 Rainfall intensity =      1.900(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.738  
 Subarea runoff =      26.111(CFS) for      20.000(Ac.)  
 Total runoff =      56.075(CFS)  
 Effective area this stream =      40.00(Ac.)  
 Total Study Area (Main Stream No. 1) =      40.00(Ac.)  
 Area averaged Fm value =      0.342(In/Hr)  
 Street flow at end of street =      56.075(CFS)  
 Half street flow at end of street =      56.075(CFS)  
 Depth of flow =      0.737(Ft.), Average velocity =      5.334(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property =      3.53(Ft.)  
 Flow width (from curb towards crown)=      32.118(Ft.)

++++++  
 Process from Point/Station      704.000 to Point/Station      30.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1076.000(Ft.)  
 Downstream point/station elevation = 1066.000(Ft.)  
 Pipe length = 1000.00(Ft.)      Manning's N = 0.013  
 No. of pipes = 1      Required pipe flow =      56.075(CFS)  
 Given pipe size =      36.00(In.)  
 Calculated individual pipe flow =      56.075(CFS)  
 Normal flow depth in pipe =      25.27(In.)  
 Flow top width inside pipe =      32.94(In.)  
 Critical Depth =      29.14(In.)  
 Pipe flow velocity =      10.57(Ft/s)  
 Travel time through pipe =      1.58 min.  
 Time of concentration (TC) =      25.60 min.

++++++  
 Process from Point/Station      30.000 to Point/Station      30.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area =      40.000(Ac.)  
 Runoff from this stream =      56.075(CFS)  
 Time of concentration =      25.60 min.  
 Rainfall intensity =      1.829(In/Hr)  
 Area averaged loss rate (Fm) =      0.3422(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.3500

++++++  
 Process from Point/Station      705.000 to Point/Station      706.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000

SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1085.700(Ft.)  
 Bottom (of initial area) elevation = 1075.300(Ft.)  
 Difference in elevation = 10.400(Ft.)  
 Slope = 0.01040 s(%)= 1.04  
 $TC = k(0.360)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 14.220 min.  
 Rainfall intensity = 2.603(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.782  
 Subarea runoff = 20.344(CFS)  
 Total initial stream area = 10.000(Ac.)  
 Pervious area fraction = 0.350  
 Initial area Fm value = 0.342(In/Hr)

+++++  
 Process from Point/Station 706.000 to Point/Station 707.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1075.300(Ft.)  
 End of street segment elevation = 1072.000(Ft.)  
 Length of street segment = 330.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 27.972(CFS)  
 Depth of flow = 0.497(Ft.), Average velocity = 3.397(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 3.40(Ft/s)  
 Travel time = 1.62 min. TC = 15.84 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 2.440(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.770  
 Subarea runoff = 12.523(CFS) for 7.500(Ac.)  
 Total runoff = 32.866(CFS)  
 Effective area this stream = 17.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 57.50(Ac.)  
 Area averaged Fm value = 0.353(In/Hr)

Street flow at end of street = 32.866(CFS)  
 Half street flow at end of street = 16.433(CFS)  
 Depth of flow = 0.518(Ft.), Average velocity = 3.622(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++  
 Process from Point/Station 707.000 to Point/Station 707.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 17.500(Ac.)  
 Runoff from this stream = 32.866(CFS)  
 Time of concentration = 15.84 min.  
 Rainfall intensity = 2.440(In/Hr)  
 Area averaged loss rate (Fm) = 0.3528(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.4143  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	56.075	25.60	1.829
2	32.866	15.84	2.440
Qmax(1) =	1.000 * 56.075 +	1.000 * 32.866 +	79.321
Qmax(2) =	1.411 * 56.075 +	1.000 * 32.866 +	81.807

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 56.075      32.866  
 Maximum flow rates at confluence using above data:  
 79.321      81.807  
 Area of streams before confluence:  
 40.000      17.500  
 Effective area values after confluence:  
 57.500      42.244  
 Results of confluence:  
 Total flow rate = 81.807(CFS)  
 Time of concentration = 15.839 min.  
 Effective stream area after confluence = 42.244(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.370  
 Stream Area average soil loss rate(Fm) = 0.345(In/Hr)  
 Study area (this main stream) = 57.50(Ac.)

++++  
 Process from Point/Station 30.000 to Point/Station 31.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1066.000(Ft.)  
 Downstream point/station elevation = 1062.200(Ft.)  
 Pipe length = 990.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 81.807(CFS)  
 Given pipe size = 39.00(In.)  
 NOTE: Normal flow is pressure flow in user selected pipe size.

The approximate hydraulic grade line above the pipe invert is  
 8.180(Ft.) at the headworks or inlet of the pipe(s)  
 Pipe friction loss = 9.715(Ft.)  
 Minor friction loss = 2.265(Ft.) K-factor = 1.50  
 Pipe flow velocity = 9.86(Ft/s)  
 Travel time through pipe = 1.67 min.  
 Time of concentration (TC) = 17.51 min.

++++  
 Process from Point/Station 31.000 to Point/Station 31.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 42.244(Ac.)  
 Runoff from this stream = 81.807(CFS)  
 Time of concentration = 17.51 min.  
 Rainfall intensity = 2.297(In/Hr)  
 Area averaged loss rate (Fm) = 0.3455(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.3696

++++  
 Process from Point/Station 708.000 to Point/Station 709.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1072.000(Ft.)  
 Bottom (of initial area) elevation = 1069.200(Ft.)  
 Difference in elevation = 2.800(Ft.)  
 Slope = 0.00280 s(%) = 0.28  
 $TC = k(0.389) * [(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 19.976 min.  
 Rainfall intensity = 2.122(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.744  
 Subarea runoff = 11.850(CFS)  
 Total initial stream area = 7.500(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.367(In/Hr)

++++  
 Process from Point/Station 709.000 to Point/Station 710.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1069.200(Ft.)  
 End of street segment elevation = 1062.600(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020

Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 27.649(CFS)  
 Depth of flow = 0.617(Ft.), Average velocity = 4.012(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 26.116(Ft.)  
 Flow velocity = 4.01(Ft/s)  
 Travel time = 2.74 min. TC = 22.72 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.367(In/Hr)  
 Rainfall intensity = 1.965(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.732  
 Subarea runoff = 27.697(CFS) for 20.000(Ac.)  
 Total runoff = 39.547(CFS)  
 Effective area this stream = 27.50(Ac.)  
 Total Study Area (Main Stream No. 1) = 85.00(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 39.547(CFS)  
 Half street flow at end of street = 39.547(CFS)  
 Depth of flow = 0.700(Ft.), Average velocity = 4.278(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 1.66(Ft.)  
 Flow width (from curb towards crown)= 30.242(Ft.)

+++++  
 Process from Point/Station 710.000 to Point/Station 710.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
 Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 27.500(Ac.)  
 Runoff from this stream = 39.547(CFS)  
 Time of concentration = 22.72 min.  
 Rainfall intensity = 1.965(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	81.807	17.51	2.297
2	39.547	22.72	1.965
Qmax(1) =	1.000 *	1.000 *	81.807) +
	1.208 *	0.771 *	39.547) + = 118.627
Qmax(2) =			

0.830 *	1.000 *	81.807) +	
1.000 *	1.000 *	39.547) + =	107.433

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
     81.807      39.547  
 Maximum flow rates at confluence using above data:  
     118.627      107.433  
 Area of streams before confluence:  
     42.244      27.500  
 Effective area values after confluence:  
     63.443      69.744

Results of confluence:  
 Total flow rate = 118.627(CFS)  
 Time of concentration = 17.512 min.  
 Effective stream area after confluence = 63.443(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.421  
 Stream Area average soil loss rate(Fm) = 0.354(In/Hr)  
 Study area (this main stream) = 69.74(Ac.)

\*\*\*\*\*  
 Process from Point/Station 31.000 to Point/Station 32.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1056.600(Ft.)  
 Downstream point/station elevation = 1052.000(Ft.)  
 Pipe length = 660.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 118.627(CFS)  
 Given pipe size = 39.00(In.)  
 NOTE: Normal flow is pressure flow in user selected pipe size.  
 The approximate hydraulic grade line above the pipe invert is  
     13.782(Ft.) at the headworks or inlet of the pipe(s)  
 Pipe friction loss = 13.619(Ft.)  
 Minor friction loss = 4.763(Ft.) K-factor = 1.50  
 Pipe flow velocity = 14.30(Ft/s)  
 Travel time through pipe = 0.77 min.  
 Time of concentration (TC) = 18.28 min.

\*\*\*\*\*  
 Process from Point/Station 32.000 to Point/Station 32.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 63.443(Ac.)  
 Runoff from this stream = 118.627(CFS)  
 Time of concentration = 18.28 min.  
 Rainfall intensity = 2.238(In/Hr)  
 Area averaged loss rate (Fm) = 0.3539(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.4210

\*\*\*\*\*  
 Process from Point/Station 711.000 to Point/Station 712.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

---

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1069.600(Ft.)  
 Bottom (of initial area) elevation = 1062.100(Ft.)  
 Difference in elevation =      7.500(Ft.)  
 Slope =      0.00750    s(%)=      0.75  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 16.404 min.  
 Rainfall intensity =      2.389(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.762  
 Subarea runoff =      9.098(CFS)  
 Total initial stream area =      5.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value =      0.367(In/Hr)

++++++  
 Process from Point/Station      712.000 to Point/Station      713.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

---

Top of street segment elevation = 1062.100(Ft.)  
 End of street segment elevation = 1058.000(Ft.)  
 Length of street segment = 990.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street =      22.746(CFS)  
 Depth of flow = 0.669(Ft.), Average velocity =      2.740(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property =      0.11(Ft.)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 28.690(Ft.)  
 Flow velocity = 2.74(Ft/s)  
 Travel time = 6.02 min.      TC = 22.43 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 0.000  
 Decimal fraction soil group B = 1.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 56.00  
 Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)=      0.367(In/Hr)  
 Rainfall intensity =      1.980(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.733  
 Subarea runoff =      19.939(CFS) for 15.000(Ac.)  
 Total runoff =      29.037(CFS)  
 Effective area this stream =      20.00(Ac.)

Total Study Area (Main Stream No. 1) = 105.00(Ac.)  
 Area averaged Fm value = 0.367(In/Hr)  
 Street flow at end of street = 29.037(CFS)  
 Half street flow at end of street = 29.037(CFS)  
 Depth of flow = 0.735(Ft.), Average velocity = 2.786(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 3.41(Ft.)  
 Flow width (from curb towards crown)= 31.992(Ft.)

++++  
 Process from Point/Station 713.000 to Point/Station 713.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 20.000(Ac.)  
 Runoff from this stream = 29.037(CFS)  
 Time of concentration = 22.43 min.  
 Rainfall intensity = 1.980(In/Hr)  
 Area averaged loss rate (Fm) = 0.3670(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	118.627	18.28	2.238
2	29.037	22.43	1.980
Qmax(1) =			
	1.000 *	1.000 *	118.627) +
	1.160 *	0.815 *	29.037) + = 146.088
Qmax(2) =			
	0.863 *	1.000 *	118.627) +
	1.000 *	1.000 *	29.037) + = 131.405

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 118.627 29.037  
 Maximum flow rates at confluence using above data:  
 146.088 131.405  
 Area of streams before confluence:  
 63.443 20.000  
 Effective area values after confluence:  
 79.746 83.443  
 Results of confluence:  
 Total flow rate = 146.088(CFS)  
 Time of concentration = 18.281 min.  
 Effective stream area after confluence = 79.746(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.440  
 Stream Area average soil loss rate(Fm) = 0.357(In/Hr)  
 Study area (this main stream) = 83.44(Ac.)

++++  
 Process from Point/Station 32.000 to Point/Station 35.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

Upstream point/station elevation = 1052.000(Ft.)  
 Downstream point/station elevation = 1041.000(Ft.)  
 Pipe length = 1320.00(Ft.) Manning's N = 0.013

No. of pipes = 1 Required pipe flow = 146.088(CFS)  
 Given pipe size = 51.00(In.)  
 Calculated individual pipe flow = 146.088(CFS)  
 Normal flow depth in pipe = 39.56(In.)  
 Flow top width inside pipe = 42.54(In.)  
 Critical Depth = 42.87(In.)  
 Pipe flow velocity = 12.36(Ft/s)  
 Travel time through pipe = 1.78 min.  
 Time of concentration (TC) = 20.06 min.

\*\*\*\*\*  
 Process from Point/Station 35.000 to Point/Station 35.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 79.746(Ac.)  
 Runoff from this stream = 146.088(CFS)  
 Time of concentration = 20.06 min.  
 Rainfall intensity = 2.117(In/Hr)  
 Area averaged loss rate (Fm) = 0.3571(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.4399

\*\*\*\*\*  
 Process from Point/Station 35.000 to Point/Station 35.000  
 \*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

---

Soil classification AP and SCS values input by user  
 USER INPUT of soil data for subarea  
 SCS curve number for soil(AMC 2) = 36.98  
 Pervious ratio(Ap) = 0.2280 Max loss rate(Fm)= 0.215(In/Hr)  
 Rainfall intensity = 2.005(In/Hr) for a 25.0 year storm  
 User specified values are as follows:  
 TC = 21.97 min. Rain intensity = 2.00(In/Hr)  
 Total area this stream = 116.10(Ac.)  
 Total Study Area (Main Stream No. 1) = 221.10(Ac.)  
 Total runoff = 198.18(CFS)

\*\*\*\*\*  
 Process from Point/Station 35.000 to Point/Station 35.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 116.100(Ac.)  
 Runoff from this stream = 198.180(CFS)  
 Time of concentration = 21.97 min.  
 Rainfall intensity = 2.005(In/Hr)  
 Area averaged loss rate (Fm) = 0.2150(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.2280  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	146.088	20.06	2.117
2	198.180	21.97	2.005
Qmax(1) =			
	1.000 *	1.000 *	146.088) +

	1.063 *	0.913 *	198.180) + =	338.411
Qmax(2) =	0.936 *	1.000 *	146.088) +	
	1.000 *	1.000 *	198.180) + =	334.941

Total of 2 streams to confluence:  
Flow rates before confluence point:  
146.088      198.180  
Maximum flow rates at confluence using above data:  
338.411      334.941  
Area of streams before confluence:  
79.746      116.100  
Effective area values after confluence:  
185.759      195.846

Results of confluence:  
Total flow rate = 338.411(CFS)  
Time of concentration = 20.061 min.  
Effective stream area after confluence = 185.759(Ac.)  
Stream Area average Pervious fraction(Ap) = 0.314  
Stream Area average soil loss rate(Fm) = 0.273(In/Hr)  
Study area (this main stream) = 195.85(Ac.)

\*\*\*\*\*  
Process from Point/Station      35.000 to Point/Station      38.000  
\*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1041.000(Ft.)  
Downstream point/station elevation = 1035.000(Ft.)  
Pipe length = 1320.00(Ft.)      Manning's N = 0.013  
No. of pipes = 1      Required pipe flow = 338.411(CFS)  
Given pipe size = 84.00(In.)  
Calculated individual pipe flow = 338.411(CFS)  
Normal flow depth in pipe = 56.06(In.)  
Flow top width inside pipe = 79.15(In.)  
Critical Depth = 58.21(In.)  
Pipe flow velocity = 12.39(Ft/s)  
Travel time through pipe = 1.78 min.  
Time of concentration (TC) = 21.84 min.

\*\*\*\*\*  
Process from Point/Station      38.000 to Point/Station      38.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
Stream flow area = 185.759(Ac.)  
Runoff from this stream = 338.411(CFS)  
Time of concentration = 21.84 min.  
Rainfall intensity = 2.012(In/Hr)  
Area averaged loss rate (Fm) = 0.2728(In/Hr)  
Area averaged Pervious ratio (Ap) = 0.3143

\*\*\*\*\*  
Process from Point/Station      38.000 to Point/Station      38.000  
\*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

---

Soil classification AP and SCS values input by user  
USER INPUT of soil data for subarea  
SCS curve number for soil(AMC 2) = 31.98

Pervious ratio(Ap) = 0.3170      Max loss rate(Fm)=      0.310(In/Hr)  
 Rainfall intensity =      2.042(In/Hr) for a      25.0 year storm  
 User specified values are as follows:  
 TC = 21.31 min.      Rain intensity =      2.04(In/Hr)  
 Total area this stream =      109.32(Ac.)  
 Total Study Area (Main Stream No. 1) =      330.42(Ac.)  
 Total runoff =      182.37(CFS)

++++  
 Process from Point/Station      38.000 to Point/Station      38.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

-----  
 Along Main Stream number: 1 in normal stream number 2  
 Stream flow area =      109.320(Ac.)  
 Runoff from this stream =      182.370(CFS)  
 Time of concentration =      21.31 min.  
 Rainfall intensity =      2.042(In/Hr)  
 Area averaged loss rate (Fm) =      0.3100(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.3170  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	338.411	21.84	2.012
2	182.370	21.31	2.042
Qmax(1) =			
	1.000 *	1.000 *	338.411) +
	0.983 *	1.000 *	182.370) + =      517.654
Qmax(2) =			
	1.017 *	0.976 *	338.411) +
	1.000 *	1.000 *	182.370) + =      518.256

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
     338.411      182.370  
 Maximum flow rates at confluence using above data:  
     517.654      518.256  
 Area of streams before confluence:  
     185.759      109.320  
 Effective area values after confluence:  
     295.079      290.599  
 Results of confluence:  
 Total flow rate =      518.256(CFS)  
 Time of concentration =      21.310 min.  
 Effective stream area after confluence =      290.599(Ac.)  
 Stream Area average Pervious fraction(Ap) =      0.315  
 Stream Area average soil loss rate(Fm) =      0.287(In/Hr)  
 Study area (this main stream) =      295.08(Ac.)

++++  
 Process from Point/Station      38.000 to Point/Station      39.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

-----  
 Upstream point/station elevation = 1035.000(Ft.)  
 Downstream point/station elevation = 1026.600(Ft.)  
 Pipe length = 990.00(Ft.)      Manning's N = 0.013  
 No. of pipes = 1      Required pipe flow = 518.256(CFS)

Given pipe size = 84.00(In.)  
 Calculated individual pipe flow = 518.256(CFS)  
 Normal flow depth in pipe = 61.22(In.)  
 Flow top width inside pipe = 74.69(In.)  
 Critical Depth = 71.20(In.)  
 Pipe flow velocity = 17.26(Ft/s)  
 Travel time through pipe = 0.96 min.  
 Time of concentration (TC) = 22.27 min.

++++++  
 Process from Point/Station 39.000 to Point/Station 39.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 290.599(Ac.)  
 Runoff from this stream = 518.256(CFS)  
 Time of concentration = 22.27 min.  
 Rainfall intensity = 1.989(In/Hr)  
 Area averaged loss rate (Fm) = 0.2866(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.3153

++++++  
 Process from Point/Station 817.000 to Point/Station 818.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 1000.000(Ft.)  
 Top (of initial area) elevation = 1049.000(Ft.)  
 Bottom (of initial area) elevation = 1044.000(Ft.)  
 Difference in elevation = 5.000(Ft.)  
 Slope = 0.00500 s(%) = 0.50  
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 17.789 min.  
 Rainfall intensity = 2.275(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.707  
 Subarea runoff = 8.039(CFS)  
 Total initial stream area = 5.000(Ac.)  
 Pervious area fraction = 0.500  
 Initial area Fm value = 0.489(In/Hr)

++++++  
 Process from Point/Station 818.000 to Point/Station 819.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1044.000(Ft.)  
 End of street segment elevation = 1042.300(Ft.)  
 Length of street segment = 330.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020

Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 12.059(CFS)  
 Depth of flow = 0.426(Ft.), Average velocity = 2.144(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 16.557(Ft.)  
 Flow velocity = 2.14(Ft/s)  
 Travel time = 2.57 min. TC = 20.35 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm) = 0.489(In/Hr)  
 Rainfall intensity = 2.099(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.690  
 Subarea runoff = 6.449(CFS) for 5.000(Ac.)  
 Total runoff = 14.488(CFS)  
 Effective area this stream = 10.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 340.42(Ac.)  
 Area averaged Fm value = 0.489(In/Hr)  
 Street flow at end of street = 14.488(CFS)  
 Half street flow at end of street = 7.244(CFS)  
 Depth of flow = 0.450(Ft.), Average velocity = 2.243(Ft/s)  
 Flow width (from curb towards crown) = 17.772(Ft.)

++++++  
 Process from Point/Station 819.000 to Point/Station 820.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1042.300(Ft.)  
 End of street segment elevation = 1039.000(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 21.732(CFS)  
 Depth of flow = 0.509(Ft.), Average velocity = 2.494(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Streetflow hydraulics at midpoint of street travel:

Halfstreet flow width = 20.000(Ft.)  
 Flow velocity = 2.49(Ft/s)  
 Travel time = 4.41 min. TC = 24.77 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)  
 Rainfall intensity = 1.866(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.664  
 Subarea runoff = 10.294(CFS) for 10.000(Ac.)  
 Total runoff = 24.782(CFS)  
 Effective area this stream = 20.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 350.42(Ac.)  
 Area averaged Fm value = 0.489(In/Hr)  
 Street flow at end of street = 24.782(CFS)  
 Half street flow at end of street = 12.391(CFS)  
 Depth of flow = 0.527(Ft.), Average velocity = 2.627(Ft/s)  
 Note: depth of flow exceeds top of street crown.  
 Flow width (from curb towards crown)= 20.000(Ft.)

++++++  
 Process from Point/Station 820.000 to Point/Station 821.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1039.000(Ft.)  
 End of street segment elevation = 1037.000(Ft.)  
 Length of street segment = 330.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 30.977(CFS)  
 Depth of flow = 0.701(Ft.), Average velocity = 3.332(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 1.74(Ft.)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 30.325(Ft.)  
 Flow velocity = 3.33(Ft/s)  
 Travel time = 1.65 min. TC = 26.42 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00

Pervious ratio(Ap) = 0.5000      Max loss rate(Fm)= 0.489(In/Hr)  
 Rainfall intensity = 1.795(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.655  
 Subarea runoff = 10.478(CFS) for 10.000(Ac.)  
 Total runoff = 35.260(CFS)  
 Effective area this stream = 30.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 360.42(Ac.)  
 Area averaged Fm value = 0.489(In/Hr)  
 Street flow at end of street = 35.260(CFS)  
 Half street flow at end of street = 35.260(CFS)  
 Depth of flow = 0.736(Ft.), Average velocity = 3.372(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 3.46(Ft.)  
 Flow width (from curb towards crown)= 32.042(Ft.)

++++++  
 Process from Point/Station 821.000 to Point/Station 821.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
 Stream flow area = 30.000(Ac.)  
 Runoff from this stream = 35.260(CFS)  
 Time of concentration = 26.42 min.  
 Rainfall intensity = 1.795(In/Hr)  
 Area averaged loss rate (Fm) = 0.4889(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.5000  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	518.256	22.27	1.989
2	35.260	26.42	1.795
Qmax(1) =			
	1.000 *	1.000 *	518.256) +
	1.148 *	0.843 *	35.260) + = 552.387
Qmax(2) =			
	0.886 *	1.000 *	518.256) +
	1.000 *	1.000 *	35.260) + = 494.489

Total of 2 streams to confluence:  
 Flow rates before confluence point:  
 518.256      35.260  
 Maximum flow rates at confluence using above data:  
 552.387      494.489  
 Area of streams before confluence:  
 290.599      30.000  
 Effective area values after confluence:  
 315.885      320.599  
 Results of confluence:  
 Total flow rate = 552.387(CFS)  
 Time of concentration = 22.266 min.  
 Effective stream area after confluence = 315.885(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.333  
 Stream Area average soil loss rate(Fm) = 0.306(In/Hr)  
 Study area (this main stream) = 320.60(Ac.)

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Process from Point/Station      39.000 to Point/Station      40.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****

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Upstream point/station elevation = 1026.600(Ft.)
Downstream point/station elevation = 1012.800(Ft.)
Pipe length = 1720.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 552.387(CFS)
Given pipe size = 84.00(In.)
Calculated individual pipe flow = 552.387(CFS)
Normal flow depth in pipe = 66.38(In.)
Flow top width inside pipe = 68.41(In.)
Critical Depth = 73.04(In.)
Pipe flow velocity = 16.94(Ft/s)
Travel time through pipe = 1.69 min.
Time of concentration (TC) = 23.96 min.

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Process from Point/Station      40.000 to Point/Station      40.000
**** CONFLUENCE OF MINOR STREAMS ****

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-----
Along Main Stream number: 1 in normal stream number 1
Stream flow area = 315.885(Ac.)
Runoff from this stream = 552.387(CFS)
Time of concentration = 23.96 min.
Rainfall intensity = 1.903(In/Hr)
Area averaged loss rate (Fm) = 0.3055(In/Hr)
Area averaged Pervious ratio (Ap) = 0.3326

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+++++
Process from Point/Station      822.000 to Point/Station      823.000
**** INITIAL AREA EVALUATION ****

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RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 32.00
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000(Ft.)
Top (of initial area) elevation = 1037.700(Ft.)
Bottom (of initial area) elevation = 1034.300(Ft.)
Difference in elevation = 3.400(Ft.)
Slope = 0.00340 s(%)= 0.34
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 19.216 min.
Rainfall intensity = 2.172(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.697
Subarea runoff = 7.576(CFS)
Total initial stream area = 5.000(Ac.)
Pervious area fraction = 0.500
Initial area Fm value = 0.489(In/Hr)

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+++++
Process from Point/Station      823.000 to Point/Station      824.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

```

Top of street segment elevation = 1034.300(Ft.)  
 End of street segment elevation = 1032.000(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 20.000(Ft.)  
 Distance from crown to crossfall grade break = 18.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [2] side(s) of the street  
 Distance from curb to property line = 10.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 11.364(CFS)  
 Depth of flow = 0.444(Ft.), Average velocity = 1.823(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 17.451(Ft.)  
 Flow velocity = 1.82(Ft/s)  
 Travel time = 6.03 min. TC = 25.25 min.  
 Adding area flow to street  
 RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)  
 Rainfall intensity = 1.844(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.661  
 Subarea runoff = 4.621(CFS) for 5.000(Ac.)  
 Total runoff = 12.198(CFS)  
 Effective area this stream = 10.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 370.42(Ac.)  
 Area averaged Fm value = 0.489(In/Hr)  
 Street flow at end of street = 12.198(CFS)  
 Half street flow at end of street = 6.099(CFS)  
 Depth of flow = 0.454(Ft.), Average velocity = 1.855(Ft/s)  
 Flow width (from curb towards crown)= 17.933(Ft.)

++++++  
 Process from Point/Station 824.000 to Point/Station 825.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

Top of street segment elevation = 1032.000(Ft.)  
 End of street segment elevation = 1027.000(Ft.)  
 Length of street segment = 660.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)

Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 18.296(CFS)  
 Depth of flow = 0.566(Ft.), Average velocity = 3.262(Ft/s)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 23.533(Ft.)  
 Flow velocity = 3.26(Ft/s)  
 Travel time = 3.37 min. TC = 28.62 min.  
 Adding area flow to street  
 CONDOMINIUM subarea type  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.342(In/Hr)  
 Rainfall intensity = 1.711(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method) (Q=KCIA) is C = 0.681  
 Subarea runoff = 11.112(CFS) for 10.000(Ac.)  
 Total runoff = 23.310(CFS)  
 Effective area this stream = 20.00(Ac.)  
 Total Study Area (Main Stream No. 1) = 380.42(Ac.)  
 Area averaged Fm value = 0.416(In/Hr)  
 Street flow at end of street = 23.310(CFS)  
 Half street flow at end of street = 23.310(CFS)  
 Depth of flow = 0.611(Ft.), Average velocity = 3.464(Ft/s)  
 Flow width (from curb towards crown)= 25.802(Ft.)

+++++  
 Process from Point/Station 825.000 to Point/Station 826.000  
 \*\*\*\* STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION \*\*\*\*

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Top of street segment elevation = 1027.000(Ft.)  
 End of street segment elevation = 1023.000(Ft.)  
 Length of street segment = 750.000(Ft.)  
 Height of curb above gutter flowline = 8.0(In.)  
 Width of half street (curb to crown) = 42.000(Ft.)  
 Distance from crown to crossfall grade break = 40.500(Ft.)  
 Slope from gutter to grade break (v/hz) = 0.020  
 Slope from grade break to crown (v/hz) = 0.020  
 Street flow is on [1] side(s) of the street  
 Distance from curb to property line = 13.000(Ft.)  
 Slope from curb to property line (v/hz) = 0.020  
 Gutter width = 1.500(Ft.)  
 Gutter hike from flowline = 1.500(In.)  
 Manning's N in gutter = 0.0150  
 Manning's N from gutter to grade break = 0.0150  
 Manning's N from grade break to crown = 0.0150  
 Estimated mean flow rate at midpoint of street = 26.806(CFS)  
 Depth of flow = 0.679(Ft.), Average velocity = 3.112(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property = 0.64(Ft.)  
 Streetflow hydraulics at midpoint of street travel:  
 Halfstreet flow width = 29.221(Ft.)  
 Flow velocity = 3.11(Ft/s)  
 Travel time = 4.02 min. TC = 32.64 min.  
 Adding area flow to street

## CONDOMINIUM subarea type

Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.3500      Max loss rate(Fm)=      0.342(In/Hr)  
 Rainfall intensity =      1.581(In/Hr) for a      25.0 year storm  
 Effective runoff coefficient used for area, (total area with modified  
 rational method)(Q=KCIA) is C = 0.673  
 Subarea runoff =      4.356(CFS) for      6.000(Ac.)  
 Total runoff =      27.666(CFS)  
 Effective area this stream =      26.00(Ac.)  
 Total Study Area (Main Stream No. 1) =      386.42(Ac.)  
 Area averaged Fm value =      0.399(In/Hr)  
 Street flow at end of street =      27.666(CFS)  
 Half street flow at end of street =      27.666(CFS)  
 Depth of flow =      0.688(Ft.), Average velocity =      3.116(Ft/s)  
 Warning: depth of flow exceeds top of curb  
 Distance that curb overflow reaches into property =      1.07(Ft.)  
 Flow width (from curb towards crown)=      29.657(Ft.)

++++++  
 Process from Point/Station      826.000 to Point/Station      826.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

 Along Main Stream number: 1 in normal stream number 2

Stream flow area =      26.000(Ac.)  
 Runoff from this stream =      27.666(CFS)  
 Time of concentration =      32.64 min.  
 Rainfall intensity =      1.581(In/Hr)  
 Area averaged loss rate (Fm) =      0.3986(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.4077  
 Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	552.387	23.96	1.903
2	27.666	32.64	1.581
Qmax(1) =	1.000 * 1.273 *	1.000 * 0.734 *	552.387) + 27.666) + =      578.231
Qmax(2) =	0.798 * 1.000 *	1.000 * 1.000 *	552.387) + 27.666) + =      468.647

## Total of 2 streams to confluence:

Flow rates before confluence point:

552.387      27.666

Maximum flow rates at confluence using above data:

578.231      468.647

Area of streams before confluence:

315.885      26.000

Effective area values after confluence:

334.971      341.885

## Results of confluence:

Total flow rate =      578.231(CFS)

Time of concentration =      23.959 min.

Effective stream area after confluence = 334.971(Ac.)  
 Stream Area average Pervious fraction(Ap) = 0.338  
 Stream Area average soil loss rate(Fm) = 0.313(In/Hr)  
 Study area (this main stream) = 341.88(Ac.)

++++  
 Process from Point/Station 40.000 to Point/Station 94.000  
 \*\*\*\* PIPEFLOW TRAVEL TIME (User specified size) \*\*\*\*

---

Upstream point/station elevation = 1011.300(Ft.)  
 Downstream point/station elevation = 1004.000(Ft.)  
 Pipe length = 900.00(Ft.) Manning's N = 0.013  
 No. of pipes = 1 Required pipe flow = 578.231(CFS)  
 Given pipe size = 102.00(In.)  
 Calculated individual pipe flow = 578.231(CFS)  
 Normal flow depth in pipe = 56.91(In.)  
 Flow top width inside pipe = 101.31(In.)  
 Critical Depth = 72.44(In.)  
 Pipe flow velocity = 17.78(Ft/s)  
 Travel time through pipe = 0.84 min.  
 Time of concentration (TC) = 24.80 min.

++++  
 Process from Point/Station 94.000 to Point/Station 94.000  
 \*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

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Along Main Stream number: 1 in normal stream number 1  
 Stream flow area = 334.971(Ac.)  
 Runoff from this stream = 578.231(CFS)  
 Time of concentration = 24.80 min.  
 Rainfall intensity = 1.864(In/Hr)  
 Area averaged loss rate (Fm) = 0.3126(In/Hr)  
 Area averaged Pervious ratio (Ap) = 0.3383

++++  
 Process from Point/Station 827.000 to Point/Station 828.000  
 \*\*\*\* INITIAL AREA EVALUATION \*\*\*\*

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RESIDENTIAL(5 - 7 dwl/acre)  
 Decimal fraction soil group A = 1.000  
 Decimal fraction soil group B = 0.000  
 Decimal fraction soil group C = 0.000  
 Decimal fraction soil group D = 0.000  
 SCS curve number for soil(AMC 2) = 32.00  
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.489(In/Hr)  
 Initial subarea data:  
 Initial area flow distance = 900.000(Ft.)  
 Top (of initial area) elevation = 1023.000(Ft.)  
 Bottom (of initial area) elevation = 1014.000(Ft.)  
 Difference in elevation = 9.000(Ft.)  
 Slope = 0.01000 s(%)= 1.00  
 $TC = k(0.389) * [(length^3)/(elevation\ change)]^{0.2}$   
 Initial area time of concentration = 14.847 min.  
 Rainfall intensity = 2.536(In/Hr) for a 25.0 year storm  
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.726  
 Subarea runoff = 11.055(CFS)  
 Total initial stream area = 6.000(Ac.)  
 Pervious area fraction = 0.500

Initial area Fm value = 0.489(In/Hr)

Process from Point/Station 828.000 to Point/Station 828.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

Along Main Stream number: 1 in normal stream number 2  
Stream flow area = 6.000(Ac.)  
Runoff from this stream = 11.055(CFS)  
Time of concentration = 14.85 min.  
Rainfall intensity = 2.536(In/Hr)  
Area averaged loss rate (Fm) = 0.4889(In/Hr)  
Area averaged Pervious ratio (Ap) = 0.5000  
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	578.231	24.80	1.864
2	11.055	14.85	2.536
Qmax(1) =			
	1.000 *	1.000 *	578.231) +
	0.672 *	1.000 *	11.055) + = 585.656
Qmax(2) =			
	1.433 *	0.599 *	578.231) +
	1.000 *	1.000 *	11.055) + = 507.139

Total of 2 streams to confluence:  
Flow rates before confluence point:  
578.231 11.055  
Maximum flow rates at confluence using above data:  
585.656 507.139  
Area of streams before confluence:  
334.971 6.000  
Effective area values after confluence:  
340.971 206.522  
Results of confluence:  
Total flow rate = 585.656(CFS)  
Time of concentration = 24.802 min.  
Effective stream area after confluence = 340.971(Ac.)  
Stream Area average Pervious fraction(Ap) = 0.341  
Stream Area average soil loss rate(Fm) = 0.316(In/Hr)  
Study area (this main stream) = 340.97(Ac.)  
End of computations, Total Study Area = 392.42 (Ac.)  
The following figures may be used for a unit hydrograph study of the same area.  
Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.343  
Area averaged SCS curve number = 36.8

DECLEREZ CHL.

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2001 Version 6.4  
Rational Hydrology Study Date: 01/13/05

-----  
FONTANA / DECLEZ CHANNEL HYDROLOGY  
25 YEAR STORM  
JN 04339  
-----

Hall & Forman, Inc. - S/N 950  
-----

\*\*\*\*\* Hydrology Study Control Information \*\*\*\*\*  
-----

Rational hydrology study storm event year is 25.0  
10 Year storm 1 hour rainfall = 0.930(In.)  
100 Year storm 1 hour rainfall = 1.350(In.)  
Computed rainfall intensity:  
Storm year = 25.00 1 hour rainfall = 1.097 (In.)  
Slope used for rainfall intensity curve b = 0.6000  
Soil antecedent moisture condition (AMC) = 2

+++++  
Process from Point/Station 93.000 to Point/Station 93.000  
\*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*  
-----

Soil classification AP and SCS values input by user  
USER INPUT of soil data for subarea  
SCS curve number for soil(AMC 2) = 67.05  
Pervious ratio(Ap) = 0.5160 Max loss rate(Fm)= 0.298(In/Hr)  
Rainfall intensity = 2.394(In/Hr) for a 25.0 year storm  
User specified values are as follows:  
TC = 16.34 min. Rain intensity = 2.39(In/Hr)  
Total area this stream = 816.23(Ac.)  
Total Study Area (Main Stream No. 1) = 816.23(Ac.)  
Total runoff = 2004.30(CFS)

+++++  
Process from Point/Station 93.000 to Point/Station 94.000  
\*\*\*\* IMPROVED CHANNEL TRAVEL TIME \*\*\*\*  
-----

Upstream point elevation = 1005.500(Ft.)  
Downstream point elevation = 1004.000(Ft.)  
Channel length thru subarea = 500.000(Ft.)  
Channel base width = 24.000(Ft.)  
Slope or 'Z' of left channel bank = 0.000  
Slope or 'Z' of right channel bank = 0.000  
Manning's 'N' = 0.015  
Maximum depth of channel = 9.000(Ft.)  
Flow(q) thru subarea = 2004.300(CFS)  
Depth of flow = 6.075(Ft.), Average velocity = 13.748(Ft/s)  
Channel flow top width = 24.000(Ft.)  
Flow Velocity = 13.75(Ft/s)  
Travel time = 0.61 min.  
Time of concentration = 16.95 min.

Critical depth = 6.000(Ft.)

+++++  
Process from Point/Station 94.000 to Point/Station 94.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 1  
Stream flow area = 816.230(Ac.)  
Runoff from this stream = 2004.300(CFS)  
Time of concentration = 16.95 min.  
Rainfall intensity = 2.343(In/Hr)  
Area averaged loss rate (Fm) = 0.2980(In/Hr)  
Area averaged Pervious ratio (Ap) = 0.5160

+++++  
Process from Point/Station 94.000 to Point/Station 94.000  
\*\*\*\* USER DEFINED FLOW INFORMATION AT A POINT \*\*\*\*

---

Soil classification AP and SCS values input by user  
USER INPUT of soil data for subarea  
SCS curve number for soil(AMC 2) = 38.89  
Pervious ratio(Ap) = 0.3410 Max loss rate(Fm)= 0.316(In/Hr)  
Rainfall intensity = 1.864(In/Hr) for a 25.0 year storm  
User specified values are as follows:  
TC = 24.80 min. Rain intensity = 1.86(In/Hr)  
Total area this stream = 340.97(Ac.)  
Total Study Area (Main Stream No. 1) = 1157.20(Ac.)  
Total runoff = 585.66(CFS)

+++++  
Process from Point/Station 94.000 to Point/Station 94.000  
\*\*\*\* CONFLUENCE OF MINOR STREAMS \*\*\*\*

---

Along Main Stream number: 1 in normal stream number 2  
Stream flow area = 340.970(Ac.)  
Runoff from this stream = 585.660(CFS)  
Time of concentration = 24.80 min.  
Rainfall intensity = 1.864(In/Hr)  
Area averaged loss rate (Fm) = 0.3160(In/Hr)  
Area averaged Pervious ratio (Ap) = 0.3410  
Summary of stream data:

Stream No.	Flow rate (CFS)	TC (min)	Rainfall Intensity (In/Hr)
1	2004.300	16.95	2.343
2	585.660	24.80	1.864
Qmax(1) =			
	1.000 *	1.000 *	2004.300) +
	1.309 *	0.683 *	585.660) + = 2528.181
Qmax(2) =			
	0.766 *	1.000 *	2004.300) +
	1.000 *	1.000 *	585.660) + = 2120.895

Total of 2 streams to confluence:  
Flow rates before confluence point:  
2004.300 585.660

Maximum flow rates at confluence using above data:

2528.181      2120.895

Area of streams before confluence:

816.230      340.970

Effective area values after confluence:

1049.219      1157.200

Results of confluence:

Total flow rate = 2528.181(CFS)

Time of concentration = 16.946 min.

Effective stream area after confluence = 1049.219(Ac.)

Stream Area average Pervious fraction( $A_p$ ) = 0.464

Stream Area average soil loss rate( $F_m$ ) = 0.303(In/Hr)

Study area (this main stream) = 1157.20(Ac.)

End of computations, Total Study Area = 1157.20 (Ac.)

The following figures may

be used for a unit hydrograph study of the same area.

Note: These figures do not consider reduced effective area effects caused by confluences in the rational equation.

Area averaged pervious area fraction( $A_p$ ) = 0.464

Area averaged SCS curve number = 58.8

HALL & FOREMAN, INC.  
420 Exchange, Suite 100  
Riverside, CA 92502-1501  
760-514-4500  
760-514-1501

FONTANA

JOB No. 04339  
BY HERMAN  
DATE  
SHT. 1649  
OF

◆ LAND PLANNING ◆ CIVIL ENGINEERING ◆ SURVEYING

# HYDRAULICS

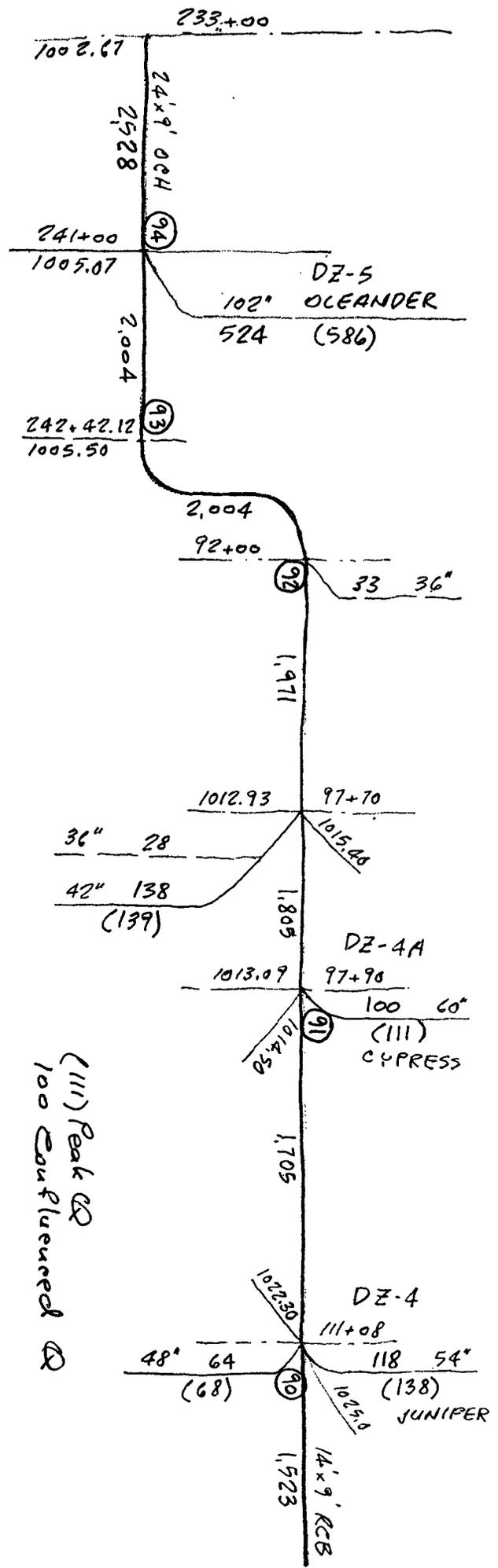
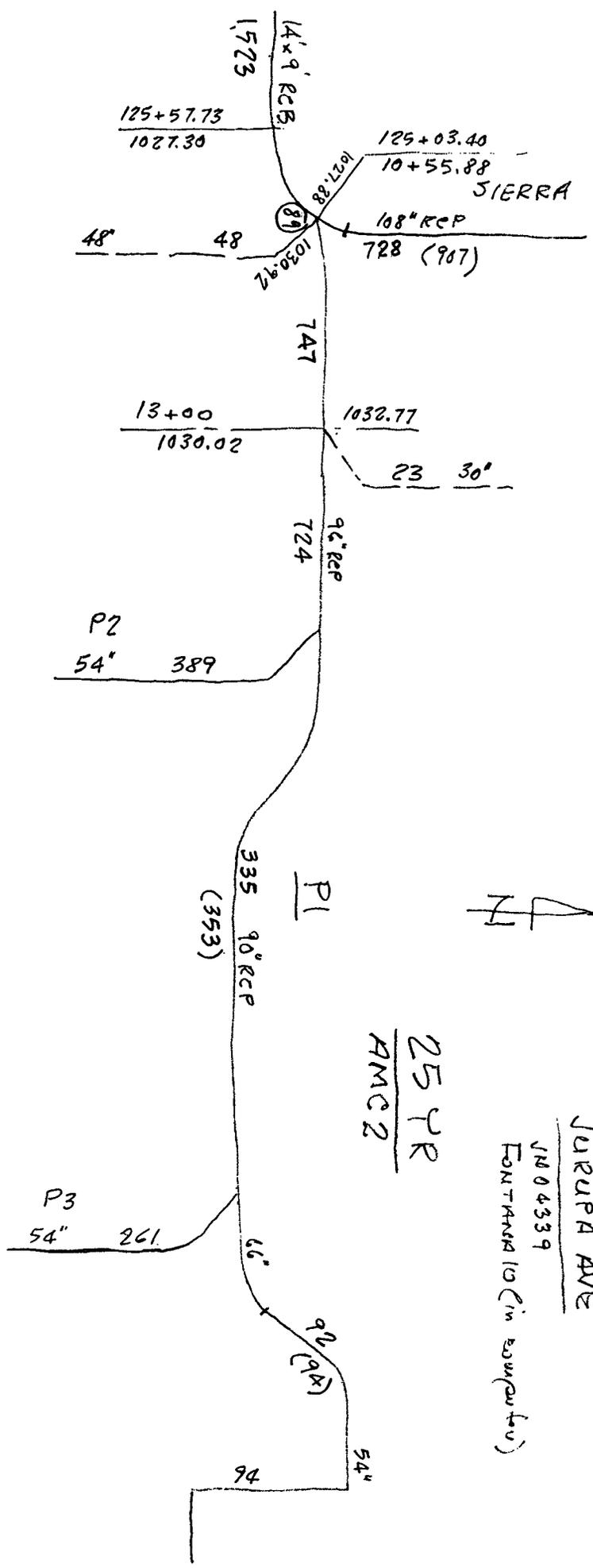


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JOB No. \_\_\_\_\_  
BY \_\_\_\_\_  
DATE \_\_\_\_\_  
SHT. 1650  
OF \_\_\_\_\_

◆ LAND PLANNING ◆ CIVIL ENGINEERING ◆ SURVEYING

# 25 YEAR



JURUPA AVE  
 JN 04339  
 FONTANA 10 (in easement)  
 25 PR  
 AMC 2

(111) Peak Q  
 100' easement Q

T1	FONTANA / DECLEZ CHANNEL W/O DETENTION (AMC2)										0	
0												
T2	25 YEAR STORM											
T3	JN 04339											
SO	23300.000	1002.670	1								1002.670	
R	24100.000	1005.070	1			.014					.000	
	.000 0											
JX	24100.010	1005.070	1	2			.014	524.000			1005.070	.0
	.000											
R	24242.120	1005.500	1			.014					.000	
WX	24242.120	1005.500	3									.000
R	24242.130	1005.500	3			.013					.000	
	.000 0											
SH	24242.130	1005.500	3								1005.500	
CD	1	2	0	.000	11.000	24.000	.000	.000				.00
CD	2	4	1	.000	9.000	.000	.000	.000				.00
CD	3	3	0	.000	9.000	14.000	.000	.000				.00
Q			2004.000			.0						



```

*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height/ | Base Wt | | No Wth
      | Elev  | (FT)  | Elev  | (CFS) | (FPS) | Head | Grd.El. | Elev  | Depth  | Width  | Dia.-FT | or I.D. | ZL | Prs/Pip
L/Elem | Ch Slope | | | | | | | | | | | | | | |
*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****
23300.000 | 1002.670 | 6.806 | 1009.476 | 2528.00 | 15.48 | 3.72 | 1013.20 | .00 | 7.01 | 24.00 | 11.000 | 24.000 | .00 | 0 .0
      | 722.635 | .0030 | | | | | | | | | | | | | | |
24022.630 | 1004.838 | 6.806 | 1011.644 | 2528.00 | 15.48 | 3.72 | 1015.36 | .00 | 7.01 | 24.00 | 11.000 | 24.000 | .00 | 0 .0
      | 77.365 | .0030 | | | | | | | | | | | | | | |
24100.000 | 1005.070 | 7.010 | 1012.080 | 2528.00 | 15.03 | 3.51 | 1015.59 | .00 | 7.01 | 24.00 | 11.000 | 24.000 | .00 | 0 .0
JUNCT STR | .0000 | | | | | | | | | | | | | | |
24100.010 | 1005.070 | 9.499 | 1014.569 | 2004.00 | 8.79 | 1.20 | 1015.77 | .00 | 6.01 | 24.00 | 11.000 | 24.000 | .00 | 0 .0
      | 142.109 | .0030 | | | | | | | | | | | | | | |
24242.120 | 1005.500 | 9.064 | 1014.564 | 2004.00 | 9.21 | 1.32 | 1015.88 | .00 | 6.01 | 24.00 | 11.000 | 24.000 | .00 | 0 .0
WALL EXIT | | | | | | | | | | | | | | |
24242.120 | 1005.500 | 9.064 | 1014.564 | 2004.00 | 15.90 | 3.93 | 1018.49 | .00 | 8.60 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | .012 | .0000 | | | | | | | | | | | | | | |
24242.130 | 1005.500 | 9.064 | 1014.564 | 2004.00 | 15.90 | 3.93 | 1018.49 | .00 | 8.60 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | | |
    
```

1654

T1 FONTANA / JURUPA AVE. 14'x 9' RCB W/O DETENTION (AMC2)									
T2 25 YEAR STORM									
T3 JN 04339									
SO	7990.5001005.500	1					1016.140		
R	8003.0701005.530	1		.013				.000	
	.000 0								
R	8143.7401005.810	1		.013				-89.554	
	.000 0								
R	8600.0001006.720	1		.013				.000	
	.000 0								
R	9200.0001009.720	1		.013				.000	
	.000 0								
JX	9200.0101009.720	1	2	.013	33.000		1013.220	-45.0	
	.000								
R	9680.0001012.120	1		.013				.000	
	.000 0								
R	9770.0001012.930	1		.013				.000	
	.000 0								
JX	9770.0101012.930	1	2	.013	28.000		1015.400	45.0	
	.000								
R	9770.0201012.930	1		.013				.000	
	.000 0								
JX	9770.0301012.930	1	3	.013	138.000		1015.400	45.0	
	.000								
R	9790.0001013.090	1		.013				.000	
	.000 0								
JX	9790.0101013.090	1	4	.013	100.000		1014.500	-45.0	
	.000								
R	10700.0001019.670	1		.013				.000	
	.000 0								
R	11000.0001021.870	1		.013				.000	
	.000 0								
R	11108.0001022.300	1		.013				.000	
	.000 0								
JX	11108.0101022.300	1	5	6.013	64.000	118.000	1025.000	1025.000	45.0-45.0
	.000								
R	12357.7301027.300	1		.013				.000	
	.000 0								
R	12503.4001027.860	1		.013				-39.369	
	.000 0								
JX	12503.4101028.860	8	7	1.013	48.000	728.000	1029.920	1027.860	45.0 .0
	.000								
R	12528.3001028.900	8		.013				30.000	
	.000 0								
SH	12528.3001028.900	8					1028.900		
CD	1 3 0	.000	9.000	14.000	.000	.000	.000	.00	
CD	2 4 1	.000	3.000	.000	.000	.000	.000	.00	
CD	3 4 1	.000	3.500	.000	.000	.000	.000	.00	
CD	4 4 1	.000	5.000	.000	.000	.000	.000	.00	
CD	5 4 1	.000	4.000	.000	.000	.000	.000	.00	
CD	6 4 1	.000	4.500	.000	.000	.000	.000	.00	
CD	7 4 1	.000	4.000	.000	.000	.000	.000	.00	
CD	8 4 1	.000	8.000	.000	.000	.000	.000	.00	
Q		747.000	.0						

WATER SURFACE PROFILE - CHANNEL DEFINITION LISTING

CARD CODE	SECT NO	CHN TYPE	NO OF PIER/PIP	AVE WIDTH	PIER WIDTH	HEIGHT 1	BASE DIAMETER	ZL WIDTH	ZR WIDTH	INV DROP	Y(1)	Y(2)	Y(3)	Y(4)	Y(5)	Y(6)	Y(7)	Y(8)	Y(9)	Y(10)
CD	1	3	0	.000		9.000	14.000	.000	.000	.00										
CD	2	4	1			3.000														
CD	3	4	1			3.500														
CD	4	4	1			5.000														
CD	5	4	1			4.000														
CD	6	4	1			4.500														
CD	7	4	1			4.000														
CD	8	4	1			8.000														

W S P G W

WATER SURFACE PROFILE - TITLE CARD LISTING

HEADING LINE NO 1 IS -  
 HEADING LINE NO 2 IS -  
 HEADING LINE NO 3 IS -

FONTANA / JURUPA AVE. 14'x 9' RCB W/O DETENTION (AMC2)  
 100 YEAR STORM  
 JN 04339

W S P G W

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	IS A	SYSTEM OUTLET	U/S DATA	STATION	INVERT	SECT	W S ELEV	RADIUS	ANGLE	ANG PT	MAN H		
ELEMENT NO 1	IS A	SYSTEM OUTLET	U/S DATA	7990.500	1005.500	1	1016.140						
ELEMENT NO 2	IS A	REACH	U/S DATA	8003.070	1005.530	1	.013	.000	.000	.000	0		
ELEMENT NO 3	IS A	REACH	U/S DATA	8143.740	1005.810	1	.013	90.000	-89.554	.000	0		
ELEMENT NO 4	IS A	REACH	U/S DATA	8600.000	1006.720	1	.013	.000	.000	.000	0		
ELEMENT NO 5	IS A	REACH	U/S DATA	9200.000	1009.720	1	.013	.000	.000	.000	0		
ELEMENT NO 6	IS A	JUNCTION	U/S DATA	9200.010	1009.720	1	.013	33.000	.000	1013.220	.000	-45.000	.000
THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING													
ELEMENT NO 7	IS A	REACH	U/S DATA	9680.000	1012.120	1	.013	.000	.000	.000	0		
ELEMENT NO 8	IS A	REACH	U/S DATA	9770.000	1012.930	1	.013	.000	.000	.000	0		
ELEMENT NO 9	IS A	JUNCTION	U/S DATA	9770.010	1012.930	1	.013	28.000	.000	1015.400	.000	45.000	.000

129

THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING  
 THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING

RADIUS .000  
 ANGLE .000

W S P G W

PAGE NO 3

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO 10 IS A REACH \* \* \*  
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H  
 9770.020 1012.930 1 .013 .000 .000 .000 0

ELEMENT NO 11 IS A JUNCTION \* \* \*  
 U/S DATA STATION INVERT SECT LAT-1 LAT-2 N Q3 Q4 INVERT-3 INVERT-4 PHI 3 PHI 4  
 9770.030 1012.930 1 3 0 .013 138.000 .000 1015.400 .000 45.000 .000  
 RADIUS ANGLE  
 .000 .000

THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING  
 THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING

ELEMENT NO 12 IS A REACH \* \* \*  
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H  
 9790.000 1013.090 1 .013 .000 .000 .000 0

ELEMENT NO 13 IS A JUNCTION \* \* \*  
 U/S DATA STATION INVERT SECT LAT-1 LAT-2 N Q3 Q4 INVERT-3 INVERT-4 PHI 3 PHI 4  
 9790.010 1013.090 1 4 0 .013 100.000 .000 1014.500 .000 -45.000 .000  
 RADIUS ANGLE  
 .000 .000

THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING  
 THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING

ELEMENT NO 14 IS A REACH \* \* \*  
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H  
 10700.000 1019.670 1 .013 .000 .000 .000 0

ELEMENT NO 15 IS A REACH \* \* \*  
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H  
 11000.000 1021.870 1 .013 .000 .000 .000 0

ELEMENT NO 16 IS A REACH \* \* \*  
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H  
 11108.000 1022.300 1 .013 .000 .000 .000 0

ELEMENT NO 17 IS A JUNCTION \* \* \*  
 U/S DATA STATION INVERT SECT LAT-1 LAT-2 N Q3 Q4 INVERT-3 INVERT-4 PHI 3 PHI 4  
 11108.010 1022.300 1 5 6 .013 64.000 118.000 1025.000 1025.000 45.000 -45.000  
 RADIUS ANGLE  
 .000 .000

THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING  
 THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING

W S P G W

PAGE NO 4

WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO 18 IS A REACH \* \* \*  
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H  
 12357.730 1027.300 1 .013 .000 .000 .000 0

ELEMENT NO 19 IS A REACH \* \* \*  
 U/S DATA STATION INVERT SECT N RADIUS ANGLE ANG PT MAN H  
 12503.400 1027.860 1 .013 212.001 -39.369 .000 0

ELEMENT NO 20 IS A JUNCTION \* \* \*  
 U/S DATA STATION INVERT SECT LAT-1 LAT-2 N Q3 Q4 INVERT-3 INVERT-4 PHI 3 PHI 4  
 12503.410 1028.860 8 7 1 .013 48.000 728.000 1029.920 1027.860 45.000 .000  
 RADIUS ANGLE

ELEMENT NO	21 IS A REACH	*	*	*
	U/S DATA	STATION	INVERT	SECT
		12528.300	1028.900	8
ELEMENT NO	22 IS A SYSTEM HEADWORKS	*	*	*
	U/S DATA	STATION	INVERT	SECT
		12528.300	1028.900	8

N  
.013

\*

	.000	.000		
	RADIUS	ANGLE	ANG PT	MAN H
	47.536	30.000	.000	0
	W S ELEV			
	1028.900			

Program Package Serial Number: 1432

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 4: 2:35

FONTANA / JURUPA AVE. 14'x 9' RCB W/O DETENTION (AMC2)

100 YEAR STORM

JN 04339

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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height/ | Base Wt |
| Elev | (FT) | Elev | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. |
L/Elem | Ch Slope | | | | | SF Ave | HF | SE Dpth | Froude N | Norm Dp | "N" | X-Fall |
*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****
7990.500 | 1005.500 | 10.640 | 1016.140 | 2004.00 | 15.90 | 3.93 | 1020.07 | .00 | 8.60 | 14.00 | 9.000 | 14.000 | .00 | 0 | .0
| | | | | | | | | | | | | | | | |
12.570 | .0024 | | | | | | | | | | | | | | | |
8003.070 | 1005.530 | 10.673 | 1016.203 | 2004.00 | 15.90 | 3.93 | 1020.13 | .00 | 8.60 | 14.00 | 9.000 | 14.000 | .00 | 0 | .0
| | | | | | | | | | | | | | | | |
140.670 | .0020 | | | | | | | | | | | | | | | |
8143.740 | 1005.810 | 11.888 | 1017.698 | 2004.00 | 15.90 | 3.93 | 1021.63 | .00 | 8.60 | 14.00 | 9.000 | 14.000 | .00 | 0 | .0
| | | | | | | | | | | | | | | | |
456.260 | .0020 | | | | | | | | | | | | | | | |
8600.000 | 1006.720 | 13.283 | 1020.003 | 2004.00 | 15.90 | 3.93 | 1023.93 | .00 | 8.60 | 14.00 | 9.000 | 14.000 | .00 | 0 | .0
| | | | | | | | | | | | | | | | |
600.000 | .0050 | | | | | | | | | | | | | | | |
9200.000 | 1009.720 | 13.313 | 1023.033 | 2004.00 | 15.90 | 3.93 | 1026.96 | .00 | 8.60 | 14.00 | 9.000 | 14.000 | .00 | 0 | .0
| | | | | | | | | | | | | | | | |
JUNCT STR | .0000 | | | | | | | | | | | | | | | |
9200.010 | 1009.720 | 13.543 | 1023.263 | 1971.00 | 15.64 | 3.80 | 1027.06 | .00 | 8.51 | 14.00 | 9.000 | 14.000 | .00 | 0 | .0
| | | | | | | | | | | | | | | | |
479.990 | .0050 | | | | | | | | | | | | | | | |
9680.000 | 1012.120 | 13.489 | 1025.609 | 1971.00 | 15.64 | 3.80 | 1029.41 | .00 | 8.51 | 14.00 | 9.000 | 14.000 | .00 | 0 | .0
| | | | | | | | | | | | | | | | |
90.000 | .0090 | | | | | | | | | | | | | | | |
9770.000 | 1012.930 | 13.119 | 1026.049 | 1971.00 | 15.64 | 3.80 | 1029.85 | .00 | 8.51 | 14.00 | 9.000 | 14.000 | .00 | 0 | .0
| | | | | | | | | | | | | | | | |
JUNCT STR | .0000 | | | | | | | | | | | | | | | |
9770.020 | 1012.930 | 13.314 | 1026.244 | 1943.00 | 15.42 | 3.69 | 1029.94 | .00 | 8.43 | 14.00 | 9.000 | 14.000 | .00 | 0 | .0
| | | | | | | | | | | | | | | | |
JUNCT STR | .0000 | | | | | | | | | | | | | | | |
    
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Program Package Serial Number: 1432

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 4: 2:35

FONTANA / JURUPA AVE. 14'x 9' RCB W/O DETENTION (AMC2)  
 100 YEAR STORM  
 JN 04339

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt/or I.D.	ZL	No Prs/Pip	Wth
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type	Ch
9770.030	1012.930	13.981	1026.911	1805.00	14.33	3.19	1030.10	.00	8.02	14.00	9.000	14.000	.00	0	.0
19.970	.0080					.0041	.08	13.98	.84	5.83	.013	.00	.00	BOX	
9790.000	1013.090	13.902	1026.992	1805.00	14.33	3.19	1030.18	.00	8.02	14.00	9.000	14.000	.00	0	.0
JUNCT STR	.0000					.0037	.00	13.90	.84		.013	.00	.00	BOX	
9790.010	1013.090	14.500	1027.590	1705.00	13.53	2.84	1030.43	.00	7.72	14.00	9.000	14.000	.00	0	.0
909.990	.0072					.0037	3.33	14.50	.79	5.80	.013	.00	.00	BOX	
10700.000	1019.670	11.248	1030.918	1705.00	13.53	2.84	1033.76	.00	7.72	14.00	9.000	14.000	.00	0	.0
300.000	.0073					.0037	1.10	11.25	.79	5.77	.013	.00	.00	BOX	
11000.000	1021.870	10.145	1032.015	1705.00	13.53	2.84	1034.86	.00	7.72	14.00	9.000	14.000	.00	0	.0
108.000	.0040					.0037	.39	10.14	.79	7.24	.013	.00	.00	BOX	
11108.000	1022.300	10.109	1032.409	1705.00	13.53	2.84	1035.25	.00	7.72	14.00	9.000	14.000	.00	0	.0
JUNCT STR	.0000					.0029	.00	10.11	.79		.013	.00	.00	BOX	
11108.010	1022.300	11.049	1033.349	1523.00	12.09	2.27	1035.62	.00	7.16	14.00	9.000	14.000	.00	0	.0
1249.721	.0040					.0029	3.65	11.05	.71	6.64	.013	.00	.00	BOX	
12357.730	1027.300	9.695	1036.995	1523.00	12.09	2.27	1039.26	.00	7.16	14.00	9.000	14.000	.00	0	.0
145.670	.0038					.0029	.43	.00	.71	6.74	.013	.00	.00	BOX	
12503.400	1027.860	9.861	1037.721	1523.00	12.09	2.27	1039.99	.00	7.16	14.00	9.000	14.000	.00	0	.0
JUNCT STR	*****					.0048	.00	.00	.71		.013	.00	.00	BOX	

----- WARNING - Junction Analysis - Change in Channel Type -----

02/

Program Package Serial Number: 1432

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 4: 2:35

FONTANA / JURUPA AVE. 14'x 9' RCB W/O DETENTION (AMC2)

100 YEAR STORM

JN 04339

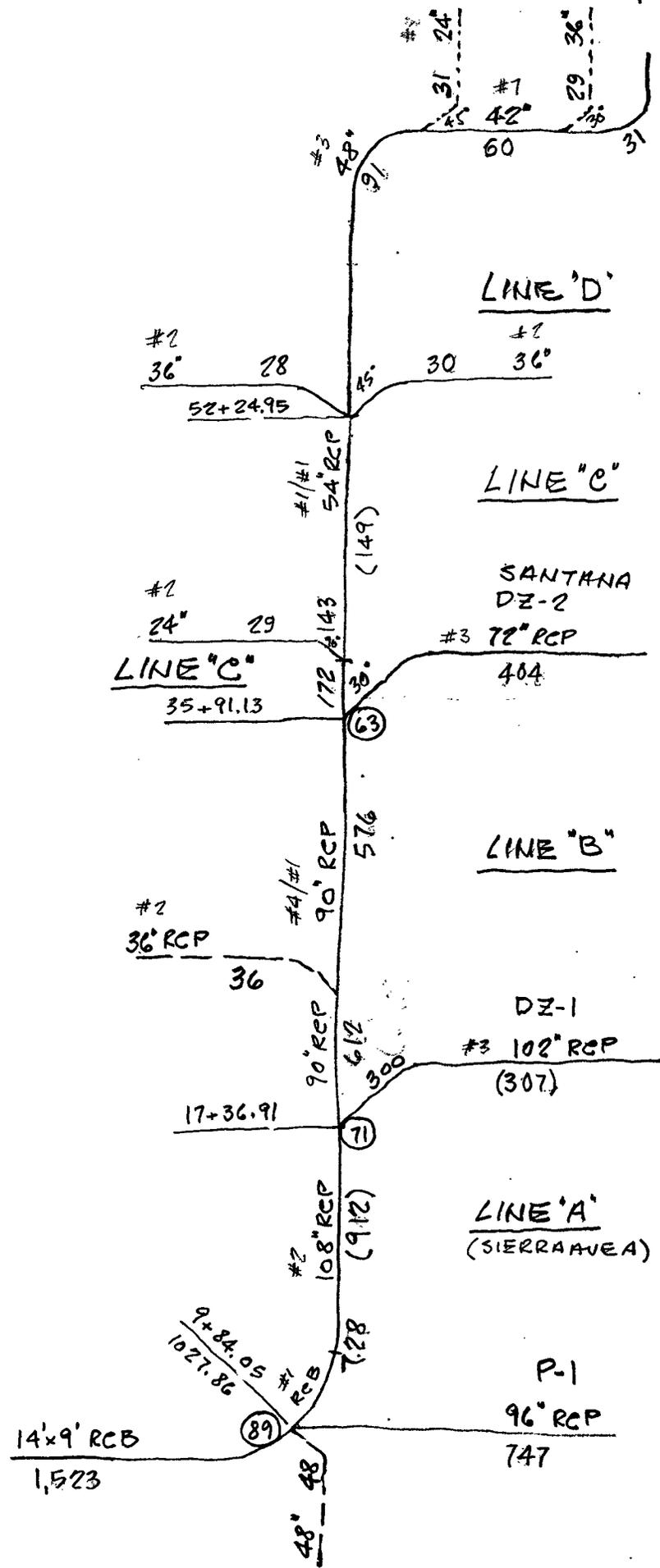
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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height/ | Base Wt | | No Wth
      | Elev  | (FT)  | Elev  | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip
L/Elem | Ch Slope | | | | | SF Ave | HF | SE Dpth | Froude N | Norm Dp | "N" | X-Fall | ZR | Type Ch
*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****
12503.410 | 1028.860 | 9.908 | 1038.768 | 747.00 | 14.86 | 3.43 | 1042.20 | .00 | 6.87 | .00 | 8.000 | .000 | .00 | 1 | .0
      | 24.890 | .0016 | | | | | .0067 | .17 | .00 | .00 | 8.00 | .013 | .00 | .00 | PIPE
12528.300 | 1028.900 | 10.431 | 1039.331 | 747.00 | 14.86 | 3.43 | 1042.76 | .00 | 6.87 | .00 | 8.000 | .000 | .00 | 1 | .0
      | | | | | | | | | | | | | | | |
    
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SIERRA AVE. W/O DETENTION  
 FONTANA 7 (in computer)

JN04339  
 1662

25 YR.



↑  
 N  
 (307) Peak Q  
 300 Confluent Q

T1 FONTANA / SIERRA AVE. LINE"A"

0

T2 25 YEAR STORM

T3 JN 04339

SO	984.0501027.860	1						1038.770	
R	1055.5801028.170	1		.013					-19.332
	.000	0							
TS	1085.5801028.290	2		.014					-8.108
R	1735.6001030.240	2		.013					.000
	.000	0							
JX	1757.8401031.790	4	3	.014	300.000			1030.640	30.0
	.000								
R	1757.8501031.790	4		.013					.000
	.000	0							
SH	1757.8501031.790	4						1031.790	
CD	1	3	0	.000	9.000	14.000	.000	.000	.00
CD	2	4	1	.000	9.000	.000	.000	.000	.00
CD	3	4	1	.000	8.500	.000	.000	.000	.00
CD	4	4	1	.000	7.500	.000	.000	.000	.00
Q				612.000	.0				

WATER SURFACE PROFILE - CHANNEL DEFINITION LISTING

CARD CODE	SECT NO	CHN TYPE	NO OF PIER/PIP	AVE WIDTH	PIER WIDTH	HEIGHT 1 DIAMETER	BASE WIDTH	ZL	ZR	INV DROP	Y(1)	Y(2)	Y(3)	Y(4)	Y(5)	Y(6)	Y(7)	Y(8)	Y(9)	Y(10)
CD	1	3	0	.000		9.000	14.000	.000	.000	.00										
CD	2	4	1			9.000														
CD	3	4	1			8.500														
CD	4	4	1			7.500														

W S P G W  
WATER SURFACE PROFILE - TITLE CARD LISTING

HEADING LINE NO 1 IS - FONTANA / SIERRA AVE. LINE"A"  
 HEADING LINE NO 2 IS - 25 YEAR STORM  
 HEADING LINE NO 3 IS - JN 04339

W S P G W  
WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	DESCRIPTION	STATION	INVERT	SECT	W S ELEV	RADIUS	ANGLE	ANG PT	MAN H
1	IS A SYSTEM OUTLET	984.050	1027.860	1	1038.770				
2	IS A REACH	1055.580	1028.170	1		211.999	-19.332	.000	0
3	IS A TRANSITION	1085.580	1028.290	2		211.997	-8.108		
4	IS A REACH	1735.600	1030.240	2		.000	.000	.000	0
5	IS A JUNCTION	1757.840	1031.790	4					
6	IS A REACH	1757.850	1031.790	4		.000	.000	.000	0
7	IS A SYSTEM HEADWORKS	1757.850	1031.790	4					

FONTANA / SIERRA AVE. LINE"A"

25 YEAR STORM

JN 04339

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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height/ | Base Wt | | No Wth
      | Elev   | (FT)  | Elev   | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip
L/Elem | Ch Slope | | | | | SF Ave | HF | SE Dpth | Froude N | Norm Dp | "N" | X-Fall | ZR | Type Ch
*****
984.050 | 1027.860 | 10.910 | 1038.770 | 912.00 | 7.24 | .81 | 1039.58 | .00 | 5.09 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | | | |
71.530 | .0043 | | | | | | | | | | | | | | | |
1055.580 | 1028.170 | 10.750 | 1038.920 | 912.00 | 7.24 | .81 | 1039.73 | .00 | 5.09 | 14.00 | 9.000 | 14.000 | .00 | 0 .0
      | | | | | | | | | | | | | | | |
TRANS STR | .0040 | | | | | | | | | | | | | | | |
1085.580 | 1028.290 | 8.801 | 1037.091 | 912.00 | 14.42 | 3.23 | 1040.32 | .00 | 7.42 | 2.65 | 9.000 | .000 | .00 | 1 .0
      | | | | | | | | | | | | | | | |
83.053 | .0030 | | | | | | | | | | | | | | | |
1168.633 | 1028.539 | 9.000 | 1037.539 | 912.00 | 14.34 | 3.19 | 1040.73 | .00 | 7.42 | .00 | 9.000 | .000 | .00 | 1 .0
      | | | | | | | | | | | | | | | |
566.967 | .0030 | | | | | | | | | | | | | | | |
1735.600 | 1030.240 | 10.324 | 1040.564 | 912.00 | 14.34 | 3.19 | 1043.76 | .00 | 7.42 | .00 | 9.000 | .000 | .00 | 1 .0
      | | | | | | | | | | | | | | | |
JUNCT STR | .0697 | | | | | | | | | | | | | | | |
1757.840 | 1031.790 | 10.781 | 1042.571 | 612.00 | 13.85 | 2.98 | 1045.55 | .00 | 6.34 | .00 | 7.500 | .000 | .00 | 1 .0
      | | | | | | | | | | | | | | | |
.010 | .0000 | | | | | | | | | | | | | | | |
1757.850 | 1031.790 | 10.781 | 1042.572 | 612.00 | 13.85 | 2.98 | 1045.55 | .00 | 6.34 | .00 | 7.500 | .000 | .00 | 1 .0
      | | | | | | | | | | | | | | | |
    
```

1665

T1 FONTANA / SIERRA AVE. LINE"B"

0

T2 25 YEAR STORM

T3 JN 04339

SO	1757.8501031.790	1						1042.570	
R	2441.5001034.530	1	.013						.000
	.000 0								
JX	2441.5101034.530	1 2	.013	36.000				1039.150	-90.0
	.000								
R	3590.5801039.120	1	.013						.000
	.000 0								
JX	3607.6501039.990	4 3	.014	172.000				1042.180	.0
	30.000								
R	3607.6601039.990	4	.013						.000
	.000 0								
SH	3607.6601039.990	4						1039.990	
CD	1 4 1	.000	7.500	.000	.000	.000	.000	.00	
CD	2 4 1	.000	3.000	.000	.000	.000	.000	.00	
CD	3 4 1	.000	4.500	.000	.000	.000	.000	.00	
CD	4 4 1	.000	6.000	.000	.000	.000	.000	.00	
Q	404.000	.0							

WATER SURFACE PROFILE - CHANNEL DEFINITION LISTING

CARD	SECT	CHN	NO OF	AVE PIER	HEIGHT 1	BASE	ZL	ZR	INV	Y(1)	Y(2)	Y(3)	Y(4)	Y(5)	Y(6)	Y(7)	Y(8)	Y(9)	Y(10)
CODE	NO	TYPE	PIER/PIP	WIDTH	DIAMETER	WIDTH			DROP										
CD	1	4	1		7.500														
CD	2	4	1		3.000														
CD	3	4	1		4.500														
CD	4	4	1		6.000														

PAGE NO 1

W S P G W  
WATER SURFACE PROFILE - TITLE CARD LISTING

HEADING LINE NO 1 IS - FONTANA / SIERRA AVE. LINE"B"  
 HEADING LINE NO 2 IS - 25 YEAR STORM  
 HEADING LINE NO 3 IS - JN 04339

W S P G W  
WATER SURFACE PROFILE - ELEMENT CARD LISTING

PAGE NO 2

ELEMENT NO	DESCRIPTION	U/S DATA	STATION	INVERT	SECT	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4	RADIUS	ANGLE	ANG PT	MAN H
1	IS A SYSTEM OUTLET		1757.850	1031.790	1								1042.570			
2	IS A REACH		2441.500	1034.530	1	.013							.000	.000	.000	0
3	IS A JUNCTION		2441.510	1034.530	1	.013	36.000		.000	1039.150	.000	-90.000	.000	.000		.000
THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING																
THE ABOVE ELEMENT CONTAINED AN INVERT ELEV WHICH WAS NOT GREATER THAN THE PREVIOUS INVERT ELEV -WARNING																
4	IS A REACH		3590.580	1039.120	1	.013							.000	.000	.000	0
5	IS A JUNCTION		3607.650	1039.990	4	.014	172.000		.000	1042.180	.000	.000	32.601	30.000		.000
6	IS A REACH		3607.660	1039.990	4	.013							.000	.000	.000	0
7	IS A SYSTEM HEADWORKS		3607.660	1039.990	4								1039.990			

FONTANA / SIERRA AVE. LINE"B"  
 25 YEAR STORM  
 JN 04339

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt/or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1757.850	1031.790	10.780	1042.570	612.00	13.85	2.98	1045.55	.00	6.34	.00	7.500	.000	.00	1 .0
683.650	.0040					.0064	4.34	10.78	.00	7.50	.013	.00	.00	PIPE
2441.500	1034.530	12.383	1046.913	612.00	13.85	2.98	1049.89	.00	6.34	.00	7.500	.000	.00	1 .0
JUNCT STR	.0000					.0060	.00	12.38	.00		.013	.00	.00	PIPE
2441.510	1034.530	13.063	1047.593	576.00	13.04	2.64	1050.23	.00	6.18	.00	7.500	.000	.00	1 .0
1149.070	.0040					.0056	6.47	13.06	.00	7.50	.013	.00	.00	PIPE
3590.580	1039.120	14.939	1054.059	576.00	13.04	2.64	1056.70	.00	6.18	.00	7.500	.000	.00	1 .0
JUNCT STR	.0510					.0085	.15	.00	.00		.014	.00	.00	PIPE
3607.650	1039.990	14.109	1054.099	404.00	14.29	3.17	1057.27	.00	5.35	.00	6.000	.000	.00	1 .0
.010	.0000					.0091	.00	14.11	.00	.00	.013	.00	.00	PIPE
3607.660	1039.990	14.109	1054.099	404.00	14.29	3.17	1057.27	.00	5.35	.00	6.000	.000	.00	1 .0

T1 FONTANA / SIERRA AVE. LINE"C"  
0

T2 25 YEAR STORM

T3 JN 04339

SO	3607.3301042.180	1						1054.100	
R	3787.6901051.310	1		.013					.000
	.000 0								
JX	3794.3501051.480	1	2	.014	29.000			1052.860	-85.0
	.000								
R	3794.3601051.480	1		.013					.000
	.000 0								
SH	3794.3601051.480	1						1051.480	
CD	1 4 1	.000	4.500	.000	.000	.000	.000	.00	
CD	2 4 1	.000	2.000	.000	.000	.000	.000	.00	
Q		149.000	.0						





T1 FONTANA / SIERRA AVE. LINE"D"

0

T2 25 YEAR STORM

T3 JN 04339

SO	3794.3601051.480	1				1056.780			
R	5219.3701065.020	1		.013				.000	
	.000 0								
JX	5227.2801055.560	3	2	2.014	30.000	28.0001066.2001066.200	45.0-45.0		
	.000								
R	5602.4801069.340	5		.013				.000	
	.000 0								
JX	5607.1401069.880	7		.014					
R	6270.8101076.000	7		.013				.000	
	.000 0								
R	6343.0401076.740	7		.013				91.966	
	.000 0								
R	6358.1601076.720	7		.013				.000	
	.000 0								
JX	6362.8301076.740	7	8	.014	31.000	1077.500		-45.0	
	.000								
R	6763.1801078.340	7		.013				.000	
	.000 0								
JX	6773.1801078.370	7	2	.014	29.000	1078.650		-30.0	
	.000								
R	7239.9301080.330	7		.013				.000	
	.000 0								
R	7373.4301081.000	7		.013				.000	
	.000 0								
R	7387.9301081.070	7		.013				.000	
	.000 0								
SH	7387.9301081.070	7				1081.070			
CD	1 4 1	.000	4.500	.000	.000	.000	.00		
CD	2 4 1	.000	3.000	.000	.000	.000	.00		
CD	3 4 1	.000	4.000	.000	.000	.000	.00		
CD	5 4 1	.000	4.000	.000	.000	.000	.00		
CD	7 4 1	.000	3.500	.000	.000	.000	.00		
CD	8 4 1	.000	2.000	.000	.000	.000	.00		
Q		31.000	.0						



U/S DATA	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4
	6362.830	1076.740	7	8	0	.014	31.000	.000	1077.500	.000	-45.000	.000
									RADIUS	ANGLE		
									.000	.000		

PAGE NO 3

W S P G W  
 WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	10	IS A REACH	*	*	*									
		U/S DATA	STATION	INVERT	SECT	N			RADIUS	ANGLE	ANG PT	MAN H		
			6763.180	1078.340	7	.013			.000	.000	.000	0		
ELEMENT NO	11	IS A JUNCTION	*	*	*				*	*	*			
		U/S DATA	STATION	INVERT	SECT	LAT-1	LAT-2	N	Q3	Q4	INVERT-3	INVERT-4	PHI 3	PHI 4
			6773.180	1078.370	7	2	0	.014	29.000	.000	1078.650	.000	-30.000	.000
											RADIUS	ANGLE		
											.000	.000		
ELEMENT NO	12	IS A REACH	*	*	*									
		U/S DATA	STATION	INVERT	SECT	N			RADIUS	ANGLE	ANG PT	MAN H		
			7239.930	1080.330	7	.013			.000	.000	.000	0		
ELEMENT NO	13	IS A REACH	*	*	*									
		U/S DATA	STATION	INVERT	SECT	N			RADIUS	ANGLE	ANG PT	MAN H		
			7373.430	1081.000	7	.013			.000	.000	.000	0		
ELEMENT NO	14	IS A REACH	*	*	*									
		U/S DATA	STATION	INVERT	SECT	N			RADIUS	ANGLE	ANG PT	MAN H		
			7387.930	1081.070	7	.013			.000	.000	.000	0		
ELEMENT NO	15	IS A SYSTEM HEADWORKS	*	*	*									
		U/S DATA	STATION	INVERT	SECT									
			7387.930	1081.070	7									

W S ELEV  
 1081.070

FONTANA / SIERRA AVE. LINE"D"  
 25 YEAR STORM  
 JN 04339

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt/or I.D.	ZL	No Prs/Pip	Wth
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type	Ch
3794.360	1051.480	5.300	1056.780	149.00	9.37	1.36	1058.14	.00	3.58	.00	4.500	.000	.00	1	.0
212.739	.0095					.0057	1.21	5.30	.00	2.98	.013	.00	.00	PIPE	
4007.099	1053.501	4.500	1058.001	149.00	9.37	1.36	1059.36	.00	3.58	.00	4.500	.000	.00	1	.0
44.426	.0095					.0053	.24	4.50	.00	2.98	.013	.00	.00	PIPE	
4051.525	1053.923	4.258	1058.182	149.00	9.57	1.42	1059.60	.00	3.58	2.03	4.500	.000	.00	1	.0
HYDRAULIC JUMP															
4051.525	1053.923	2.982	1056.905	149.00	13.32	2.75	1059.66	.00	3.58	4.26	4.500	.000	.00	1	.0
620.664	.0095					.0095	5.90	2.98	1.45	2.98	.013	.00	.00	PIPE	
4672.188	1059.821	2.982	1062.803	149.00	13.32	2.75	1065.56	.00	3.58	4.26	4.500	.000	.00	1	.0
259.206	.0095					.0095	2.45	2.98	1.45	2.98	.013	.00	.00	PIPE	
4931.395	1062.284	2.988	1065.272	149.00	13.28	2.74	1068.01	.00	3.58	4.25	4.500	.000	.00	1	.0
203.938	.0095					.0089	1.82	2.99	1.44	2.98	.013	.00	.00	PIPE	
5135.333	1064.221	3.119	1067.341	149.00	12.67	2.49	1069.83	.00	3.58	4.15	4.500	.000	.00	1	.0
55.949	.0095					.0080	.45	3.12	1.33	2.98	.013	.00	.00	PIPE	
5191.282	1064.753	3.259	1068.012	149.00	12.08	2.26	1070.28	.00	3.58	4.02	4.500	.000	.00	1	.0
22.196	.0095					.0071	.16	3.26	1.22	2.98	.013	.00	.00	PIPE	
5213.478	1064.964	3.412	1068.376	149.00	11.51	2.06	1070.44	.00	3.58	3.85	4.500	.000	.00	1	.0
5.892	.0095					.0064	.04	3.41	1.11	2.98	.013	.00	.00	PIPE	

10/12

Program Package Serial Number: 1432

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 5:33:13

FONTANA / SIERRA AVE. LINE"D"  
25 YEAR STORM  
JN 04339

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT or I.D.	Base Wt	ZL	No Prs/Pip	Wth
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type	Ch
5219.370	1065.020	3.582	1068.602	149.00	10.98	1.87	1070.47	.00	3.58	3.63	4.500	.000	.00	1	.0
JUNCT STR	-1.1960					.0058	.05	3.58	1.00		.014	.00	.00	PIPE	
5227.280	1055.560	15.222	1070.782	91.00	7.24	.81	1071.60	.00	2.89	.00	4.000	.000	.00	1	.0
331.015	.0367					.0040	1.33	15.22	.00	1.58	.013	.00	.00	PIPE	
5558.295	1067.717	4.393	1072.110	91.00	7.24	.81	1072.92	.00	2.89	.00	4.000	.000	.00	1	.0
HYDRAULIC JUMP															
5558.295	1067.717	1.816	1069.533	91.00	16.40	4.18	1073.71	.00	2.89	3.98	4.000	.000	.00	1	.0
15.944	.0367					.0213	.34	1.82	2.45	1.58	.013	.00	.00	PIPE	
5574.239	1068.303	1.869	1070.172	91.00	15.79	3.87	1074.05	.00	2.89	3.99	4.000	.000	.00	1	.0
15.945	.0367					.0190	.30	1.87	2.32	1.58	.013	.00	.00	PIPE	
5590.184	1068.888	1.939	1070.827	91.00	15.06	3.52	1074.35	.00	2.89	4.00	4.000	.000	.00	1	.0
12.296	.0367					.0168	.21	1.94	2.16	1.58	.013	.00	.00	PIPE	
5602.480	1069.340	2.014	1071.354	91.00	14.36	3.20	1074.56	.00	2.89	4.00	4.000	.000	.00	1	.0
JUNCT STR	.1159					.0144	.07	2.01	2.01		.014	.00	.00	PIPE	
5607.140	1069.880	2.702	1072.582	91.00	11.42	2.02	1074.61	.00	2.96	2.94	3.500	.000	.00	1	.0
522.263	.0092					.0092	4.82	2.70	1.22	2.70	.013	.00	.00	PIPE	
6129.403	1074.696	2.702	1077.398	91.00	11.42	2.02	1079.42	.00	2.96	2.94	3.500	.000	.00	1	.0
141.407	.0092					.0094	1.33	2.70	1.22	2.70	.013	.00	.00	PIPE	

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 5:33:13

FONTANA / SIERRA AVE. LINE"D"  
 25 YEAR STORM  
 JN 04339

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT or I.D.	Base Wt	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
6270.810	1076.000	2.649	1078.649	91.00	11.65	2.11	1080.76	.28	2.96	3.00	3.500	.000	.00	1 .0
19.022	.0102					.0095	.18	2.93	1.27	2.58	.013	.00	.00	PIPE
6289.833	1076.195	2.671	1078.866	91.00	11.55	2.07	1080.94	.27	2.96	2.98	3.500	.000	.00	1 .0
44.009	.0102					.0090	.40	2.94	1.25	2.58	.013	.00	.00	PIPE
6333.842	1076.646	2.804	1079.450	91.00	11.01	1.88	1081.33	.23	2.96	2.79	3.500	.000	.00	1 .0
9.198	.0102					.0082	.07	3.04	1.13	2.58	.013	.00	.00	PIPE
6343.040	1076.740	2.957	1079.697	91.00	10.49	1.71	1081.41	.00	2.96	2.53	3.500	.000	.00	1 .0
1.916	-.0013					.0075	.01	2.96	1.00	.00	.013	.00	.00	PIPE
6344.956	1076.737	3.105	1079.842	91.00	10.09	1.58	1081.42	.00	2.96	2.22	3.500	.000	.00	1 .0
6.074	-.0013					.0072	.04	3.10	.88	.00	.013	.00	.00	PIPE
6351.030	1076.729	3.260	1079.990	91.00	9.75	1.48	1081.47	.00	2.96	1.77	3.500	.000	.00	1 .0
7.130	-.0013					.0071	.05	3.26	.75	.00	.013	.00	.00	PIPE
6358.160	1076.720	3.375	1080.095	91.00	9.57	1.42	1081.52	.00	2.96	1.30	3.500	.000	.00	1 .0
JUNCT STR	.0043					.0062	.03	3.38	.62		.014	.00	.00	PIPE
6362.830	1076.740	4.293	1081.033	60.00	6.24	.60	1081.64	.00	2.43	.00	3.500	.000	.00	1 .0
400.350	.0040					.0036	1.42	4.29	.00	2.71	.013	.00	.00	PIPE
6763.180	1078.340	4.117	1082.457	60.00	6.24	.60	1083.06	.00	2.43	.00	3.500	.000	.00	1 .0
JUNCT STR	.0030					.0026	.03	4.12	.00		.014	.00	.00	PIPE

Program Package Serial Number: 1432

WATER SURFACE PROFILE LISTING

Date: 1-16-2005 Time: 5:33:13

FONTANA / SIERRA AVE. LINE"D"  
25 YEAR STORM  
JN 04339

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt/or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
6773.180	1078.370	4.666	1083.036	31.00	3.22	.16	1083.20	.00	1.72	.00	3.500	.000	.00	1 .0
358.822	.0042					.0009	.34	4.67	.00	1.70	.013	.00	.00	PIPE
7132.002	1079.877	3.500	1083.377	31.00	3.22	.16	1083.54	.00	1.72	.00	3.500	.000	.00	1 .0
92.816	.0042					.0009	.08	3.50	.00	1.70	.013	.00	.00	PIPE
7224.818	1080.266	3.175	1083.442	31.00	3.38	.18	1083.62	.00	1.72	2.03	3.500	.000	.00	1 .0
15.112	.0042					.0008	.01	3.18	.28	1.70	.013	.00	.00	PIPE
7239.930	1080.330	3.120	1083.450	31.00	3.42	.18	1083.63	.00	1.72	2.18	3.500	.000	.00	1 .0
38.474	.0050					.0009	.03	3.12	.30	1.61	.013	.00	.00	PIPE
7278.404	1080.523	2.942	1083.465	31.00	3.59	.20	1083.67	.00	1.72	2.56	3.500	.000	.00	1 .0
31.728	.0050					.0010	.03	2.94	.34	1.61	.013	.00	.00	PIPE
7310.132	1080.682	2.793	1083.475	31.00	3.77	.22	1083.70	.00	1.72	2.81	3.500	.000	.00	1 .0
27.727	.0050					.0011	.03	2.79	.39	1.61	.013	.00	.00	PIPE
7337.858	1080.822	2.661	1083.483	31.00	3.95	.24	1083.72	.00	1.72	2.99	3.500	.000	.00	1 .0
24.883	.0050					.0012	.03	2.66	.43	1.61	.013	.00	.00	PIPE
7362.741	1080.946	2.541	1083.488	31.00	4.14	.27	1083.75	.00	1.72	3.12	3.500	.000	.00	1 .0
10.689	.0050					.0013	.01	2.54	.47	1.61	.013	.00	.00	PIPE
7373.430	1081.000	2.489	1083.489	31.00	4.24	.28	1083.77	.00	1.72	3.17	3.500	.000	.00	1 .0
14.500	.0048					.0013	.02	2.49	.49	1.63	.013	.00	.00	PIPE

FONTANA / SIERRA AVE. LINE"D"  
 25 YEAR STORM  
 JN 04339

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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height/ | Base Wt | | No Wth
      | Elev  | (FT)  | Elev  | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip
L/Elem | Ch Slope | | | | | SF Ave | HF | SE Dpth | Froude N | Norm Dp | "N" | X-Fall | ZR | Type Ch
*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****
7387.930 | 1081.070 | 2.422 | 1083.492 | 31.00 | 4.36 | .30 | 1083.79 | .00 | 1.72 | 3.23 | 3.500 | .000 | .00 | 1 | .0
      | - | - | - | - | - | - | - | - | - | - | - | - | - | - | -
    
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1617

**HALL & FORRESTER**  
Exchange  
Riverside, CA 92502-1501  
4500  
665-4501

\_\_\_\_\_ FONTANA \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

JOB No. 04339  
BY HERMAN  
DATE 1/19/05  
SHT. 99  
OF \_\_\_\_\_

◆ LAND PLANNING ◆ CIVIL ENGINEERING ◆ SURVEYING

# HYDRAULICS

## FOR

# INDIVIDUAL PIPES

Subject CHECK MASTER PLAN  
STORM DRAIN PIPE SIZES  
 By HERMAN  
 Dept. IRVINE

Date 8/6/04  
 Project Name FONTANA  
 Project No. 04339  
 Page No. ① of \_\_\_\_\_

NODES	ΔH	L	S	Q <sub>25</sub>	Given Size	?	Proposed Size
* DZ-2A							
55-54	1.7	340	0.0045	125	63"	✓	
54-53	4.3	860	0.0045	112	60"	✓	
53-52	2.5	500	0.0045	82	42"	X	48"
52-116	7.7	650	0.0108	51	39"	✓	
* DZ-2							
63-57	1.8	560	0.0029	404	87"	✓	
57-56	2.0	640	0.0029	343	84"	✓	
56-55	3.2	1000	0.0029	259	78"	✓	
55-51	8.9	900	0.009	70	42"	✓	
51-50	8.2	1,320	0.0056	49	39"	✓	
* 50-102	5.8	460	0.0117		24"	Built	
* 50-105	4.3	570	0.0068		30"	Built	
* DZ-1							
71-70	4.0	800	0.0045	* 408	102"	✓	
70-69	4.2	880	0.0043	* 280	102"	✓	
69-68	2.0	400	0.0045	* 250	93"	✓	
68-67	3.8	760	0.0045	* 160	84"	✓	
67-66	3.8	760	0.0045	* 131	75"	✓	
66-65	3.3	660	0.0045	* 67	57"	✓	
65-302	3.3	660	0.0045	* 49	36"	X	42"
70-331	4.0	800	0.0045	* 71	42"	✓	
68-319	13.0	900	0.0126	* 75	48"	✓	
* DZ-4							
90-45	19.0	750	0.018	104	42"	✓	
45-607	6.0	660	0.0081	70	36"	X	42"



# Hall & Foreman, Inc.

Subject \_\_\_\_\_

Date \_\_\_\_\_

By \_\_\_\_\_

Project Name \_\_\_\_\_

Dept. \_\_\_\_\_

Project No. \_\_\_\_\_

Page No. (2) of \_\_\_\_\_

* DZ-4A							
91-46	11.9	750	0.0135	79	42"	✓	
46-629	7.3	660	0.0099	52	36"	✓	
* DZ-6							
35-34	6.2	660	0.0085	167	39"	X	54"
34-33	12.8	990	0.0117	122	39"	X	48"
33-717	14.0	990	0.0126	71	39"	✓	
* DZ-7							
38-37	5.9	660	0.0075	153	42"	X	54"
37-36	10.9	990	0.0095	118	42"	X	48"
36-803	19.0	990	0.0135	68	42"	✓	
* DZ-5							
94-40	7.3	900	0.0072		102"	Built	
40-39	13.8	1,720	0.0072	* 707	84"	X	96"
39-38	8.4	990	0.0077	* 680	84"	X	90"
38-35	8.0	1,320	0.0054	* 444	84"	✓	
35-32	11.0	1,320	0.0075	146	51"	✓	
32-31	4.6	660	0.0063	119	39"	X	48"
31-30	3.8	990	0.0034	82	39"	X	48"
30-704	10.0	990	0.0101	56	36"	✓	

\*722 Indicates Q<sub>100</sub>

LINE "DZ-2A"

Circular Channel Analysis & Design  
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2A / INDIVIDUAL PIPE 55-54

Solve For Actual Depth

Given Input Data:

Diameter.....	5.25 ft
Slope.....	0.0045 ft/ft
Manning's n.....	0.013
Discharge.....	123.00 cfs

Computed Results:

Depth.....	2.99 ft
Velocity.....	9.67 fps
Flow Area.....	12.71 sf
Critical Depth....	3.13 ft
Critical Slope....	0.0039 ft/ft
Percent Full.....	56.88 %
Full Capacity.....	198.99 cfs
QMAX @.94D.....	214.05 cfs
Froude Number.....	1.09 (flow is Supercritical)

Circular Channel Analysis & Design  
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2A / INDIVIDUAL PIPE 54-53

Solve For Actual Depth

Given Input Data:

Diameter.....	5.00 ft
Slope.....	0.0045 ft/ft
Manning's n.....	0.013
Discharge.....	109.00 cfs

Computed Results:

Depth.....	2.86 ft
Velocity.....	9.38 fps
Flow Area.....	11.61 sf
Critical Depth....	2.98 ft
Critical Slope....	0.0040 ft/ft
Percent Full.....	57.21 %
Full Capacity....	174.71 cfs
QMAX @.94D.....	187.94 cfs
Froude Number.....	1.08 (flow is Supercritical)

Circular Channel Analysis & Design  
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2A / INDIVIDUAL PIPE 53-52

Solve For Actual Depth

Given Input Data:

Diameter.....	4.00 ft
Slope.....	0.0045 ft/ft
Manning's n.....	0.013
Discharge.....	80.00 cfs

Computed Results:

Depth.....	2.78 ft
Velocity.....	8.57 fps
Flow Area.....	9.33 sf
Critical Depth....	2.71 ft
Critical Slope....	0.0048 ft/ft
Percent Full.....	69.55 %
Full Capacity.....	96.36 cfs
QMAX @.94D.....	103.65 cfs
Froude Number.....	0.95 (flow is Subcritical)

Circular Channel Analysis & Design  
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2A / INDIVIDUAL PIPE 52-116

Solve For Actual Depth

Given Input Data:

Diameter.....	3.75 ft
Slope.....	0.0108 ft/ft
Manning's n.....	0.013
Discharge.....	49.00 cfs

Computed Results:

Depth.....	1.63 ft
Velocity.....	10.67 fps
Flow Area.....	4.59 sf
Critical Depth....	2.14 ft
Critical Slope....	0.0042 ft/ft
Percent Full.....	43.36 %
Full Capacity....	125.68 cfs
QMAX @.94D.....	135.19 cfs
Froude Number.....	1.69 (flow is Supercritical)

LINE "DZ-2"

Circular Channel Analysis & Design  
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2 / INDIVIDUAL PIPE 63-57

Solve For Actual Depth

Given Input Data:

Diameter.....	7.25 ft
Slope.....	0.0029 ft/ft
Manning's n.....	0.013
Discharge.....	398.00 cfs

Computed Results:

Depth.....	6.37 ft
Velocity.....	10.35 fps
Flow Area.....	38.44 sf
Critical Depth....	5.21 ft
Critical Slope....	0.0043 ft/ft
Percent Full.....	87.91 %
Full Capacity.....	377.77 cfs
QMAX @.94D.....	406.37 cfs
Froude Number.....	0.64 (flow is Subcritical)

Circular Channel Analysis & Design  
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2 / INDIVIDUAL PIPE 57-56

Solve For Actual Depth

Given Input Data:

Diameter.....	7.00 ft
Slope.....	0.0029 ft/ft
Manning's n.....	0.013
Discharge.....	339.00 cfs

Computed Results:

Depth.....	5.65 ft
Velocity.....	10.19 fps
Flow Area.....	33.27 sf
Critical Depth....	4.85 ft
Critical Slope....	0.0041 ft/ft
Percent Full.....	80.67 %
Full Capacity.....	344.02 cfs
QMAX @.94D.....	370.07 cfs
Froude Number.....	0.73 (flow is Subcritical)

Circular Channel Analysis & Design  
Solved with Manning's Equation

Open Channel - Uniform flow

Worksheet Name: FONTANA / JN 04339

Comment: DZ-2 / INDIVIDUAL PIPE 56-55

Solve For Actual Depth

Given Input Data:

Diameter.....	6.50 ft
Slope.....	0.0029 ft/ft
Manning's n.....	0.013
Discharge.....	256.00 cfs

Computed Results:

Depth.....	4.85 ft
Velocity.....	9.64 fps
Flow Area.....	26.56 sf
Critical Depth....	4.29 ft
Critical Slope....	0.0040 ft/ft
Percent Full.....	74.64 %
Full Capacity.....	282.33 cfs
QMAX @.94D.....	303.71 cfs
Froude Number.....	0.78 (flow is Subcritical)